

Laurence and Associates, LLC 918 Government Street Mobile, AL 36604

February 7th, 2024

SOUTH CAROLINA PORTS AUTHORITY 200 Ports Authority Dr Mt Pleasant, SC 29464

Attention: Eric J. Scanlon

Mechanical Technical Specialist, Crane and Equipment Maintenance

Subject: SCPA ZPMC Crane H-39-037 (#37) Vessel Impact Damage Assessment

LA, LLC Project Number 2405

#### Mr. Scanlon.

We have inspected the damage due to vessel impact with the boom of ZPMC Crane #37 at the North Charleston Terminal (NCT) in North Charleston, SC. The initial inspection was carried out between January 5<sup>th</sup> and January 8<sup>th</sup>, 2024 immediately after the vessel impact event. Additional inspection work was carried out on January 11<sup>th</sup>, 2024 and on February 5<sup>th</sup>, 2024. The inspection included a visual inspection of the point of impact, some of the critical structural joints, obvious points of distress, and key components where alignment is critical (boom hinge, boom-girder trolley rail, and main equalizer beams). The inspection work was completed around activities to stabilize the crane.

The visible damage noted included a nearly complete wrecking of the gantry assemblies at each corner (compromising the cranes stability), minor damage to the checkers cabin, damage to the platforms and appurtenances at the boom tip (point of impact), dislodging of the crane from the pier's gantry rail system, and surface damage to the pier structure.

A visual survey of the boom hinge areas and the trolley rail along the length of the boom and girder indicates that the boom alignment is acceptable. Additionally, the boom has been raised and the trolley driven from about the middle of the boom to the extreme backreach position without issue, both providing further evidence that the boom alignment is acceptable.

The following reports on the emergency stabilization steps taken, recommendations for permanent stabilization and storage efforts, the recommendations for repair, and other work to be considered.

#### Emergency Stabilization:

The gantry assemblies provide the vertical and lateral support for the crane structure. The event caused significant damage to the gantry assembly such that their ability to support the crane dead weight or the lateral forces (from wind and operating inertia forces) has been compromised.

The pier structure is composed of pile supported reinforced concrete crane rail beams and interior reinforced concrete deck slabs. The crane rail beams are designed to support the operating load cases (wheel loads) of the crane (such as dead loads, lifted loads, wind loads, inertia loads, etc). The deck slabs are designed to carry the lighter loads imposed by terminal traffic (such as cargo laden trucks). During the event the crane was dislodged off of the crane rail beams and onto the deck slabs in several locations. Therefore, immediately after the event certain

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components of the pier structure were loaded in a manner that would not have been considered in their design.

The weather forecast immediately after the event called for poor conditions including rain and high wind. There was no confidence that the wrecked state of the gantry system would be adequate to support the dead load of the crane with additional lateral loads due to wind. The crane was in danger of collapse and that emergency stabilization efforts were required to eliminate the potential for additional damage to the crane, loss of the crane entirely, or additional damage to the pier structure.

Immediate steps were taken to enhance the stability of the crane structure as follows:

- 1. Wide flange columns/braces were welded to the sill beam at all four corners of the crane. The columns/braces were angled down from the sill beam to the top of the pier's concrete deck. In some cases, the bottom of the columns/braces were secured with water laden containers.
- 2. At least four of the eight main equalizer beam connections to the intermediate beams were in a visible state of failure. At these locations, the bolts securing the connections failed allowing the components to separate. Plate materials were field cut and welded between the separated components in an effort to preserve the post event condition of the connection.
- 3. In a clear weather window, the crane was further stabilized by removal of the compromised gantry assembly components below the main equalizer beam and placing the remaining crane structure on cribbing as follows:
  - a. Utilizing ZPMC NA's crane transporter beam (Big Bird) and Berard's Self Propelled Modular Transporters (SPMT's), the crane structure was lifted and relocated to the north end of the pier. During the relocation work the damaged 8x intermediate gantry assemblies (below the main equalizer), the 2x stowage pin brackets, the 4x tie down devices, portions of 2x landside stairways, and the checkers cabin were removed and placed in the yard.
  - b. The crane was placed on crib stacks of various materials provided by ZPMC NA and Berard in a strategic location of the pier which was suitable to support the crane dead weight with limited points of support.
  - c. Utilizing ZPMC NA's cribbing materials and their climbing jacks the crane was further and systematically lowered in elevation by about 4.5 ft until it rested firmly on 8x high capacity stands provided by ZPMC NA and Berard.

## Recommendations for Permanent Stabilization and Storage:

Although the emergency stabilization effort was completed, we are recommending additional stabilization efforts to secure and store the crane for a period of 6 months or more while replacement parts are procured and final repairs can be implemented.

1. As we expect that the procurement and installation of the needed replacement parts will take over 180 days, the current and governing building code stipulates that the means to secure the crane must be suitable for full hurricane winds. Therefore, we recommend that the crane, pier and support stands are analyzed for stowed load combinations including hurricane winds. If required by analysis, additional stands and tie down devices should be

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- added. This analysis is currently in the works and we have confirmed that at a minimum tie downs must be installed between the crane structure and the pier to prevent toppling in hurricane winds. We are still working toward verification of the pier and stands.
- 2. The gantry level crane-to-crane collision absorption system (bumpers) were removed with the damaged gantry assemblies leaving the crane vulnerable to gantry collisions. We recommend that temporary gantry end stops be fabricated and secured to the concrete gantry rail beams between Crane #37 and the adjacent operating crane. The intent of these end stops would be to prevent the adjacent ship to shore crane from inadvertently colliding with the subject crane.

## Recommendations for Repair:

The following outlines our recommendations for repair and returning the crane to service.

- 1. In order to eliminate doubt, replace all main equalizer beam to sill beam connection bolts. All of the collision forces flowed through these connections/bolts. The connection/bolts in question are not designed for such a load case.
- 2. During our inspection work on February 5<sup>th</sup>, we noted that although the distance between the main equalizer pins at corners 1/4 and corners 2/3 measured within ½" of each other, the straight-line measurements between the ends of the main equalizer beams at corners 1/4 and corners 2/3 varied by as much as 2 11/16" from the least to the greatest. This is an indication that some or all of the main equalizer beams may have rotated at their connection to the sill beam and/or that there could be damage to the main equalizer beam that has permanently changed their shape. We recommend that a licensed land surveyor be engaged to complete a thorough survey of the main equalizer beams relative to the sill beams. The survey information should then be evaluated to see if additional repairs are required at the main equalizer beams. While the surveyor is on site, it might be convenient to complete a survey of points of the boom relative to the sill beams for final verification that the boom-girder are correctly aligned.
- 3. Although a brief visual inspection of the crane has been completed, it focused on the point of impact, alignment of the boom-girder, and the gantry assemblies. We recommend that a more thorough point to point visual structural inspection is completed on the remaining crane structure.
- 4. All damaged platforms at the boom tip should be repaired. In addition to the platforms the walkway lighting system and lighting grounding system will need to be repaired. In order to complete this work, the crane will need to be boomed down and the trolley used to transmit materials to the boom tip. The current support system for the crane as well as the pier structure will need to be checked for this load combination. Booming down and moving the trolley toward the water will result in increased loads on the waterside supports (stands) and the pier.
- 5. We recommend that all of the components below the main equalizer beam be replaced with the exception of a few items which can easily be relocated. We make this recommendation for the following reasons:
  - a. The loads imposed during the event are not considered in the international design codes that would have been followed in the design of the crane. Therefore, we believe that through an analysis of the gantry componentry it would be determined that some to many of the components have been overloaded. Although

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the components are robust, overload conditions may result in a reduced expected useful life.

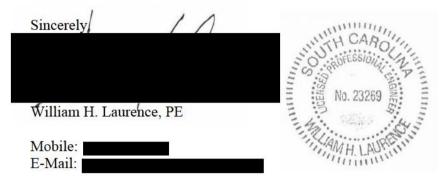
- b. The gantry assemblies are manufactured using designs, tolerances, and processes suitable for high grade machinery. This is required for the long term performance of the crane. The precession that was involved in the manufacture of the crane may have been offset by the slightest damage to an individual part.
  - i. It is possible that this damage would become evident through testing, but it may not become evident for years resulting in deteriorated crane performance and additional repair cost to SCPA at a later date.
  - ii. In the case that the damage becomes evident in testing, the process of repairing and returning the crane to service will be further delayed to the burden of SCPA.
- c. There is obvious physical damage to many components of the assemblies. However, most of the componentry is not visible and must be disassembled entirely to physically inspect and test in order to rule out any damage.
  - i. This work would need to be completed by personnel skilled in the manufacture, maintenance and repair of high grade machinery. It would be time consuming and expensive.
  - ii. We would expect that some or many of the components that did survive the event and might be reuseable in the future may be damaged in the work of salvaging from the other wrecked components.
- d. We understand that the original crane manufacture (ZPMC) has been engaged to provide the replacement components. They have the expertise to manufacture, assemble, outfit, and ship in significant sub-assemblies at very reasonable cost compared to what could be obtained in the US. Although we have not analyzed the potential cost differences, we would expect that receiving the sub-assemblies from ZPMC for installation by a US contractor would be more cost-effective than salvaging undamaged parts from the damaged assemblies, integrating them with the new components supplied by ZPMC and then installing them on the crane.
- e. The method of jacking the crane for the installation of the new components may be different than that used for removal. The method for jacking and installation should be planned/engineered prior to arrival of the new components in case additional jacking equipment is required to complete the work.
- f. After all repairs are completed above, the crane should be re-commissioned, tested (including overload testing), and recertified by OSHA.
- g. After the testing, the crane will need to be relocated to its proper position on the pier with the ZPMC NA crane transport system (Big Bird) and SPMT's.
- h. The temporary crane rail beam end stops will need to be removed.
- i. Once all of the above are completed the crane can be returned to service.

#### Other Work to Consider:

1. We recommend that the underside of the pier in the area of the event is inspected.

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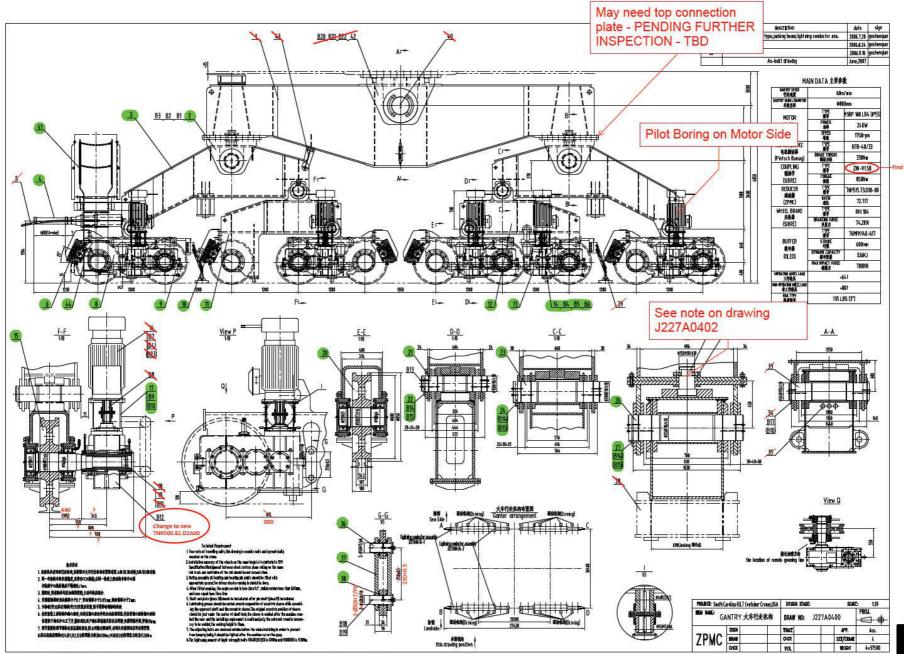
If you have any questions concerning this letter, please feel free to call or email.



## Attachments:

ZPMC gantry drawings with requested new parts indicated.

ZPMC crane general arrangement drawing.



\*Note - ZPMC Engineering to verify dimensions, component updates, and comments in red.



## SUBSIDIARY LIST

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<sup>\*</sup>Note - ZPMC Engineering to verify for accuracy

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\* The quantity and weight of this list is to one set

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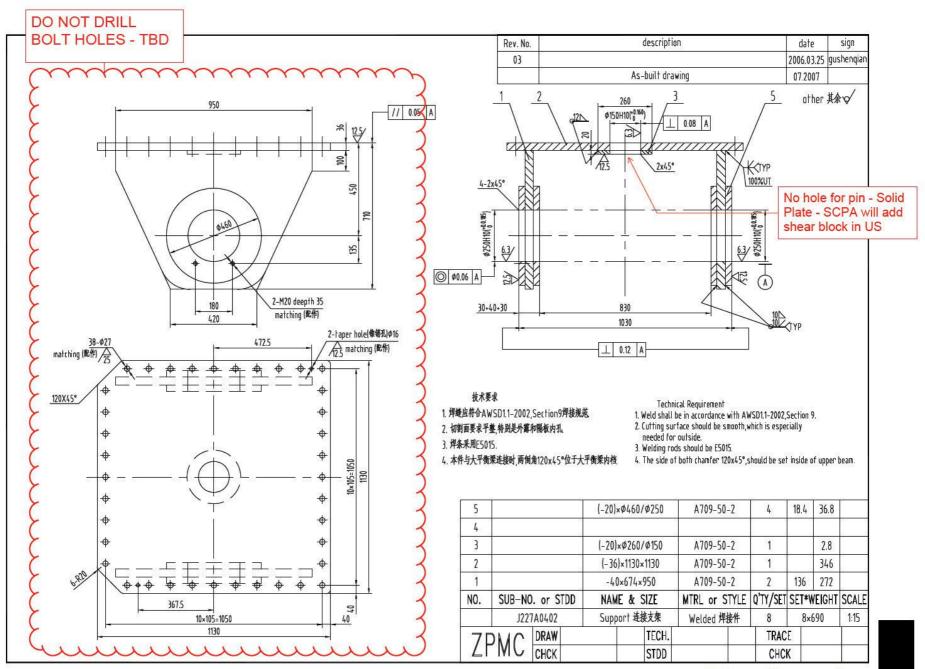
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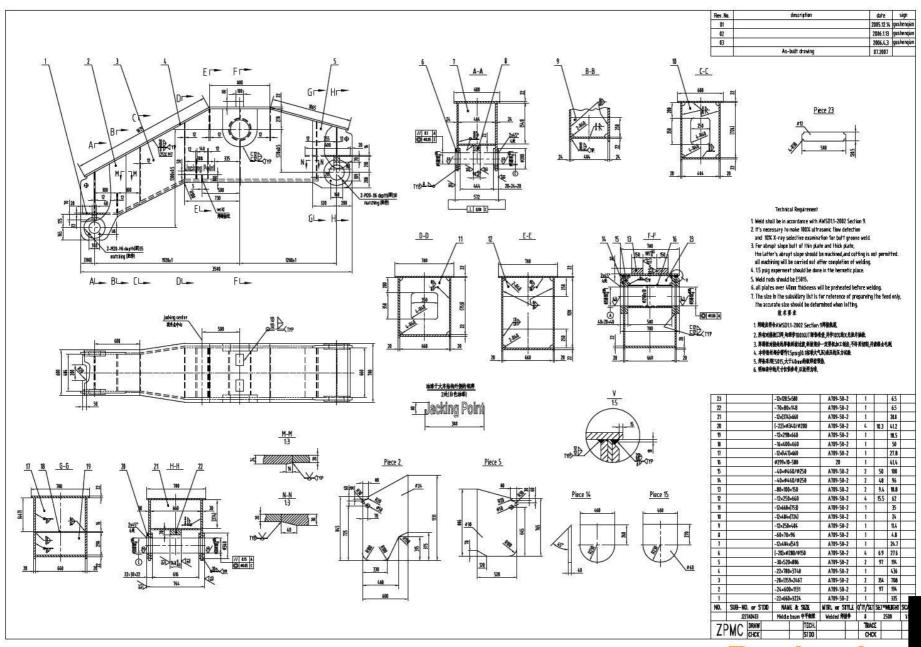
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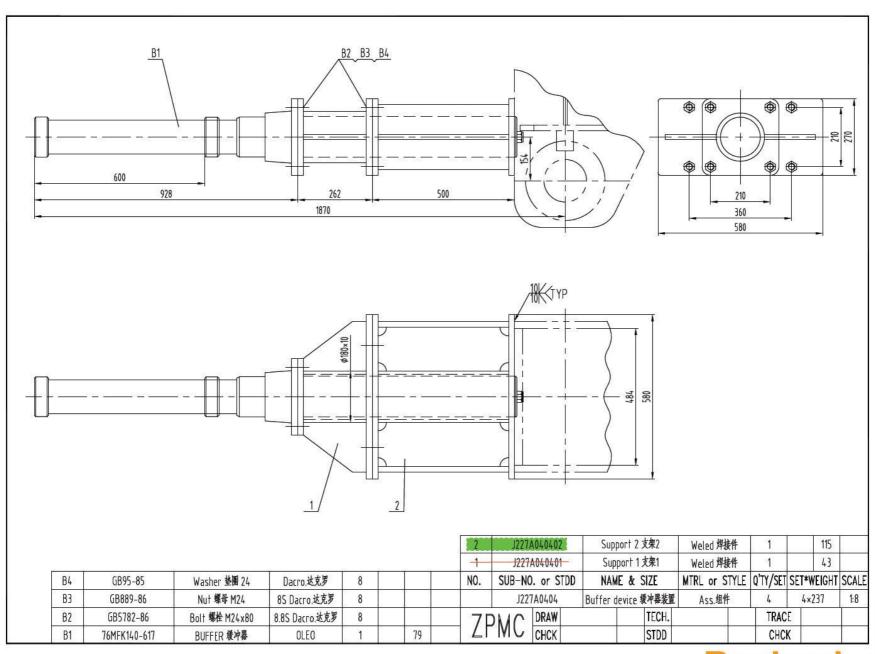
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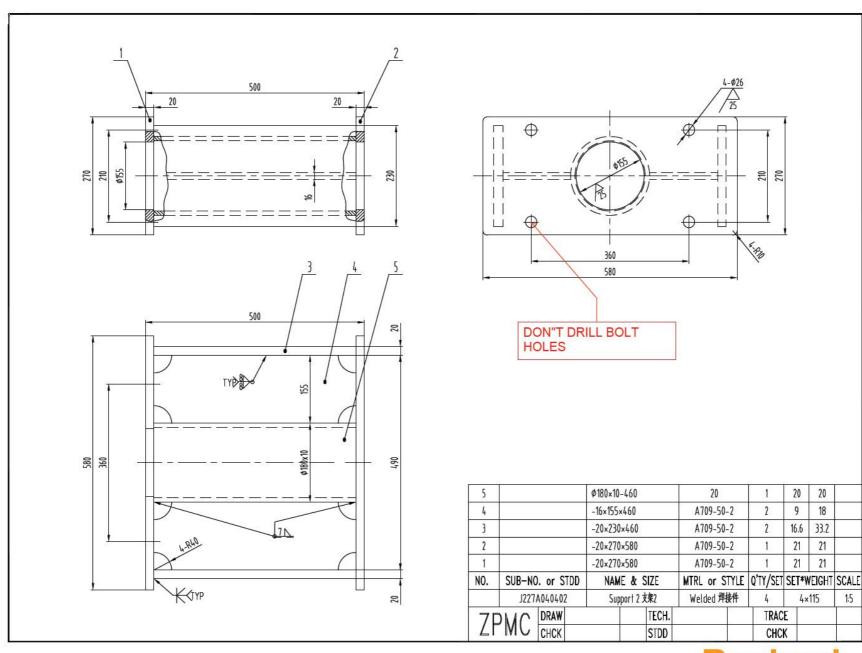




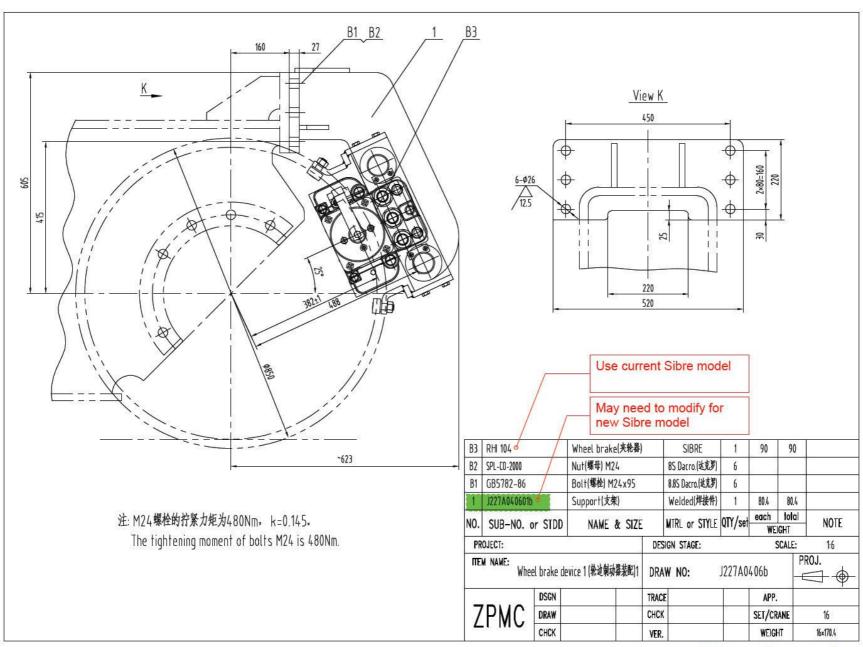
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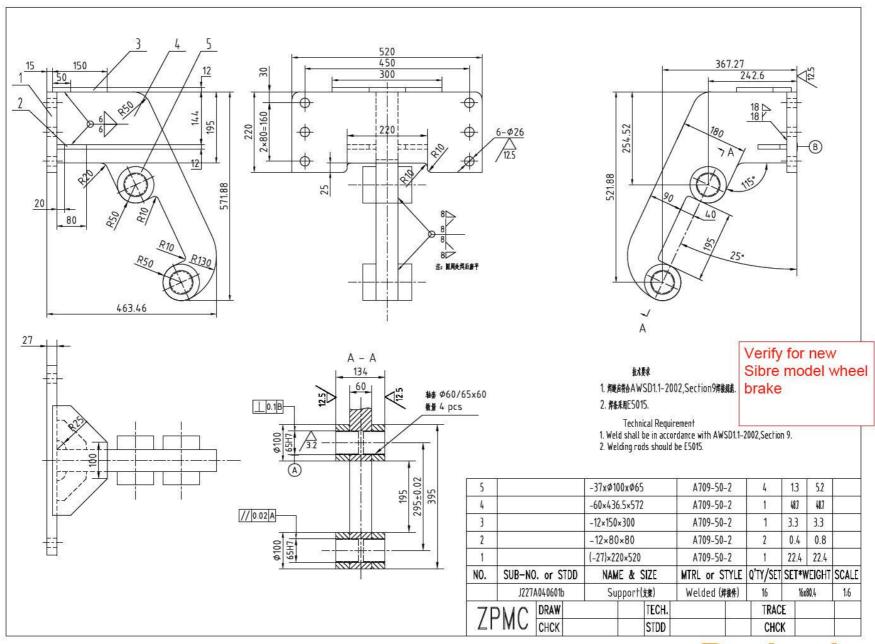






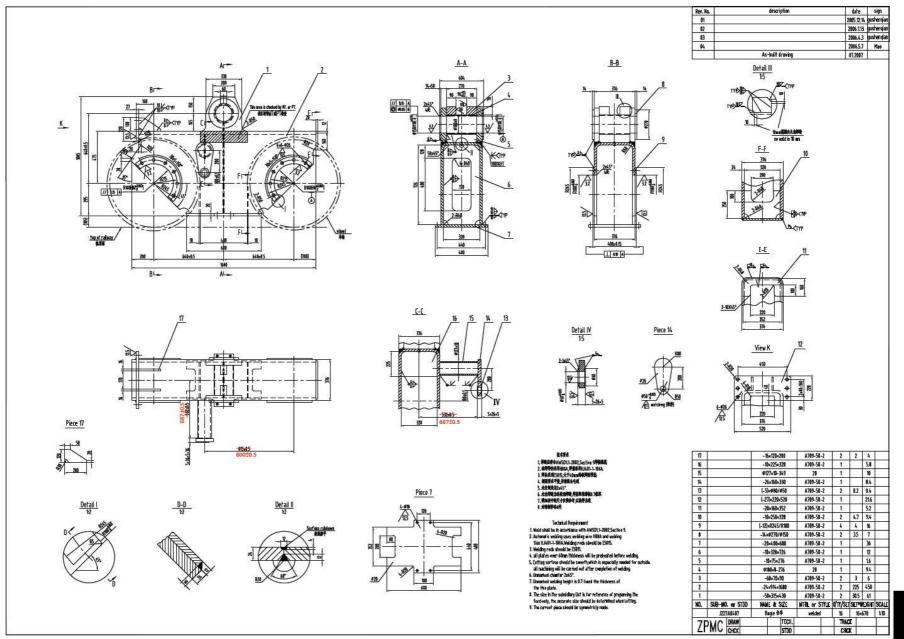
\*Note - ZPMC Engineering to verify dimensions, component updates, and comments in red.



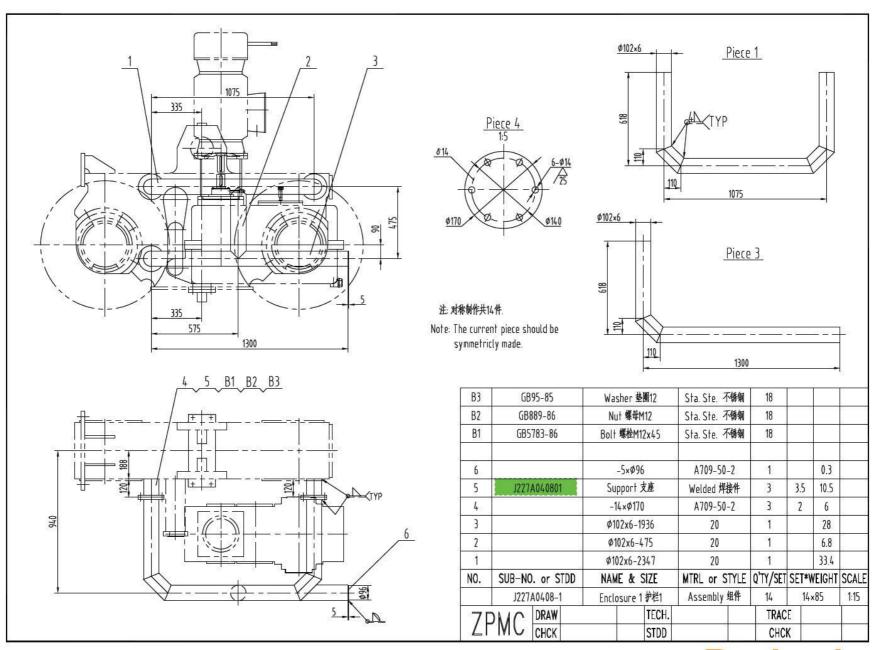


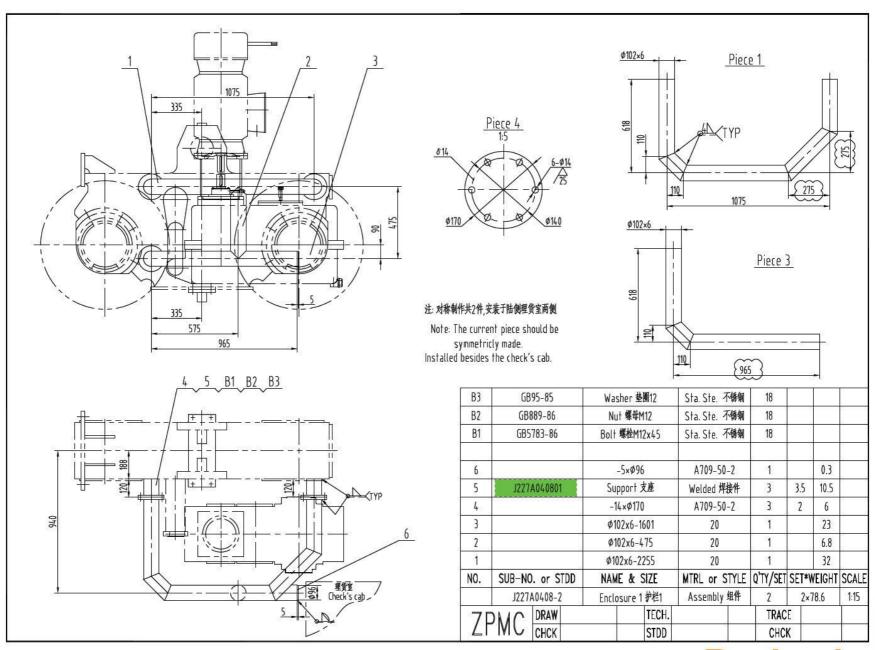
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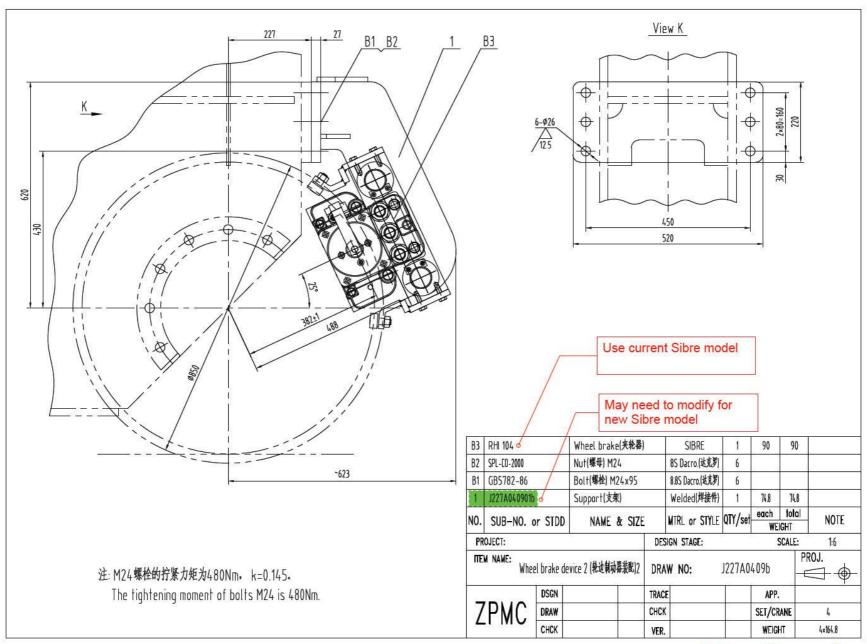




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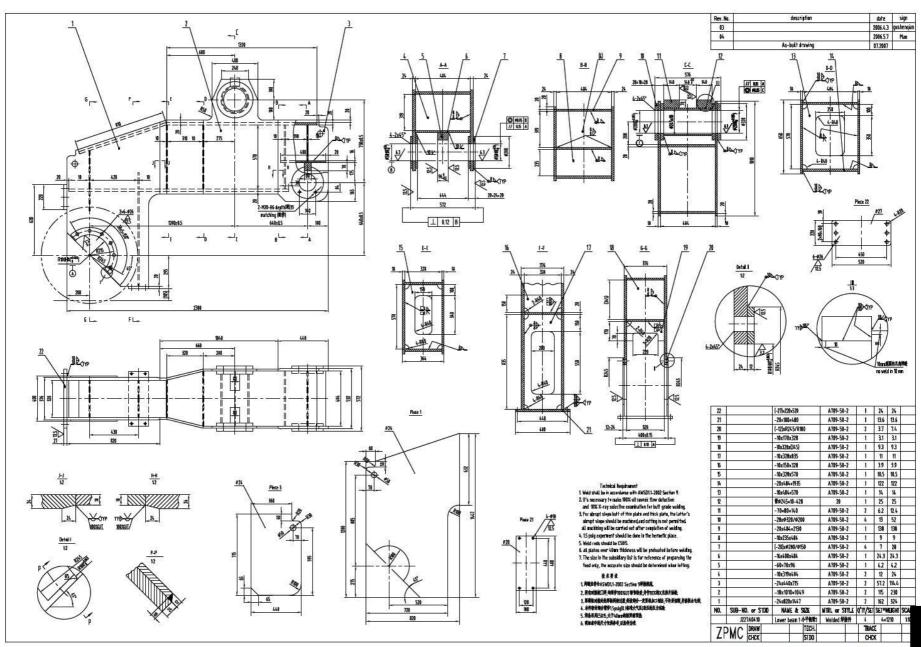






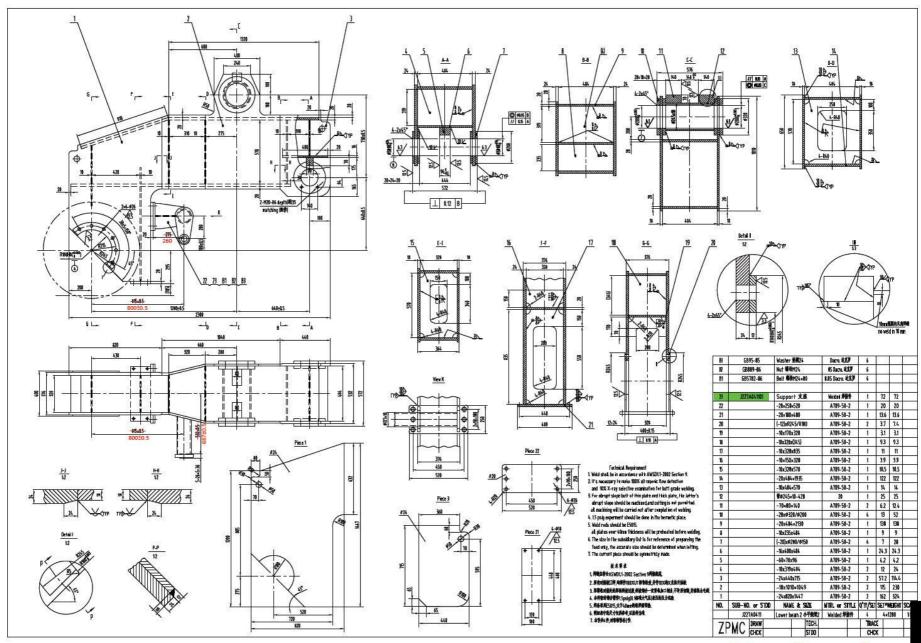
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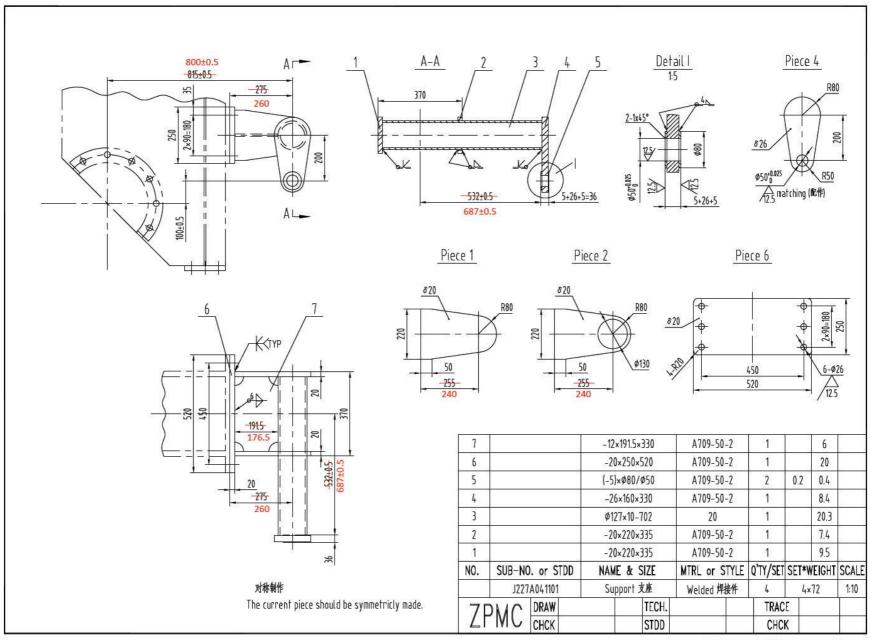


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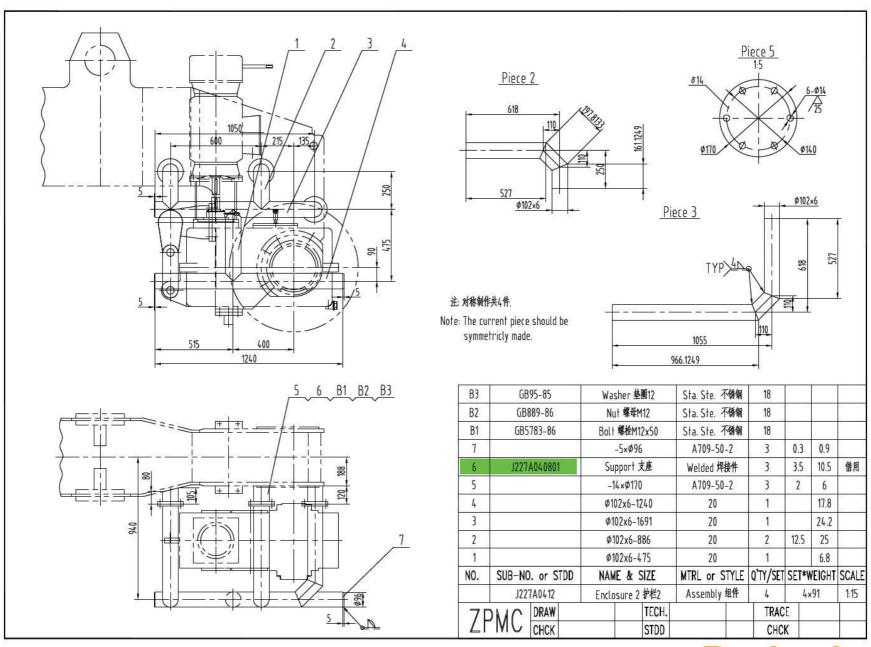
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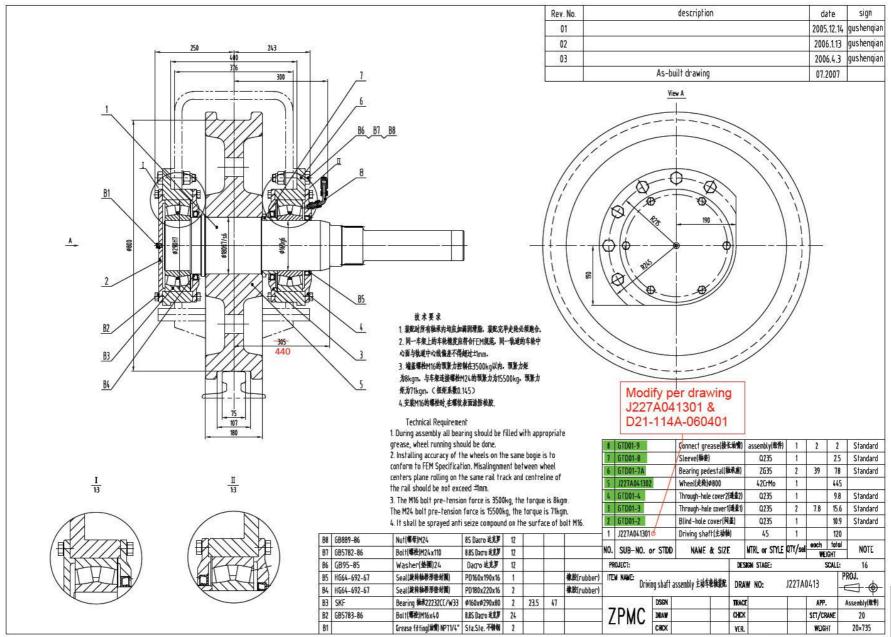


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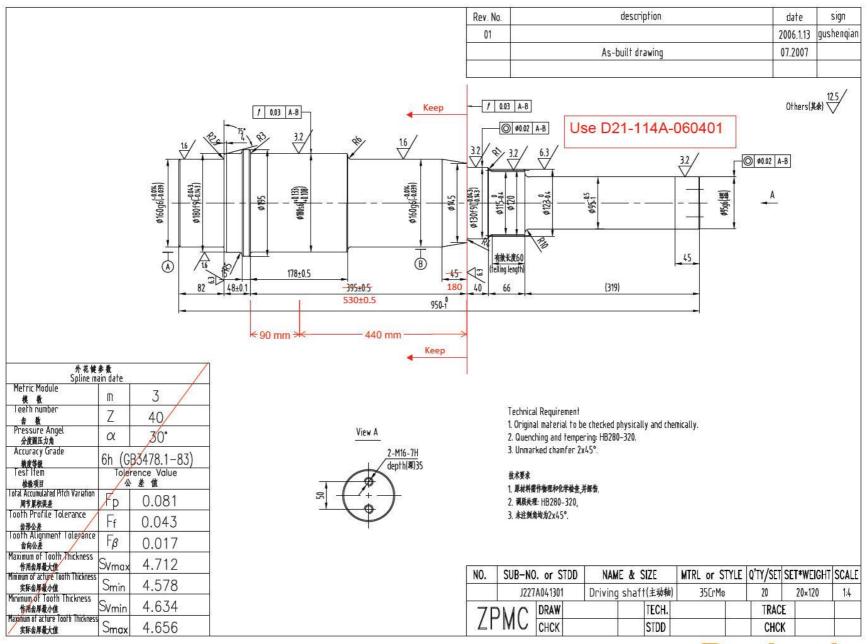


\*Note - ZPMC Engineering to verify dimensions, component updates, and comments in red.



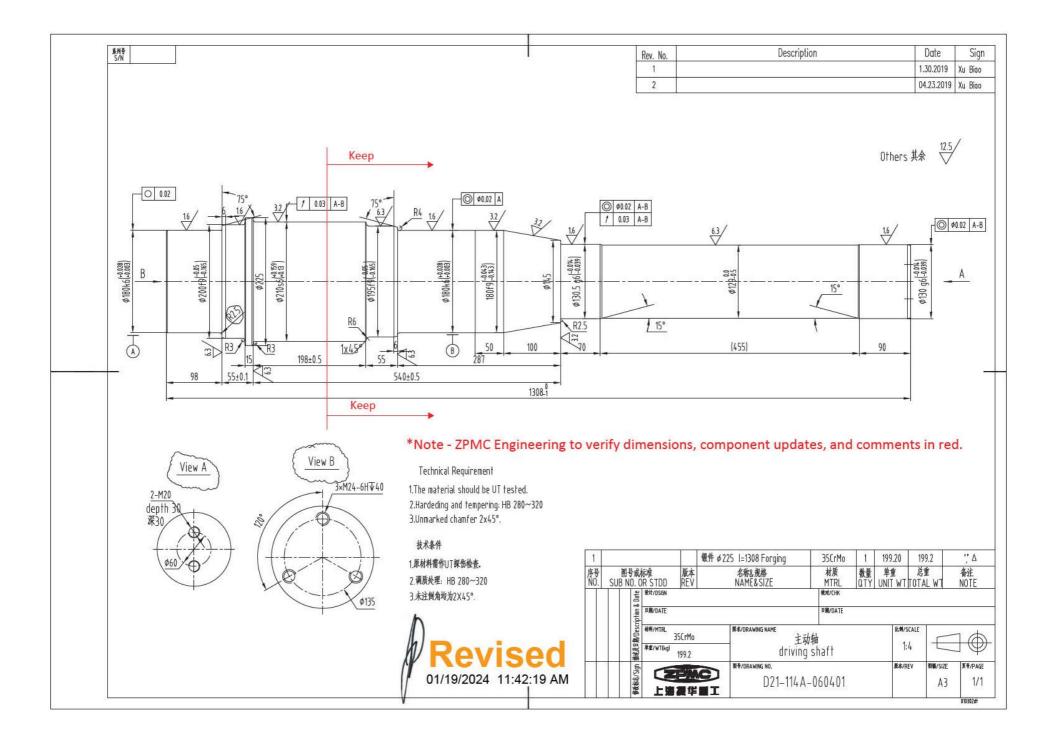


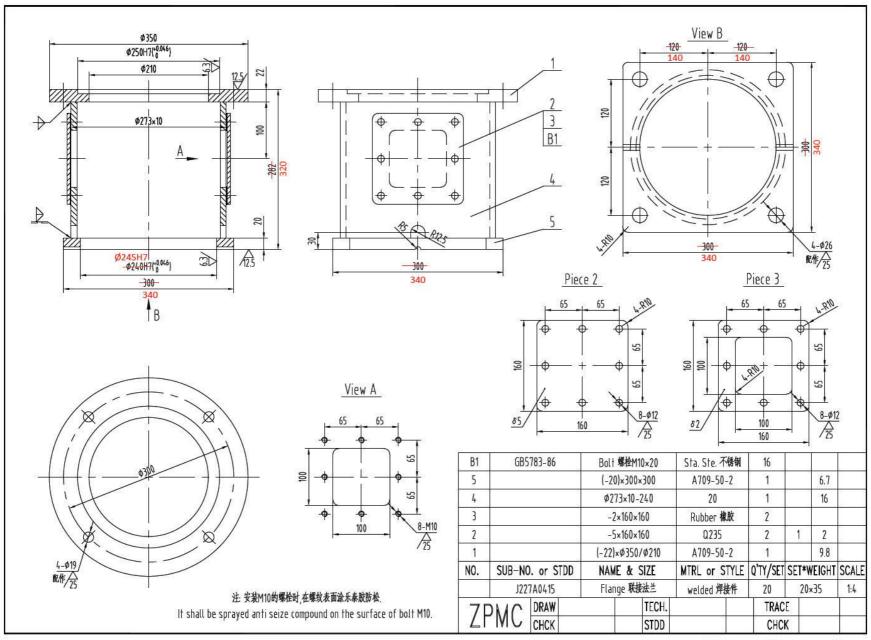
 $\hbox{*Note-ZPMC Engineering to verify dimensions, component updates, and comments in red.}$ 



<sup>\*</sup>Note - ZPMC Engineering to verify dimensions, component updates, and comments in red.

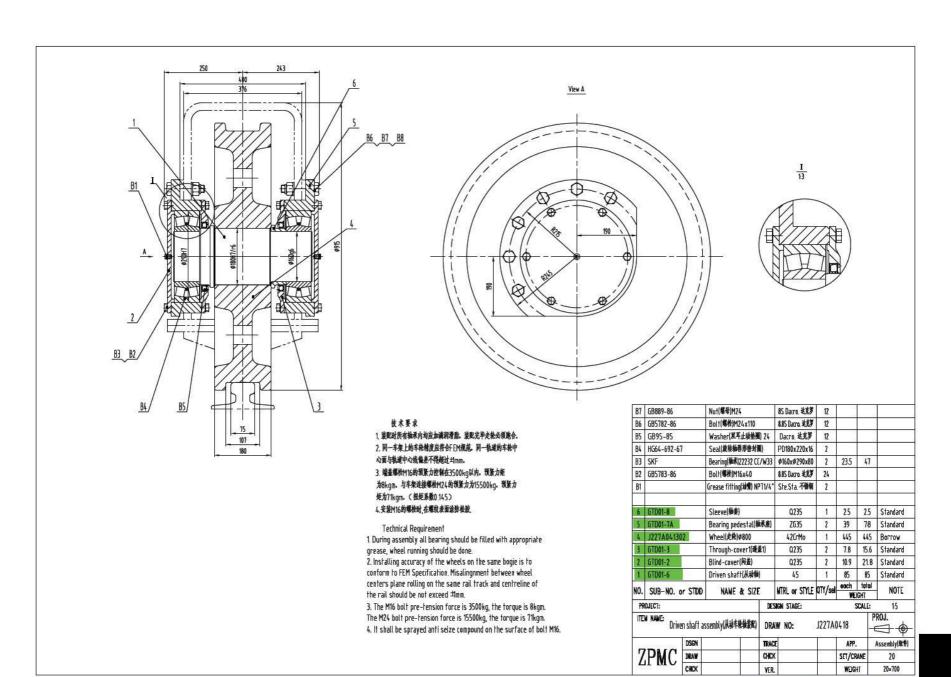




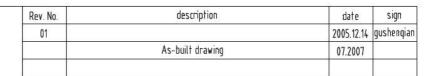


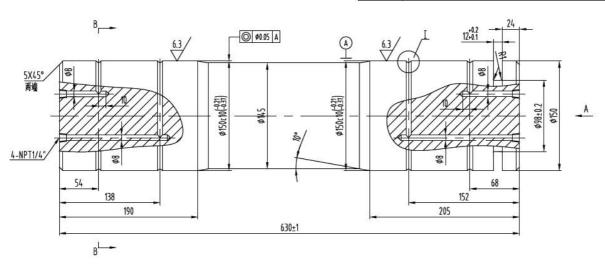
\*Note - ZPMC Engineering to verify dimensions, component updates, and comments in red.



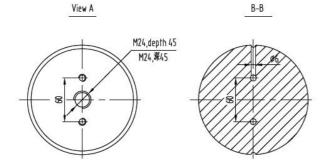


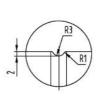






Others(其余)





Technical Requirement

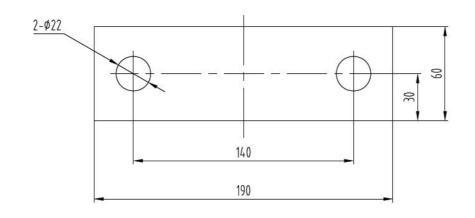
- 1. Quenching and tempering: HB280~320. 2. Original material to be checked physically and chemically.

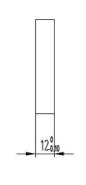
### 技术要求

- 1. 调质: HB280~320.
- 2. 原材料需作物理和化学检查,并探伤.

NO.	SUB-NO	or STDD	NAME & SIZ	E MTRL or S	STYLE Q'TY/SET	SET*WEIGHT	SCALE
	J22	7A0419	Shaft(轴)ø15	0 35CrMc	16	16×85	1:3
71	OMC	DRAW	TI	ECH.	TRAC	Ε	
ЬΓ		СНСК	S	TDD	CHC	K	

All(全部) 25

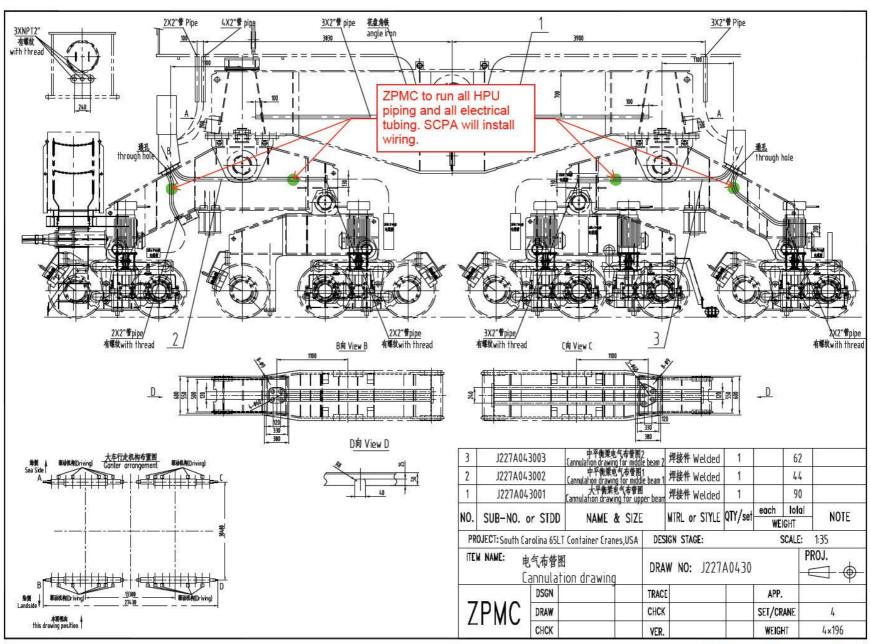


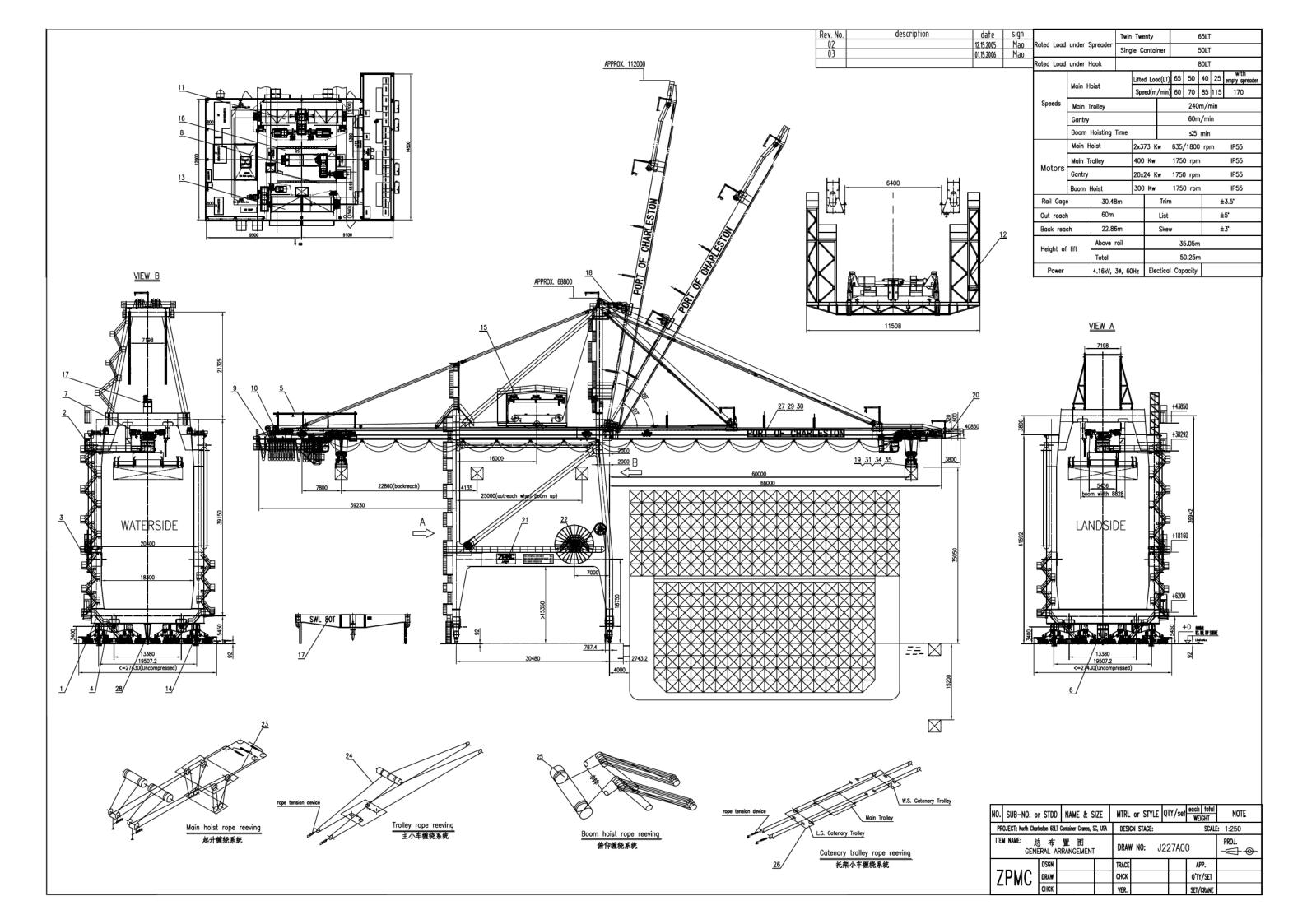


Breaking sharp cornser 注:棱边倒角1X45°.

NO.	SUB-NO	or S	TDD	NAM	E & S	SIZE	MTRL	or S	TYLE	Q'TY/SET	SET*WEIGHT	SCALE
	J22	7A0420		Shaft e	nd plat	e(卡轴板)		Q235		16	16×1.1	1:2
70		DRAW	,		3	TECH.	9			TRAC	E	
$\angle \Gamma$		CHCK	A.		3	STDD	9			CHCI	(	







# SUBSIDIARY LIST

	Ē		set/cran			<u> ку</u> /	SEI,_	SUB-PAR				PAGE:	1/2 SUB DRAW NO			
		North (	PROJECT NAME  Charleston 6	or CODE: SSLT Conf	ainer	Cranes	ENED									
	ŀ	NO.	SUB-NO. or				E & SIZE	<u> </u>	11//	MTRL or STY		Q'TY/SET	PIECE WGHT	TOTAL W	 GHT	
•	۱	1	J227A	0100	钅					Structu	re	1				
:	2	2	J227A	0200		电梯				Manlift arrar		1				
3	,	3	J227A	0300	7	梯子,走	道月	r 台		Stairs , Platforms	•	1 4				
	۱,	4	J227A	0400	-	大车行				Gantry	a waniwaya	4				
	,	5	J227A	0500	13.1	室外维	修行	 车		Outdoors mainte	nance lift	1				
-	,	6	J227A	0600	F	<b></b>	定及	理货室	<i>_</i>	Landside anchortcl		1				
7	, [	7	J227A	0700	-	主小车	总成			Trolley arrar		1				
8	,	8	J227A	0800		主小车	驱动	机构		Trolley Dri	•	1				
9	,	9	J227A	0900	1	电缆托	令系统	 统		Festoon S		1				
_ <sub>1</sub>	۰	10	J227A	1000	ß	方挂舱	装置			Snag	,	1				
1	1	11	J227A	1100	-	主起升	机构			Main Hois	t Drive	1				
1	2	12	J227A	1200		大梁维	修平	台		Service Pl		1				
1	3	13	J227A	1300	1	俯仰机	构			Boom hois		1				
- 1	4	14	J227A	1400	ŀ	<b>防风拉</b>	索装	置		Tie down :		1 4				
1	5	15	J227A	1500	;	机器房	•			Machinery	•	۱ ،				
1	6	16	J227A	1502		换绳装				Rereeving		۱ ،				
1	, [	17	J227A	1600		30LT吊		—— 発		Cargo Bea	•	2/4				
1	8	18	J227A	1700	-	安全钩				Boom Lat		1				
1	9	19	J227A	1800		7月上				Headblock		1				
2	20	20	J227A	1900	3	头部倾	转装员	置		Trim.list &ske		1				
2	21	21	J227A2	2000	4	路牌布	置			Nameplate ar		1			_	
2	22	22	J227A2	2100	-	大车电	缆卷	 筒		HV cable reel	•	1				
		7 [		DSGN				TECH		04510 1001	207100	MTRL			_	
		$\angle \vdash$	PMC	CHCK				STDD				СНСК				

# SUBSIDIARY LIST

\* The quantity and weight of this list is to one set

\_\_\_\_\_ set/crane, \_\_\_\_\_ kg/set, \_\_\_\_\_ kg/crane kg/crane PAGE: 2/2

	<u></u>	set/crane,	<u> </u>		_ K	g / set, _			_ kg/cro	ine	PAUE:	2/2	
	North	PROJECT NAME or ( Charleston 65L		lginer Cr	gnes		SUB-PAR 总布置	图				SUB DRAW NO	
						GENER	AL AR	RAI	NGEMENT		OITY (CET	Ι	
	NO.	SUB-NO. or STI		+		AME & SIZE 上编线 3	《公		MTRL or STYL		1	PIECE WGHT	TOTAL WGHT
1	<u> </u>	J227A22		-+		十缠绕系			Main hoist Rope	Reeving			1
2	24					车缠绕系			Main trolley rope	reeving			
3		J227A24		+		連绕系統		<u></u>	Boom hoist rope	•			<u> </u>
4		J227A25		1.1	-	小车缠织		允	Catenary trolley	rope ree	ving 1		
5	27	J227A26	<u>600</u>		-	限位布5	直		Limit sw	itch_	1		
6	28	J227A27	700			锚定			Seaside A	<u>nchor</u>	1		
7	29	J227A28	800			系统			<u>Lubrication</u> s	<u>system</u>	1		
8	30	J227A29	900		(压	机系统			Air compress	or syst	<sub>em</sub> 1		
9	31	J227A30	00C	Ì	重.	<u>水箱</u>			Test Tank		2/4		
10	32	J227A31	100	係	F仰:	室			Boom operate	station	1		
11	33	J227AH	-	液	压.	系统			Hydraulic s	system	1		
12	34	J227AE	=	电	气	系统			Electrical sy	stem	1		
13	35			R	ΑM	吊具			RAM Spread		1		
14	36			R	AM	超高效	Ę		Overheight Sp		1/4		
15									J		•		
16													
17													
18													
19													
20													
21													
22													
	<u> </u>		SGN				TECH				MTRL		
	ZF	JM( ⊢	HCK				STDD				СНСК		