National Transportation Safety Board

Office of Railroad, Pipeline and Hazardous Materials Washington, DC 20594



RRD23LR008 – ANNISTON, ALABAMA

MECHANICAL

Group Chair's Factual Report April 21, 2023

TABLE OF CONTENTS

Α.	ACC	CIDENT	,
Β.	MEC	CHANICAL GROUP	,
C.	SUM	1MARY	,
D.	FAC	TUAL INFORMATION	;
	1.0	Train Consist	;
	1.1	Locomotive Consist	F
	1.2	Car Consist	,
	2.0	Pre-departure Inspections and Tests	,
	2.1	In-Tow Locomotive Inspection)
	2.2	NS Communications Regarding ME-9258	;
	2.3	Train pre-departure Tests)
	3.0	Accident Sequence	•
	4.0	Post-accident Inspections and Tests	,
	4.1	Locomotive Couplers17	,
	4.2	Locomotive Wheel Profiles23	;
	4.3	TBOGI Data	,
	4.4	Locomotive Bolster Stop Blocks40)
	4.5	In Train Forces	•
	4.6	Coupler Angle Calculations44	F
	4.7	Rolling Radius Differential44	F
	4.8	Mechanical Condition48)
E.	DOC	CUMENTS REVIEWED)

A. ACCIDENT

Location:	Anniston, Alabama
Date:	March 9, 2023
Time:	0619 (Local)

Train: 245A109

B. MECHANICAL GROUP

Group Chair	John Manutes National Transportation Safety Board Denver, Colorado
Group Member	Lamont Hay Federal Railroad Administration Birmingham, Alabama
Group Member	Kevin Krull Norfolk Southern Railway Atlanta, Georgia
Group Member	Eric Shapach Norfolk Southern Railway Atlanta, Georgia
Group Member	Eddie Nix Alabama Public Service Commission Gardendale, Alabama

C. SUMMARY

For a summary of this accident, please see the Investigator-In-Charge (IIC) Synopsis in the docket for this investigation.

D. FACTUAL INFORMATION

1.0 Train Consist

Norfolk Southern Train No. 245A019 departed Atlanta, Georgia bound for Birmingham, Alabama with six locomotives and 108 railcars. No pickups or setouts were conducted while enroute prior to the accident. The train was 9,795 feet long and weighed 10,262 tons.

1.1 Locomotive Consist

All 6 locomotives were located at the front of the train. There were no midtrain or rear-end distributed power units (DPU). The first locomotive, UP 5574, was on-line and occupied by the two-person operating crew, located in their normal positions at the time of the accident. Prior to departure from Atlanta, the operating crew determined the second locomotive, UP 9039, had inoperative dynamic brakes. Therefore, this locomotive was placed in isolated status. While isolated, it could not produce tractive effort and dynamic braking. The pneumatic brakes operated normally and responded to control inputs from the front locomotive. The third locomotive, NS 4408, was in the process of undergoing periodic maintenance for the first time in calendar year 2023. The majority of the work was completed in Atlanta but was being moved to Birmingham for wheel truing.¹ The wheels did not have Federal defective conditions, they were scheduled to be trued as regular maintenance. Because the locomotive maintenance was not yet fully complete, the NS mechanical department did not place a current FRA Form F6180.49A (Blue Card) in the cab. There was a daily inspection card in the cab, but it contained no entries. The mechanical department did not place an out-of-service tag in the locomotive cab.

Prior to departure, the crew of the train noted inoperative dynamic brakes on the second locomotive. They placed the third locomotive on-line for tractive effort and dynamic braking and did not notice any concerns. The fourth locomotive was undergoing similar maintenance to the third locomotive and was therefore isolated. The fifth and sixth locomotives, RMEX 08 and RMEX 06, were "dead-in-tow" as revenue "waybilled" locomotives. Similar to the isolated status, the tractive effort was not available. Pneumatic braking functioned similar to a boxcar, the engineer could activate the automatic brake, but the independent brake was cut out. The cabs were locked to prevent access. The NS was moving these locomotives for a customer, Reliance Rail, from Bluffton, Indiana to Mobile, Alabama where they were to be placed on an ocean vessel for shipment to an overseas customer. The NS had moved RMEX 08 and RMEX 06 on four previous trains prior to placement in the accident train.

¹ Wheel truing consists of cutting the wheel on a lathe to obtain the proper wheel profile.

Road Number	Туре	Status	Coupler Type
UP 5574	C44ACCTE	Online	Front: F8513AE Rear: BF10AE
UP 9039	SD70AH	Isolated	Front: BF10AE Rear: F8513AE
NS 4408	AC44C6M	Online	Front: E8311E Rear:E8311E
NS 9485	D9-40CW	Isolated	Front: 8311E Rear: E8311E
RMEX 08	GP11	Dead-in-tow	Front: E4881E Rear: E7304
RMEX 06	GP10	Dead-in-tow	Front: E8305E Rear: E8305E

1.2 Car Consist

The train was comprised of 108 mixed-freight cars included four cars placarded "Class 8 (Corrosive Material) Dangerous", one general hazardous, and one "Class 3 (Flammable Liquid) Dangerous". Some of the cars in the train were articulated intermodal cars. NS identifies these cars as a single car. For the purposes of factually identifying the weight distribution of the train, the NS created a chart (marked "draft" below for investigation purposes) which breaks out each "well" or unit of these articulated cars. The ends of freight cars are designed to transfer the longitudinal loads of in-train forces, switching, and coupling through the ends of the cars where the couplers themselves connect to the car body through a draft pocket assembly. To manage these large forces without damaging equipment or lading, North American freight cars generally have either a standard draft gear, made up of resilient blocks or cast wedges, or a hydraulic end of car cushioning unit (EOCC). Draft gear systems have approximately 6.5-inches of travel over which the forces are absorbed in each device. EOCC systems absorb forces through hydraulic pistons in various ranges, generally about 15-inches per device. In the chart below, cars equipped with standard draft gear are indicated with blue bars, and cars with EOCC are indicated with yellow bars.



Figure 1. Tonnage profile for the accident train.

2.0 Pre-departure Inspections and Tests

2.1 In-Tow Locomotive Inspection

An NS mechanical employee conducted an inspection of RMEX 08 and 06 in Bluffton, IN. The employee filled out form "ME-925: In Tow Unit Inspection Form" which states, "Instructions in LDI 1-21, see LDI for further Instructions". On these forms, there are a number of inspection items. The line for "Is unit equipped with alignment control draft gear?" was checked "yes". The next line for "*if NO to above, stop blocks must be applied. Are stop blocks applied?" was also checked "Yes". The area for "Inspecting Mechanical Officers recommendations: type of service, location to be placed in train, suggested speed, and/or any added restrictions:" was left blank.



Figure 2. ME-925 for RMEX 06



Figure 3. Form ME-925 for locomotive RMEX 08

On April 4, 2023, FRA inspectors from the Mechanical Working Group interviewed the NS Electrician who performed the ME-925 inspections on RMEX 06 and RMEX 08. The Electrician stated he had worked at NS for 11-years and had performed one previous ME-925 inspection in late 2022. In an interview with FRA inspectors, he stated he performed the inspection alone and did not receive prior training. He stated that at the time of the inspection he did not know what an alignment control coupler was. He was allowed as much time as needed to conduct the inspections, and due to weather and operational issues, took two days to complete them over several hours each day.

2.2 NS Communications Regarding ME-925

Between January 11, 2023, and February 23, 2023, NS arranged the inspection, waybilling, and movement of locomotives RMEX 06 and RMEX 08 through email communications. On January 18, mechanical department employees

submitted the inspection form to the NS Clearance desk, who approved the movement of the locomotive via email shortly thereafter.

On February 2, 2023, NS mechanical employees submitted the inspection form for RMEX 08 to the NS Clearance desk. In subsequent emails that same day, there was a discussion related to the boxes marked "yes" for alignment control couplers and stop blocks.

Waybills for both locomotives were distributed on February 23, 2023. In the body of the email containing the waybills, the following three statements were included:

Unit(s) is/are reported to have **4** axles, roller bearings, and are equipped with alignment control draft gear.

*** non alignment draft control gear in place - move per NS1 L214 & L231

Per Tariff NS 8002-A Item 6275, Dead in Tow units not equipped with alignment control draft gear will move in Special Train Only.

Later that day, NS officials asked if the electrician who conducted the inspection had verified the presence of alignment control couplers. It was stated that "The electrician said the unit has stop blocks", and the movement was approved.

2.3 Train pre-departure Tests

Prior to the train's departure a Class I air brake test and pre-departure inspection was performed in two portions on March 8th and 9th in Atlanta by qualified mechanical inspectors.

	REPORT OF SATISFACTOR	ORY CLASS 1 BRAKE TEST (A6)	PERFORMED
BRAKE TEST TRAIN LOCATION ABOVE TRAIN WA TERMINAL INSPE	NO. CARS 148H AS INSPECTED AND FOUND CTION) OF THE DEPARTMENT	35 DATE 3/8 23 LEAKAGE 31 EOTD	TIME A
	NAME OF PERSON RE	PORTING Si	MAS .
EOTD TEST:	EOTD NO	(If not same as no	ted above, show number)
DATE	TIME	LOCATION	and the second
ABOVE EOTD WAS END-OF-TRAIN DEV	TESTED AND FOUND TO B	E IN COMPLIANCE WITH CFR 49 PA NT OF TRANSPORTATION'S POWER	RT 232 (INSPECTION AND TESTING O R BRAKE REQUIREMENTS.

Figure 4. Class I air brake record for a portion of the accident train

RF	EPORT OF SATISFA CTOR	
	REPORT OF SATISFACTORY CLASS	1 BRAKE TEST (A6) PERFORMED EOTD TEST PERFORMED
BRAKE TEST:		
TRAIN	15 NO. CARS 74 D	ATE 3/9 TIME 1:24
LOCATION	1484 LEAKAGE	216 FOTD NO 75714
	NAME OF PERSON REPORTING	Sims
	Paul Company and	a strain and an an an an an an an
EOTD TEST:	EOTD NO. 75714	 (If not same as noted above, show number)
EOTD TEST: DATE 3/9	EOTD NO. 75714 	- (If not same as noted above, show number) LOCATION14どに
EOTD TEST: DATE <u>3/9</u> ABOVE EOTD WAS END-OF-TRAIN DEV	EOTD NO. 75714 TIME 1:55 A TESTED AND FOUND TO BE IN COMPL VICES) OF THE DEPARTMENT OF TRAN	- (If not same as noted above, show number) _ LOCATION

Figure 5. Class I air brake record for a portion of the accident train

In addition to the FRA required inspections and tests, NS uses a Gold Card inspection process. The Gold Card process is outlined in NS Standard Work Instruction ME-114 with the most current revision dated June 3, 2022. NS Rule Number L-202, Taking Charge of Locomotives states, "When a locomotive consist is received from a mechanical facility, the presence of a current and properly completed form ME-114 (Gold Card) will indicate that the required tests and inspections have been successfully completed.

	FORMME-74 (SEV 04/08/2020)	
	Train Symbol: Location: Date:/	
9	Loco Consist: AF 22/2 4/ 10/1 4/408 24/2 AREA AREA ENLY 6	
ion in	Fuel Readings:	
D Pled	The following have been checked on this consist per applicable NS-1 rules (reference graphic for work path):	
S in G	1. Confirmed calendar day inspection is completed and signed	
N day	2. Locomotives properly equipped with tools, supplies, ice, and water	
Der ndal	3. Verified the following LCDI items: Toilet, Sand, MU Hoses/Cables, Head/Ditch Lights, Bell, Horn, Air Brake, and Alerter	
nge	4. Radio & HOTD tested - If prelinked, EOTD ID#:	
NSI ext of	😤 😘 . Completed: 🗆 PTC Departure Test (<i>as required</i>) 🔲 Ceb Signal Departure Test (<i>where required</i>) 🗔 Bidirectional Loading 🗖 Dynamic Brake Test	
til n	6. DP consist: 🗆 Yes 🗆 No. Units pre-linked per SW-L-0300: 🗀 Yes 🛛 Linked DP units:	
Si Si	C 7. Checked ATC equipment for seals	
valio or a	8. Completed Form ME-615 for defective locomotives being towed (<i>if applicable</i>)	
4 C	9. Locomotives set up properly per NS-1 L-213	
En la	10. Cleaned and sanitized per department instructions	
Ч. М.	11. Left a copy of Gold Card and DP Quick Reference (<i>if applicable</i>) in the cab of the lead locomotive	
	Name of person(s) inspecting:	

Figure 6. Form ME-114 (Gold Card) From accident train.

3.0 Accident Sequence

Between East End District Milepost 719 and 720, Train No. 245A109 was traveling on a track that undulated between ascending and descending grade, then began a downhill grade of 1.29-percent. The train was in the process of traversing multiple curves simultaneously. Maximum authorized speed in this area is 35 MPH.

At MP 721.05 the track profile is briefly tangent between a left-hand and righthand curve. Witness marks indicate that at this point, the south rail experienced a catestrophic lateral force to the south and subsequent rail rollover/gage rupture event. The head of the rail had witness marks consistent with the suspension hanger from a locomotive riding on the rail for approximately 29 feet. Following this mark, wheel flange impact marks from north-rail wheels were found inside the gage on the ties.

The witness marks found on the track structure matched witness marks found on locomotive RMEX 06. Specifically, the R3 wheel had outside wheel plate/rim scoring and damage. The right-rear (south in the direction of travel) suspension hanger had witness marks from the rail. The witness marks are consistent with the R3 wheel of RMEX 06 being the first wheel to derail in a gage widening/ rail roll over event.



Figure 7. East End Derailment Overview

Train 245A109 West End Facing East 13. SDWX 9802 14. SDWX 9721 15. CEMX 1481 16. BKTY 151297 17. BKTY 150433 18. TBOX 662485 19. CR 56202 20. NS 195032 21. LRS 2135 22. DJNX 42025 23. BBFX 425 24. MWCX 204356 25. CAIX 316274 26. NDYX 839017 27. AEX 24993 28. FLOX 79212 29. NS 163534 30. UTLX 641472 31. CRDX 20766 32. CEFX 86083 33. CRYX 5269 34. COER 804792 35. COER 804785 36. COER 804804 37. CRYX 5269



Figure 8. East End Derailment Overview



Figure 9. West End Derailment Overview



Figure 10. Wheel and wheel tread departure mark near MP 721.05.



Figure 11. RMEX 06 R3 Wheel with rail burn witness marks.



Figure 12. RMEX 06 rear right hanger with rail burn witness marks.



Figure 13. Cars at rest (post-derailment) near MP 721.05 with jackknifed couplers

4.0 Post-accident Inspections and Tests

4.1 Locomotive Couplers

Modern locomotives, like the first four in this consist, are equipped with alignment control couplers.² Alignment control couplers are cast with 'shoulders' at the rear of the drawbar portion of the coupler and plungers designed to engage with the wings and draft gear when the train experiences compressive, or buff, forces (See Figure 14). Through the activation of the draft gear, the plungers provide a centering torque to the coupler.

² Alignment control couplers, installed on most locomotives, will allow only limited lateral movement when longitudinal in-train forces are compressed or in buff. This reduces lateral forces on the track, transformed from longitudinal forces, and therefore reduces the possibility of derailment. Manufacturers' specifications indicate that alignment control couplers, under buff conditions, can limit the draw bar angle to eight degrees, while the non-alignment control couplers permit a draw bar angle as large as 19 degrees, creating increased coupler offsets between locomotives and cars.



Figure 14. Alignment control coupler with plungers



Figure 15. A Wabtec SBE8301E Coupler with alignment control.

Locomotives used extensively in switching service in areas with tight track curvature, similar to RMEX 08 and RMEX 06, may be equipped with non-alignment control couplers. These couplers lack the wings and are not equipped with the draft gear engaging plungers. The coupler head is free to rotate to larger degrees of freedom without resistance, even when the train is in buff. Norfolk Southern representatives on scene noted that NS maintains approximately 2,600 locomotives and only three of those locomotives are equipped with non-alignment control couplers. These shop switchers are used in a select few locomotive maintenance shop areas where track curvature necessitates their use to move other locomotives around the facility. NS locomotives not equipped with alignment control couplers have a large white stripe painted under the locomotive reporting marks (numbers) for rapid identification. The RMEX 06 and 08 were not owned by NS, therefore they did not have the white stripe identification marking.



Figure 16. Coupler without alignment control.



Figure 17. NS 2103 with non-alignment control coupler identification stripe

Railroads sometimes place a removable alignment block between the front of the coupler pocket and the coupler to limit the full rotation of the coupler. RMEX 08 and 06 were equipped with these alignment blocks prior to departure from Bluffton. The application of stop blocks does not serve the same effect as an alignment control

MECHANICAL GROUP CHAIR'S FACTUAL REPORT coupler. The blocks resist rotation of the coupler, but they do not apply rotational pressure from the draft gear and provide positive rotational torque in the same way modern alignment control couplers do.



Figure 18. RMEX 08 non-alignment control coupler alignment block

Locomotives RMEX 06 and RMEX 08 were equipped with non-alignment control couplers. The draft pocket of RMEX 08 was bulged out on the left rear side. The rust, wear, and moss found inside the broken weld are consistent with 'old' break. The coupler stop block of RMEX 06 was missing at the right rear location. The bracket that held the rubber stop in place had fracture features consistent with fracture in overstress from outward bending. The facture surface was relatively flat with the exception of an upward facing shear lip toward the right, outer corner, and a depression with sharp corners on the left. The fracture was rough, with a uniform surface luster. The surface oxide was a light maroon or rust color, consistent with post-fracture oxidation from exposure to humidity or water. (Post-accident, there was significant rainfall in the area) There were no indications of localized areas of discoloration or geometries that would indicate a pre-existing crack. Investigators contacted the Pennsy company via email to ask about the proper installation of coupler stop blocks. In the email, the Pennsy company stated that they have never seen the blocks welded to the coupler carrier in this manner. That was an incorrect application. The coupler alignment blocks are shipped assembled with the securement chain bolted to the ends of the vertical tabs, which indicates the correct method of application.



Figure 19. Draft gear pocket of RMEX 08, left rear location



Figure 20. RMEX 06 Pennsy coupler alignment block, improperly secured with weld.



Figure 21. Pennsy stop block. The bolts and chain are for securement purposes. (Pennsy marketing image)³

³ <u>https://pennsy.com/product/locomotive-coupler-alignment-block/</u>



Figure 22. Draft gear pocket of RMEX 06 left rear location, showing broken coupler stop bracket.

4.2 Locomotive Wheel Profiles

Locomotive RMEX 08 had flanges over 1.5-inches at the following locations. Wheel R2, flange height 1.553 inches. Wheel R4, flange height 1.539 inches. Wheel L4, 1.588 inches. High flanges over 1.5-inches are FRA non-compliant conditions.⁴

⁴ 49 CFR Section 229.75(h) - Wheels and tire defects

Wheel numbers R3 and R2 had a distinctive, non-standard, flange root shape.⁵ The shape of the flange root is consistent with non-standard wheel lathe procedures, and not normal wear from wheel/rail contact.



Figure 23. Exemplar Worn (red) and unworn (blue) wheel profiles with an exemplar rail profile (green).⁶

⁵ The flange root is the radius between the tread of the wheel and the flange of the wheel.

⁶ https://www.globalrailwayreview.com/article/2222/shape-optimisation-of-a-railway-wheel-profile/



Figure 24. RMEX 08 L1 Wheel profile (Red) and new wheel profile (Blue)



Figure 25. RMEX 08 R1 Wheel profile(Red) and new wheel profile (Blue)



MECHANICAL GROUP CHAIR'S FACTUAL REPORT





Figure 28. RMEX 08 L3 Wheel profile(Red) and new wheel profile (Blue)



Figure 29. RMEX 08 R3 Wheel profile(Red) and new wheel profile (Blue)



Figure 30. RMEX 08 L4 Wheel profile(Red) and new wheel profile (Blue)



MECHANICAL GROUP CHAIR'S FACTUAL REPORT

			×	RM	EX &							- 2	a					
Г				LEE	SIDE		1.841				RIGH	SIDE				REA	SON	DESCRIPTION
ł	Pos.	R	im		Flar	nge			R	im	NIGHT	Fla	ange		SHIM	СН		CHAMFER
ł		Thic	kness	He	right	Thic	kness	100	Thic	kness	Hei	ght	Thic	kness	FG	FS		FLAT SPOT
	1	-	16		16		16			16		16		16		HF		HIGH FLANGE
•	2	1	15	1	7	1	3		1	15	1	C	1	6		HT		HIGH THIN FLANG
ŀ		-	16	/	16	1	16	100		16	-	116		16		MM		MISMATCHED
ŀ	3	1	16		16	-	16	1		16		16		16		ST		SHELLED TREAD
•	4	2	0	1	(°	1	5		1	15	1	C		3		TC		TRUCK CHANGE
ŀ	5			/	10	-	10		-	10	-	10		10		TM		TRACTION MOTOR
ŀ	-	-	16		16		16			16		16		16		П		THIN TREAD
L	6		16		16		16			16		16	1	16		wc		WHEEL CHANGE
,	Wheel	s mea	sured	by:													_	
						122		3					Min	Co	31 - 1	leight	H	Pilot Height
	Coupl	er mea	asured	by:									Front			-	F	
	Coupl	er mea	asured	by:									Front Rear			-	F	
	Couple Pilot n RECC	er mea neasu)RD N	red by:	by:	REME	NTS, F	PUT A	"C'	OR	"T" AF	TER	RUIN	Front Rear Max.	D CH/	34 - 1/	2" DUT :		6"
	Coupl Pilot n RECC (R = Re	er mea neasu ORD N egage,	red by: IEW M C = Cha	by: EASU	REMEI = Turn)	NTS, F	PUT A	."C'	'OR	"T" AF	TER	RUIN	Front Rear Max.	D CH/	34 - 1/ ANGE R C T	2" OUT : SHIM RSN FG		6" EMPLOYEE
	Couple Pilot n RECC (R = Re	er mea neasu ORD N egage,	red by: EW M C = Cha	by: EASU ange, T	REMEI = Turn)	NTS, F	PUT A	."C'	" OR	"T" AF	TER	RUIN	Front Rear Max.	D CHA	34 - 1/ ANGE R C T	2" OUT : SHIM RSN FG		6" EMPLOYEE
Ę	Pilot n RECO (R = Re	er mea neasu PRD N egage,	red by: EW M C = Cha	by:	REME! = Turn)	NTS, F	PUT A	."C'	" OR	"T" AF	TER	RUIN	Front Rear Max.	D CHA	34 - 1/ ANGE C T	2" DUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECO (R = Re	er mea neasu ORD N gage,	red by: EW M C = Chi 16	by:	REMEI = Turn) 16 16	NTS, F	PUT A	."C'	" OR "	"T" AF	TER	16 16	Front Rear Max.	D CHA	34 - 1/ ANGE R C T	2" OUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECO (R = Re 1 2 3	er mea neasu ORD N ogage,	red by: EW M C = Cha 16 16	EASU	REME! = Turn) 16 16 16	NTS, F	PUT A	."C'	" OR "	"T" AF	TER	16 16	Front Rear Max.	D CH4	34 - 1/ NGE C T	2" DUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECO (R = Re 1 2 3 4	er mea neasu DRD N gage,	red by: EW M C = Chi 16 16	by:	REME = Turn) 16 16 16	NTS, F	PUT A		" OR "	"T" AF	TER	16 16 16	Front Rear Max.	D CHA	34 - 1/ ANGE R C T	2" DUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECC (R = Re 1 2 3 4 5	er measur DRD N gage,	red by: EW M C = Cha 16 16 16	EASU	REMEI = Turn) 16 16 16	NTS, F	PUT A	."C'	" OR '	"T" AF	TER	16 16 16	Front Rear Max.	16 16 16 16	34 - 1/ ANGE R C T	2" OUT : SHIM RSN FG		6" EMPLOYEE
	Couple Pilot n RECCO R = Re 1 2 3 4 5	er mea neasui DRD N lgage,	red by: EW M C = Cha 16 16 16 16	by:	REMEI = Turn) 16 16 16 16 16	NTS, F	PUT A	"C'	" OR '	"T" AF	TER	RUIN	Front Rear Max.	16 16 16 16 16	34 - 1/ NNGEC R C T	2" DUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECCO (R = Re 1 2 3 4 5 6	er mea neasu PRD N ngage,	red by: EW M C = Chi 16 16 16 16	EASU	REME = Turn) 16 16 16 16 16 16	NTS, F	PUT A	."C'	" OR	"T" AF	TER	RUIN 16 16 16 16 16	IG AN	16 16 16 16 16	34 - 1/ ANGEA C T	2" OUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECO R = Re 1 2 3 4 5 6	er med neasur DRD N ngage,	red by: EW M C = Chi 16 16 16 16	by:	REMEI = Turn) 16 16 16 16 16 16	NTS, F	PUT A		" OR "	"T" AF	TER	RUIN	Front Rear Max.	16 16 16 16 16 16	34 - 1/ ANGEC R C T	2" DUT : SHIM RSN FG		6" EMPLOYEE
	Pilot n RECCO (R = Re 1 2 3 4 5 6	er mea neasun PRD N ngage,	red by: EW M C = Ch 16 16 16 16 16	by:	REMEI = Turn) 16 16 16 16 16 16 16	LEFT RIGHT	PUT A 16 16 16 16 16 16 16 16 16 16	-"C'	" OR	"T" AF	TER	RUIN 16 16 16 16 16 16	IG AN	16 16 16 16 16 16 16	34 - 1/ NAGEE C T	2" OUT : SHIM RSN FG	ent	6" EMPLOYEE
	Pilot n RECO R = Re 1 2 3 4 5 6	er mea neasu DRD N ngage,	EW M C = Chi 16 16 16 16 16	by:	REMEI = Turn) 16 16 16 16 16 16 16 16	NTS, F	PUT A 16 16 16 16 16 16 16 16 16 16	"C'	* OR	"T" AF	TER	RUIN	Front Rear Max. IG AN	16 16 16 16 16 16 16 16	34 - 1/ ANGE(R C T	2" DUT : SHIM RSN FG	ent	6" EMPLOYEE
	Pilot n RECO R = Re 1 2 3 4 5 6	er mea neasur DRD N ggage, insitior	red by: EW M C = Chi 16 16 16 16 16	by:	REMEI = Turn) 16 16 16 16 16 16 16 ator	NTS, F	PUT A 16 16 16 16 16 16 16 16 16 17 1 2 7 1 2	-"C"	* OR +	"T" AF		RUIN	m to wi	16 16 16 16 16 16 16 16 16 20 20 20 20 20 20 20 20 20 20 20 20 20	34 - 1/ ANGEC R C T T J J J T O O V E U D I T O O V E	2" DUT : SHIM RSN FG Measurements eight 2"	ent	6" EMPLOYEE 16 Pilot Height 3"
	Pilot n RECCO (R = Re 1 2 3 4 5 6	er mea neasun PRD N rgage, i i i i i i i i i i i i i i i i i i i	red by: EW M C = Chi 16 16 16 16 16	by:	REME = Turn) 16 16 16 16 16 16 16 16 16 16 16 16	LEFT RIGHT	PUT A	."C'	" OR	"T" AF		RUIN 16 16 16 16 16 16 16 16 16 16 16 16 16	Front Rear Max. IG AN	16 16 16 16 16 16 16 16 16 Co	34 - 1/ R C T J J J J J J J J J J J J J J J J J J	2"	ont	6" EMPLOYEE

Figure 32. RMEX 08 Post-accident wheel inspection form.

The Mechanical Working Group toured the NS wheel truing shop in Chattanooga, Tennessee. Wheel truing operators use in-track machines equipped with wheel profile cutting tools to re-shape worn wheels into standard profiles. Wheel truing restores flange shape, flange root, and wheel tread profiles. The truing process will therefore eliminate high flanges and hollow worn tread, returning a worn wheel profile to a standard profile by removing material from the wheel. Because this is a cutting process, the wheel must have enough metal in the rim to allow the new shape to be cut without creating a thin-rim wheel. A wheel without enough metal remaining is scrapped instead of trued.



Figure 33. NS Wheel True Machine

Investigators noted that the wheel profiles of RMEX 08 R2 and L4 had nonstandard 'grooves' in the wheel flange profile. These grooves are consistent with the effects of wheel truing and not normal wheel-rail wear.



Figure 34. NS Wheel Profile cutting tool with a wheel profile sketched for reference. (NTSB photo and annotation)



Figure 35. RMEX 08 Wheel Profiles and POD Track Profiles

4.3 TBOGI Data

Locomotives RMEX 08 and RMEX 06 passed an NS Truck Bogie Optical Geometry Inspection and Hunting Detection (TBOGI) system on March 13, 2023, in Flat Rock, Kentucky. The TBOGI wayside system is manufactured by Wayside Inspection Devices. It uses laser-based systems on trains passing at normal operating speeds. It is capable of detecting axle angle of attack, axle tracking position, misalignments between axles, differentials between the tracking of two axles, truck rotation, truck lateral shift, and truck hunting/ lateral instability. According to manufacturer documents, these systems are designed to allow customers to increase wheel life, stop premature wear, improve fuel efficiency, reduce the risk of unscheduled maintenance and derailments, and reveal hidden root causes of wear through rolling stock condition monitoring. These detectors do not send alerts to the train crews. Rather, the information is collected by maintenance personnel for diagnosis and scheduled maintenance. According to NS officials, the information can also be used post-accident to help determine root causes of accidents when applicable.



Figure 36. A field installation of TBOGI (WDI stock image)



Figure 37. TBOGI measurements. (Manufacturer sales document)

Following the accident, NS officials provided the TBOGI data for RMEX 08 and RMEX 06. There were no exceptions noted with RMEX 06. For RMEX 08, TBOGI identified large angles of attack on axle numbers 4 and 2, -9.5 milliradians and 7.9 milliradians respectively.⁷ Additionally, axle number 3 displayed a tracking position

⁷ A milliradian is an SI unit for angular measurement which is defines as a thousandth of a radian. They

error of 12.9 millimeters. These conditions are not subject to Federal regulations or industry standards and are therefore not considered "defective" on their own. Rather, the railroad uses these measurements for maintenance scheduling and post-accident analysis to make improvements as needed.



Figure 38. RMEX 08 TBOGI Data

are generally used for very small angles.

RMEX 08 at TBOGI Site	Angle of Attack (mrad)	Tracking Position (mm)
(Speed 52 km/h)		
Axle 1	-0.8	-5.0
Axle 2	7.9	10.2
Axle 3	1.5	12.9
Axle 4	-9.5	2.5

4.4 Locomotive Bolster Stop Blocks

Locomotives RMEX 06 and RMEX 08 were equipped with bolster stops, at the time of the derailment, two bolster stops were missing/broken.⁸ Alignment control couplers and bolster stops both serve to limit coupler angles and coupler rotation. Bolster stops are applied to locomotives with pin-type couplers and no alignment control features to allow operation in consists with locomotives capable of high dynamic braking effort (but not over 200,000 pounds). Bolster stops are designed to prevent jackknifing when locomotives are subject to high dynamic braking effort.⁹ Norfolk Southern rules do not account for the use of bolster stops.

Locomotive RMEX 06 was missing the stop block at the right rear location. Locomotive RMEX 08 was missing the stop block at the left rear location. The brackets holding the stop blocks were broken at the 90-degree bend. The rusty and worn condition of the brackets is consistent with 'old' break. The mechanical working group determined the bolster stop blocks were broken/missing before departure of the train from Atlanta.

⁸ Bolster stops are removable blocks mounted to the truck side frame that resist the lateral movement of the locomotive body bolster.

⁹ https://tsb.gc.ca/eng/rapports-reports/rail/2002/r02c0050/r02c0050.html



Figure 39. Location of missing bolster stop blocks



Figure 40. RMEX 08 Bolster stop bock in the normal configuration.



Figure 41. RMEX 08 broken bolster stop block

4.5 In Train Forces

NS conducted TOES in-train force modeling for three different scenarios. Scenario 1 was a recreation of the accident events using all available data. Scenario 2 was a recreation of the events the train experienced near Mile Post 707 where investigators noticed a chance for higher in-train forces prior to the derailment sequence. Finally, Scenario 3 attempted to simulate in-train forces near the POD, but with the rear articulated cars moved to the front position just behind the locomotives.







Figure 43. TOES Scenario 2



Figure 44. TOES Scenario 3

4.6 Coupler Angle Calculations

Investigators measured the lateral coupler travel for locomotives RMEX 06 and RMEX 08.



Coupler Angle Calculations

Figure 45. Locomotive coupler angle calculations.

= NS

4.7 Rolling Radius Differential

Although wheel flanges are designed to interact with the rail, in principle, in low degree curves a rail vehicle can guide itself around curves in the track without the 23

wheel flanges touching the rails.¹⁰ This phenomenon arises from the conical shape of the wheel profile. When a wheelset deviates to one side, as in a curve, the conical wheel tread will mover relative to the rail surface so that its effective rolling radius increases while at the same time the other wheel will have its effective rolling radius decrease. The difference in radius between the two wheels of a wheel set is known as the rolling radius differential. Rail wheels wear over time, creating a worn profile with differing rolling radius. The process of reshaping a worn wheel into an ideal profile is known as truing and was described in this report above.

The risk for a derailment through wheel climb or rail-rollover mechanisms can be calculated using the Lateral-over-Vertical force index or threshold.¹¹ In a railrollover derailment, the L/V index is primarily a function of the wheel-rail contact points, lateral forces applied by the wheel flange (including any in-train forces translated from the couplers), and by the height and base dimensions of the rail section (known as Base-over-Height, or B/H ratio).



Figure 46. L-over-V Ratio (Wolfe 2021)

¹⁰ https://the-contact-patch.com/book/rail/r0415-curving

¹¹ Wolfe (2021)



Figure 47. B/H Description (Wolfe 2021)



Investigators calculated the rolling radius differentials and wheel-rail contact points for the locomotive consist. The information for RMEX 08 is below, the other data will be in the docket for this investigation.



Figure 49. RMEX 08 wheel-rail contact data.



Figure 50. RMEX 08 Rolling Radius Differential plots

4.8 Mechanical Condition

Investigators conducted inspections and air brake tests on the EOT and nonderailed portion of the train. Two cars had brakes that failed to apply during the air brake test, however the brakes were not re-tested.

Investigators noted the following conditions not mentioned in Section 3.0.

- RMEX 06 and RMEX 08 were equipped with non-alignment control couplers.
- The RMEX 06 was missing the right-rear coupler pocket stopping block. The welded securement tab had evidence consistent with a recent break. The alignment block was not recovered from the accident wreckage.
- RMEX 08 had wheel flanges greater than 1.5-inches at the R2, R4, and L4 locations.
- RMEX 08 had brake shoe rigging securement bolt with a missing cotter key.
- RMEX 08 had the right rear switching step loose, a loose safety appliance, a disconnected sanding hose, and possible side bearing excessive clearance on the front truck which needed to be reinspected on level and tangent track.
- RMEX 06 had an auxiliary light missing, window glazing shattered, excessive front pilot height, switching step improperly secured, fuel safety shut off not labeled, defective MU valve handles, and a walkway tripping hazard.
- Locomotives NS 4408 and NS 9485 did not have blue cards or daily inspection records.

- Near MP 721.05 (post derailment) two bulkhead flat cars, COER 804792 and COER 804785, came to rest with 'jackknifed' couplers pushed to the south. Investigators observed the couplers re-center when the rear portion of the train was pulled away.
- One car had a loose safety appliance, one car had a broken safety appliance
- One car had one brake shoe with the backing plate in contact with the wheel.
- One car had an inoperative uncoupling lever (consistent with derailment damage)
- CALIPI and Miniprof wheel profiles were taken on the locomotive consists.

E. DOCUMENTS REVIEWED

- NS Train 245A109 Consist Printed 03/09/23 07:03 PM CST
- Interview transcripts from Locomotive Engineer, Conductor, and NS Managers
- ME-925 For RMEX 06 (Dated 1/18/23) and RMEX 08 (Dated 2/2/23)
- NS Locomotive Department Instruction (LDI) 1-21
- NS LDI 10-11
- NS-1 Rules for Equipment Operation and Handling (Eff. 1/1/2019)
- Email communications between NS staff regarding RMEX 06 and RMEX 08
- Train pre-departure inspection and test documents
- NS Drone Imagery
- CALIPRI and Miniprof Wheel and Rail Profile Data
- Wayside Detector data including TBOGI and Wheel Profile
- NS Presentation to Mechanical Working Group including wheel profile and TOES model data.
- FRA Inspection Reports (F6180.96)
- Train Profile information derived from WILD detector data and train consist data
- Locomotive Event Recorder Data
- Track Profiles
- EOT Download Data
- Inspection, testing, and maintenance records
- Waybills
- Blue Cards
- UMLER Records
- NS Gold Card Instructions and Forms
- NS Presentation on results of TOES modeling, wheel and track profile measurements, etc. Given to the Mechanical Working Group in Chattanooga; April 2023

Submitted by:

John Manutes Railroad Accident Investigator, Mechanical Working Group Chair