## GOVERNMENT GEOTECHNICAL REPORT FOR NATIONAL TRANSPORTATION SAFETY BOARD



### PREPARED BY

### **U.S. ARMY CORPS OF ENGINEERS**

### FORT WORTH DISTRICT

### **ENGINEERING AND CONSTRUCTION DIVISION**

### **GEOTECHNICAL BRANCH**

CESWF-EC-G

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#### **GOVERNMENT GEOTECHNICAL REPORT**

#### 1. General.

The purpose of this report is to outline the results of a geotechnical study performed to help the National Transportation Safety Board (NTSB) evaluate the technical accuracy of the preliminary geotechnical assessment report provided by Bryant Consultants, Incorporated (BCI) regarding the possible cause of the gas pipeline explosion in Dallas, TX.

The NTSB has requested the services of U.S. Army Corps of Engineers (USACE) for this study. This work is being performed as per the Inter/Intra-Agency Agreement Number 9531BM19H0019 dated October 10, 2018 between NTSB and USACE. This agreement was modified on February 20, 2019 to change the technical point of contact and extend the period of performance to April 30, 2019. The scope of our work included reviewing the preliminary assessment report prepared by Bryant Consultants, Incorporated, performing borings to determine subsurface stratigraphy and collecting soil samples within the accident area, determining the characteristics of the soil samples and performing analyses to determine the shrink/swell potential of the soils. Figure 1 shows the accident block and the location of natural gas leaks.



Accident Block: Espanola Dr.—El Centro Dr.—Durango Dr.—Larga Dr.

Figure 1 Map of the block bounded by Durango Drive, Larga Drive, Espanola Drive, and El Centro Drive showing the location of natural gas leaks and affected houses.

#### 2. Subsurface Investigation.

In line with the Scope of Work developed by the U.S. Army Corps of Engineers (USACE), Fort Worth District, three (3) borings were drilled for this assessment. One of the originally proposed borings (Boring B-3) could not be drilled due to the presence of existing utilities. The borings were drilled to depths of 20 feet below ground surface. The field investigation was performed using a Gus Pech 1300C truck-mounted drill rig and conventional drilling attachments. Test hole advancement and sample recovery was performed using 6-inch diameter short flight hollow stem augers, a nominal 3-inch diameter Shelby tube sampler, and a 6-inch diameter drag bit. Samples recovered from the borings were sealed in airtight containers and taken to the laboratory of TEAM Consultants, Incorporated (Arlington, Texas) for testing. Boring locations are shown in Figure B-101. Results of the field investigation are shown in Logs of Borings (Appendix A).

a. <u>Groundwater Conditions.</u> Groundwater conditions were monitored during and upon completion of drilling operations. The borings were dry during the observation period. However, it should be noted that groundwater conditions are relative to the time of drilling, annual precipitation, and drainage conditions at the site.

#### 3. Subsurface Conditions.

<u>General Geology.</u> Based on the Geological Atlas of Texas, Dallas Sheet, primary material underlying the accident block consists of Eagle Ford Shale Formation ( $K_{ef}$ ). Figure 2 shows the location of the accident block. To the West of the block is the Fluviatile Terrace Deposits ( $Q_t$ ) and to the East of the block is the Austin Chalk Formation ( $K_{au}$ ). Eagle Ford Shale Formation and the Austin Chalk Formation are of the Upper Cretaceous age whereas the Fluviatile Terrace Deposits are of the Pleistocene age.

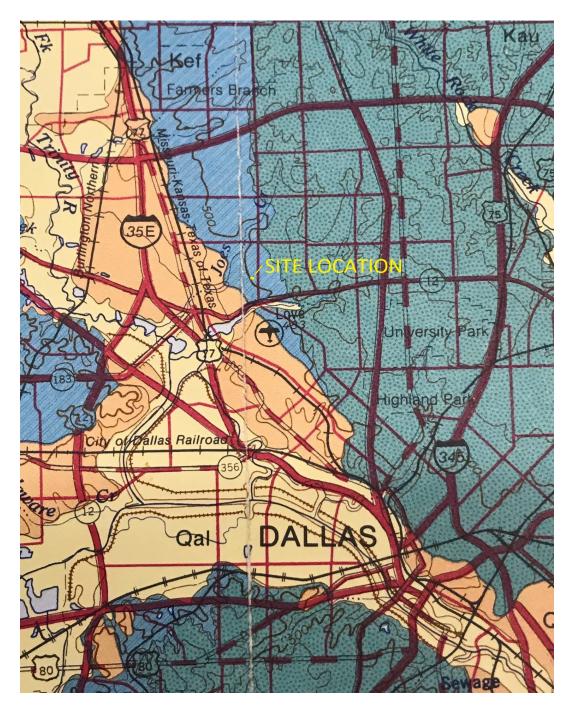


Figure 2 Geology at the accident block (Geological Atlas of Texas, Dallas Sheet)

The Eagle Ford Shale Formation typically consists of shale, sandstone, and limestone interbedded with clay seams. Soils derived from the Eagle Ford Shale Formation are typically plastic clays exhibiting high shrink/swell potential with variations in moisture content. The Austin Chalk Formation consists of gray chalky limestone with some shale and partings. This

unit weathers to a light tan; it is typically overlain by a layer of residual, dark colored clay. The residual clays on top of the chalky limestone are highly expansive. Fluviatile Terrace deposits consist of gravel, sand, silt and clay.

Subsurface conditions representative of the project site are shown on the logs of borings in Appendix A. The legend on the individual boring logs show materials as classified in the laboratory using procedures presented in ASTM D 2488. It should be noted that the actual interface between material types may be far more gradual or abrupt than presented; therefore, actual subsurface conditions in areas not sampled may differ from those predicted.

#### 4. Testing.

Laboratory Testing. Representative soil samples recovered from test holes were subjected to laboratory testing for identification, moisture content, grain-size distribution, Atterberg limits, density, and controlled expansion-consolidation. The accumulative test results are tabulated and presented in Appendix B. Results of identification and moisture content testing are shown on the boring logs, Appendix A.

Results of laboratory testing performed on samples obtained from the site are presented graphically in Appendix B as follows: Plasticity characteristics are shown on Plate 1, Plasticity Chart. Moisture content values of representative samples are shown with respect to depth on Plate 2. Atterberg limits test results are shown with respect to depth on Plate 3. Dry density values of representative undisturbed samples and their corresponding moisture contents are shown with respect to depth on Plate 4.

#### (1) Controlled Expansion-Consolidation Testing and Swell Pressure

<u>Testing.</u> Controlled expansion-consolidation (CEC) testing was performed on eight specimens of high plasticity (CH) clay and one specimen of low plasticity (CL) clay collected at the site. The high plasticity (CH) clay overburden specimens were collected at depths ranging between

2 to 15 feet. Liquid limits (LL) measured from representative samples of the high plasticity clays vary between 51 and 64, plastic limits (PL) vary between 18 and 25 with plasticity indices (PI) between 32 and 41. The moisture content is equal to and up to 3 percent higher than the plastic limit. An expansion pressure ( $P_{exp}$ ) of approximately 0.75 tons per square foot (tsf) to 1.5 tsf was recorded during CEC testing of the high plasticity clay specimens. Based on CEC test results, and the considerations discussed above, the high plasticity clay specimens have a moderate to high expansion potential ( $C_s = 0.04$  to 0.06) and a moderate to high consolidation potential ( $C_c = 0.15$  to 0.22) at present moisture contents.

Controlled expansion-consolidation testing was performed on one specimen of the low plasticity clay at depth of 18 to 20 feet. LL measured from representative samples of the low plasticity clays were 45 and 46, PL was 18, with PI of 27 and 28. The moisture content is 2 percent higher than the plastic limit. An expansion pressure ( $P_{exp}$ ) of approximately 1.0 tsf was recorded during CEC testing of the low plasticity clay specimen. Based on CEC test results, the low plasticity clay specimen has moderate expansion potential ( $C_s = 0.04$ ) and a moderate consolidation potential ( $C_c = 0.15$ ) at present moisture content. Controlled expansion-consolidation test results are presented in Appendix C at the end of this report.

| Boring<br>Number | Depth<br>(feet) | Liquid<br>Limit | Plasticity<br>Index | P <sub>exp</sub> (tsf) | $P_{exp}/P_o$ | Cs   | Cc   | Soil<br>Type |
|------------------|-----------------|-----------------|---------------------|------------------------|---------------|------|------|--------------|
| B-1              | 2.0             | 63              | 39                  | 0.75                   | 4.0           | 0.06 | 0.19 | СН           |
| B-1              | 8.0             | 55              | 33                  | 1.0                    | 1.8           | 0.05 | 0.18 | СН           |
| B-2              | 2.0             | 61              | 36                  | 1.0                    | 5.4           | 0.06 | 0.22 | СН           |
| B-2              | 4.0             | 57              | 36                  | 1.0                    | 3.2           | 0.05 | 0.19 | СН           |
| B-2              | 13.0            | 60              | 40                  | 1.5                    | 1.7           | 0.05 | 0.15 | СН           |
| B-4              | 1.0             | 64              | 40                  | 1.5                    | 12.0          | 0.06 | 0.22 | СН           |
| B-4              | 5.0             | 61              | 39                  | 1.0                    | 2.7           | 0.06 | 0.19 | СН           |
| B-4              | 8.0             | 52              | 32                  | 1.0                    | 1.8           | 0.04 | 0.16 | СН           |
| B-4              | 18.0            | 45              | 27                  | 1.0                    | 0.8           | 0.04 | 0.15 | CL           |

Controlled expansion-consolidation test results are summarized below.

 $P_{exp}$ = Swell Pressure in tons per square foot;  $P_0$ = Overburden Pressure in tons per square foot

C<sub>s</sub>= Swell Index; C<sub>c</sub>= Compression Index

#### 5. Discussions.

The surficial soils encountered in the borings are high plasticity clays. Swell potential significantly increases as subgrade moisture content increases. Based on TxDOT test method TEX-124-E which uses Atterberg limits values and in situ moisture content, we estimate a potential vertical rise (PVR) in the range of  $1-\frac{3}{4}$  to  $2-\frac{1}{2}$  inches. Our estimate assumes a zone of influence of 15.0 feet below ground surface. PVR in the range of  $2-\frac{1}{2}$  to 3.0 inches is estimated assuming a dry soil moisture condition.

As mentioned previously in the general geology section of this report, the accident block is located in an area underlain by the Eagle Ford Shale Formation. Fluviatile Terrace deposits are located to the west and Austin Chalk Formation is located to the east of the Eagle Ford Formation. Soils derived from the Eagle Ford Shale Formation and the residual soils on top of the Austin Chalk Formation are high plasticity clays. These clays shrink on drying and swell when provided access to water. This shrink/swell movement causes a lot of distress to the structures constructed on top or within these formations.

The borings were drilled in March during the colder months. So, the soils encountered at the site were moist and the moisture content was equal to and up to 3 percent higher than the plastic limit of the soil. The swell pressure recorded in the soil samples tested ranged between 0.75 tons per square foot (tsf) to 1.5 tsf. Drier high plasticity soils exert very high swell pressures (5 to 6 tsf) when provided access to water and prevented from swelling. The ratio of the swell pressure to overburden pressure ( $P_{exp}/P_o$ ) of high plasticity clays at this site ranged from 1.7 to 12 indicating a moderate to very high swell potential.

Structures and pipes founded within highly expansive soils as well as in different geological formations experience differential movements when variable moisture conditions are present in the soils supporting the structures or pipes. Clays are impermeable and water cannot easily flow through them whereas sands and gravels are permeable and provide easy access for water to permeate. Granular backfill around the pipes also provide a medium through which

water flows easily. There may be localized areas where water may stagnate within these granular backfill and cause heave. This localized heave will cause differential movement between this area and the area not provided access to water. There may also be low areas where water is ponding causing localized heave. During summer, the highly plastic clays shrink. This cyclic shrink /swell movement exerts a lot of forces on the joints and pipe connections. The magnitude of the force is directly proportional to the plasticity of the soil and the variability of the moisture content within the soil. Construction in the vicinity of the buried pipes may also provide access to water in the soils supporting the pipes.

#### 6. Conclusions.

BCI's report asserts there are two different geologic formations, the Eagle Ford and Austin Chalk, underlying the accident site. USACE, Fort Worth District disagrees that there are two different geologic formations underlying the accident site. Based on the site-specific borings, drilled as part of the USACE subsurface investigation, there is only one geologic formation, the Eagle Ford Shale, underlying the accident site. Furthermore, based on the lab test results, the plasticity characteristics and swell potential of the subsurface materials within the accident block are highly uniform.

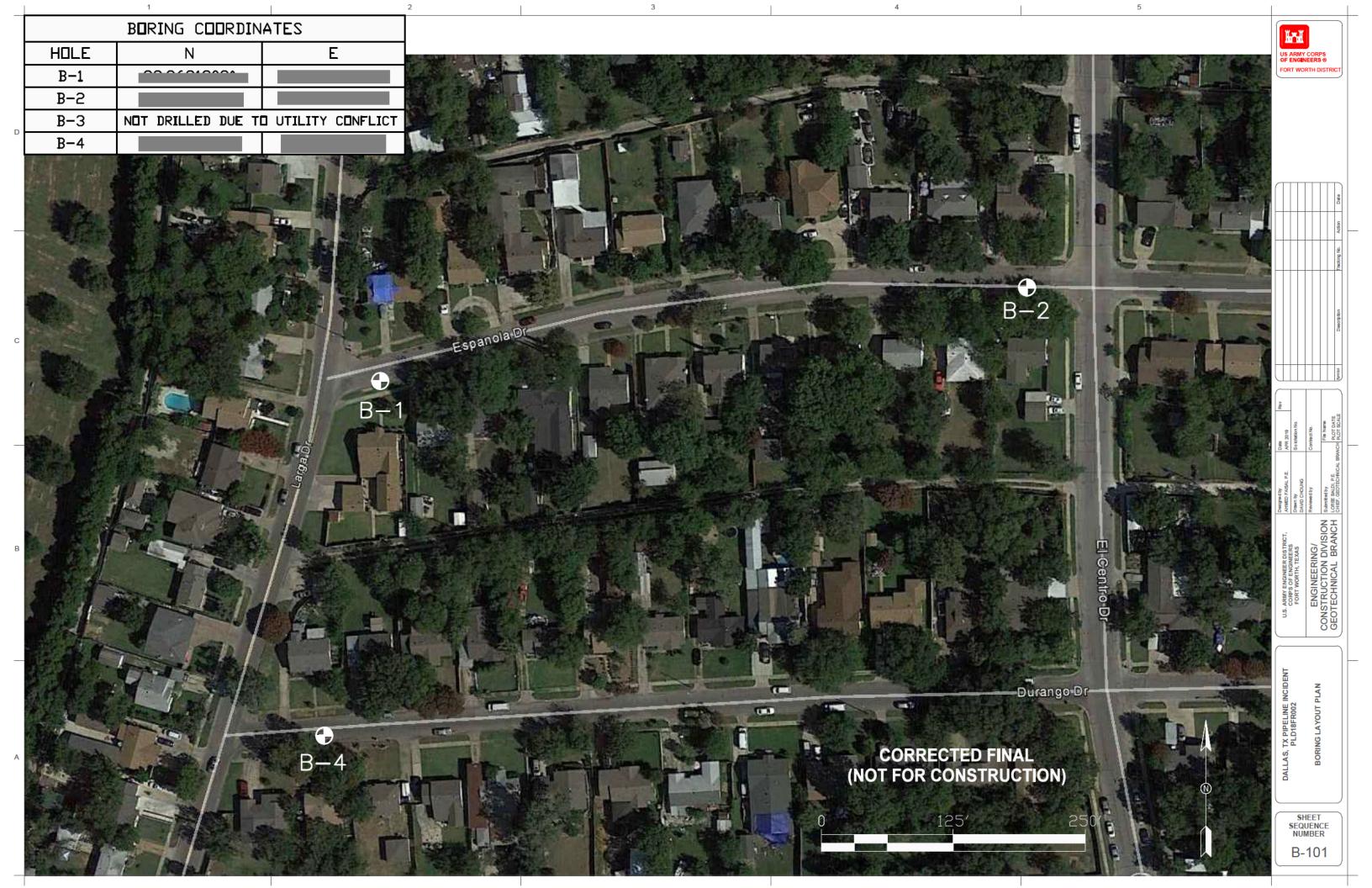
#### **References:**

- TEAM Consultants, Incorporated Report No. 192031
- TM 5-818-1 Soils and Geology Procedures for Foundation Design of Buildings and Other Structures (Except Hydraulic Structures)
- TM 5-818-7 Foundations in Expansive Soils
- UFGS Guide Specifications for Construction

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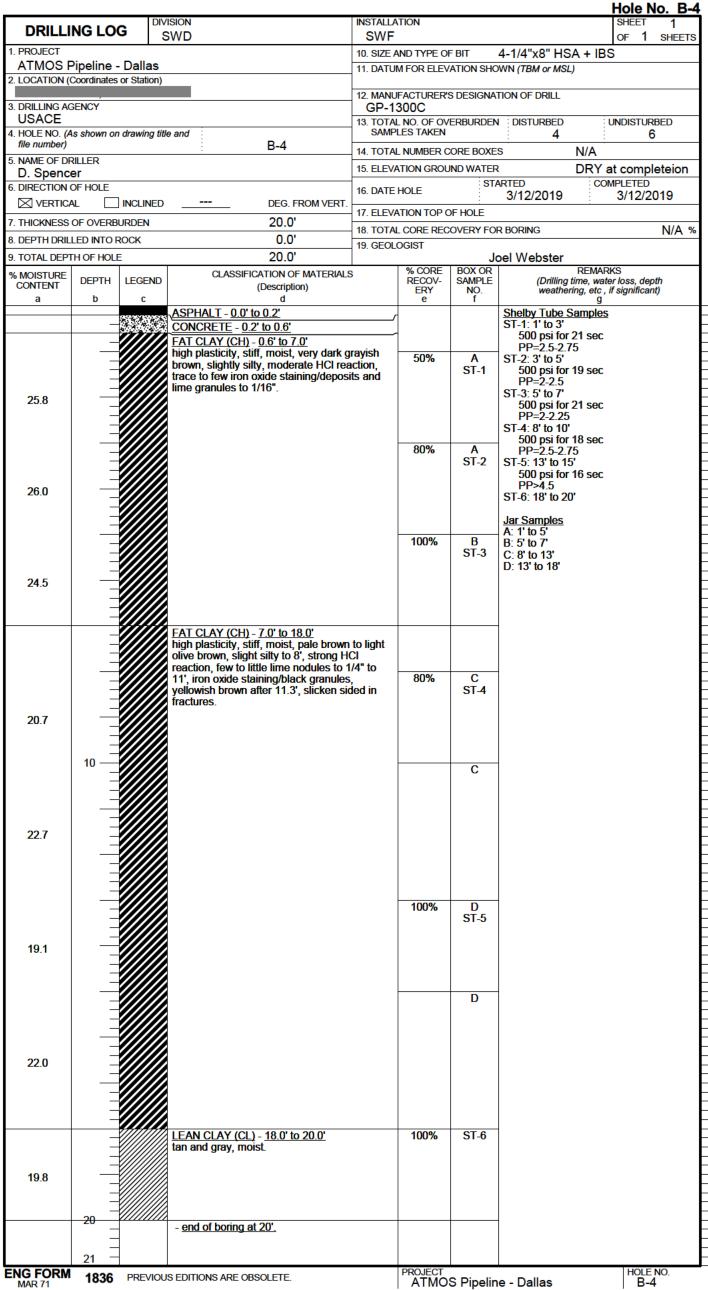
APPENDIX A

**BORING LOCATIONS & LOGS OF BORINGS** 



| DRILLI                  |            |                      | ision<br>SWD  | INSTALLA<br>SWF   | TION                     |               | SHEET  |              |
|-------------------------|------------|----------------------|---|-------------------|--------------------------|---------------|--|--------------|
| PROJECT                 |            |                      |   |                   | ND TYPE O                | F BIT         |  | SHEE         |
|                         |            |                      |   |                   |                          |               | DWN (TBM or MSL)   |              |
| LOCATION (C             |            | or station)          |   | 12. MANU          | FACTURER                 | S DESIGNA     | TION OF DRILL  |              |
| DRILLING AG             | ENCY       |                      |   | GP-1              | 300C                     |               |  |              |
| USACE<br>HOLE NO. (A    | s shown on | drawing titl         | e and   |                   | . NO. OF OV<br>LES TAKEN | ERBURDEN      | N DISTURBED UNDISTU  | JRBED        |
| file number)            |            | <b>,</b>             | B-1   | 14. TOTAL         | NUMBER C                 | ORE BOXE      |  | -            |
| NAME OF DR<br>D. Spence |            |                      |   | 15. ELEVA         | TION GROU                |               | DRY at com   | pleteio      |
| DIRECTION               |            |                      |   | 16. DATE          | HOLE                     | ST            | ARTED COMPLETED 3/13/2019 3/13/                                |              |
|                         |            | INCLINED             | DEG. FROM VERT.   | 17. ELEVA         |                          | DF HOLE       | 3/13/2018 3/13/  | 2013         |
| THICKNESS (             |            |                      | 20.0'   | 18. TOTAL         | CORE REC                 | OVERY FO      | R BORING   | N/A          |
| DEPTH DRILL             |            |                      | 0.0'<br>20.0'   | 19. GEOL          | OGIST                    |               | oel Webster  |              |
| MOISTURE                |            |                      | CLASSIFICATION OF MATERIALS   | 3                 | % CORE                   | BOX OR        | REMARKS  |              |
| ONTENT                  | DEPTH      | LEGEND               | (Description)   |                   | RECOV-<br>ERY            | SAMPLE<br>NO. | (Drilling time, water loss, d<br>weathering, etc , if signific | əpth<br>ant) |
| а                       | b          | C                    | d<br>ASPHALT - 0.0' to 0.3'   |                   | e                        | f             | g<br>Shelby Tube Samples                                       |              |
|                         |            | *****                | <b>BASE MATERIAL - SANDY GRAVEL</b>   | - <u>0.3' to</u>  |                          |               | ST-1: 2' to 4'<br>500 psi for 20 sec                           |              |
|                         |            |                      | <u>1.6'</u><br>coarse to fine grained, subangular, ma                                   | edium             |                          |               | PP=2.25  |              |
|                         |            | *****                | dense, moist to wet, pale brown, chall<br>to few fines.                                 | ky, trace         |                          |               | ST-X: 4' to 6'<br>500 psi for 17 sec                           |              |
|                         |            |                      | FAT CLAY (CH) - 1.6' to 7.2'  |                   |                          |               | no recovery<br>ST-2: 8' to 10'                                 |              |
|                         |            |                      | high plasticity, stiff, moist, gray, silty, f<br>little fine grained sand, moderate HCI | reaction.         | IBS<br>85%               | A<br>ST 1     | 500 psi for 16 sec   |              |
|                         |            |                      | trace to few lime granules to 1/16", tra<br>oxide staining; becoming gray and ligh      | ace iron          | 80%                      | ST-1          | PP=2.5<br>ST-Y: 13' to 15'                                     |              |
| 25.3                    |            |                      | with little lime granules to 1/4" below 6   |                   |                          |               | 500 psi for 16 sec<br>no recovery                              |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               | Jar Samples<br>A: 2' to 4'                                     |              |
|                         |            |                      |   |                   | IBS<br>100%              | B             | B: 4' to 7.2'<br>C: 8' to 13'                                  |              |
|                         |            |                      |   |                   | _                        |               | D: 13' to 17.1'  |              |
|                         |            |                      |   |                   |                          |               | E: 17.1' to 17.9'<br>F: 18' to 20'                             |              |
| 25.0                    | _          |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      | FAT CLAY (CH) - 7.2' to 17.1'   |                   |                          |               | -  |              |
|                         |            |                      | high plasticity, stiff, moist, light gray w<br>vellowish brown staining, moderate H     | rith<br>Cl        |                          |               |  |              |
|                         |            |                      | reaction, trace black staining/iron oxid<br>granules to 1/4", trace lime granules to    | e                 | IBS                      | ST-2          | 1  |              |
|                         |            |                      | granules to 1/4, trace lime granules to   | U 1/4 .           | 100%                     |               |  |              |
| 22.1                    |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         | 10 —       |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          | С             |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
| 23.9                    |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               | -  |              |
|                         |            |                      |   |                   | SPT-N<br>6-8-9-9         | D             |  |              |
|                         |            |                      |   |                   | 95%                      |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
| 26.6                    |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         |            |                      | LEAN CLAY WITH SAND (CL) - 17.1   |                   |                          | E             | -  |              |
| 17.5                    |            |                      | tan and gray, moist, very silty with sor<br>grained, slickensided in fractures.         |                   |                          |               |  |              |
|                         |            |                      | SILTY SAND (SM) - 17.9' to 20.0'  |                   |                          | F             | 1  |              |
|                         |            |                      | fine grained, poorly graded quartz, me<br>dense, light gray to 19', yellowish brow      | edium<br>vn below |                          | '             |  |              |
| 10.0                    |            |                      | 19', trace fines.   |                   |                          |               |  |              |
| 19.0                    |            |                      |   |                   |                          |               |  |              |
|                         |            |                      |   |                   |                          |               |  |              |
|                         | -20 _      | ··· (••· •• •• •• •• | - end of boring at 20'.   |                   |                          |               | 1  |              |
|                         |            |                      |   |                   |                          | 1             |  |              |
|                         | 21 -       |                      |   |                   |                          |               |  |              |

| DRILL                 | NG LOO      |              |   |                      | TION                    |                  | SHEET 1   |
|-----------------------|-------------|--------------|---|----------------------|-------------------------|------------------|---|
| PROJECT               |             |              | SWD   | SWF                  |                         |                  |   |
| ATMOS F               |             |              |   |                      | ND TYPE O               |                  | 4-1/4"x8" HSA + IBS                               |
| LOCATION (            |             |              |   |                      |                         |                  | . ,   |
| DRILLING AC           | GENCY       |              |   | 12. MANU             |                         | S DESIGNA        | TION OF DRILL                                     |
| USACE                 |             | drawing      | o and   | 13. TOTAL            | . NO. OF OV<br>ES TAKEN | ERBURDEN         |   |
| file number)          | as snown on | drawing titi | B-2   |                      | . NUMBER C              |                  | <u>    6     4    </u><br>s <u>N/A</u>            |
|                       |             |              |   |                      | TION GROU               |                  |   |
| D. Spenc              |             |              |   | 16. DATE I           |                         |                  | ARTED COMPLETED                                   |
|                       |             | INCLINED     | DEG. FROM VERT.   |                      |                         |                  | 3/13/2019 3/13/2019                               |
| THICKNESS             | OF OVERBU   | JRDEN        | 20.0'   |                      | TION TOP C              |                  | R BORING N/A                                      |
| DEPTH DRIL            | LED INTO R  | OCK          | 0.0'  | 19. GEOLO            |                         | OVERTIFU         | R BORING IN/P                                     |
| TOTAL DEPT            | TH OF HOLE  |              | 20.0'   |                      | A/ 0005                 |                  | oel Webster                                       |
| 6 MOISTURE<br>CONTENT | DEPTH       | LEGEND       | CLASSIFICATION OF MATERIALS<br>(Description)  | 3                    | % CORE<br>RECOV-        | BOX OR<br>SAMPLE | REMARKS<br>(Drilling time, water loss, depth      |
| а                     | b           | с            | d   |                      | ERY<br>e                | NO.<br>f         | weathering, etc , if significant)                 |
|                       |             | *****        | <u>ASPHALT - 0.0' to 0.3'</u><br>BASE MATERIAL - SANDY GRAVEL                         | - 0 3' to            |                         |                  | Shelby Tube Samples<br>ST-1: 2' to 4'             |
|                       |             |              | 1.0'  |                      |                         |                  | 500 psi for 15 sec<br>PP=2.75                     |
|                       |             |              | coarse to fine grained, subangular, m<br>dense, moist, pale brown, chalky, trac       | edium<br>ce to few [ |                         |                  | ST-2: 4' to 6'                                    |
|                       |             |              | fines.<br><u>FAT CLAY (CH)</u> - <u>1.0' to 5.7'</u>                                  | ]                    |                         |                  | 500 psi for 15 sec<br>PP=2.5                      |
|                       |             |              | high plasticity, stiff, moist, dark gray,   | slightly             | 85%                     | A                | ST-3: 8' to 10'<br>500 psi for 19 sec             |
|                       |             |              | silty, trace fine grained sand, trace ling<br>granules to 1/16", trace rootlets; beco | ming                 | 0070                    | ST-1             | PP=2.5  |
| 26.6                  |             |              | light gray with little lime granules to 1/<br>4.5', strong HCI reaction.              | 8" below             |                         |                  | ST-4: 13' to 15'<br>500 psi for 20 sec            |
| 20.0                  |             |              | H.J., SUUNY FICHTERCUUM.  |                      |                         |                  | PP=2.75<br>ST-5: 18' to 20' (no recovery - SPT or |
|                       |             |              |   |                      |                         |                  | 2nd attempt)                                      |
|                       |             |              |   |                      | 100%                    | A                | 500 psi for 19 sec<br>PP=2.75                     |
|                       | 1           |              |   |                      |                         | ST-2             | Jar Samples                                       |
| 21.7                  |             |              |   |                      |                         |                  | A: 2' to 5.7'                                     |
|                       | =           |              |   |                      |                         |                  | B: 5.7' to 8'<br>C: 8' to 11.3'                   |
|                       |             |              | FAT CLAY (CH) - 5.7' to 8.0'  |                      |                         |                  | D: 11.3' to 12.1'<br>E: 13' to 18'                |
|                       |             |              | 'same as CH below'  |                      | IBS<br>100%             | В                | F: 18' to 20'                                     |
|                       |             |              |   |                      | 10070                   |                  |   |
| 19.4                  |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      | IDe                     | С                |   |
|                       |             |              | LEAN CLAY (CL) - 8.0' to 11.3'<br>tan and gray, moist.                                |                      | IBS<br>100%             | ST-3             |   |
| / <del></del> -       |             |              |   |                      |                         |                  |   |
| 17.8                  |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       | 10 —        |              |   |                      |                         | С                | -   |
| 20.0                  |             |              |   |                      |                         |                  |   |
| 20.8                  |             |              |   |                      |                         |                  |   |
|                       |             |              | LEAN CLAY WITH SAND (CL) - 11.3   | ' to 12.1'           |                         | D                | -   |
| 14.7                  | =           |              | tan, moist, some lime nodules to 1'.  |                      |                         |                  |   |
|                       |             |              | FAT CLAY (CH) - 12.1' to 20.0'  |                      |                         |                  | -   |
|                       |             |              | high plasticity, stiff, moist, light gray w<br>yellowish brown staining, moderate H   | vith little<br>Cl    |                         |                  |   |
|                       |             |              | reaction, trace to few silt, few lime no  | dules to             | IBS                     | E                | -   |
|                       |             |              | 1/4", trace black staining/granules to to little slickensides at 30° to 60°; yell     | owish                | 95%                     | ST-4             |   |
| 21.2                  |             |              | brown with some light gray below 12.  | 1'.                  |                         |                  |   |
| £1.£                  |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         | E                | 1   |
|                       |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
| 23.3                  |             |              |   |                      |                         |                  |   |
| _                     |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      | SPT-N                   | F                |   |
|                       | 1           |              |   |                      | 2-5-7-9<br>100%         |                  |   |
| 21.4                  |             |              |   |                      |                         |                  |   |
|                       |             |              |   |                      |                         |                  |   |
|                       | 20          |              |   |                      |                         |                  |   |
|                       |             |              | - end of boring at 20'.   |                      |                         |                  |   |
|                       | 21 -        |              |   |                      |                         |                  |   |
| NG FORM               |             |              |   |                      |                         |                  | he - Dallas B-2                                   |



**APPENDIX B** 

LABORATORY TESTING DATA PLOTS

## **ATMOS PIPELINE - DALLAS** PLASTICITY CHART

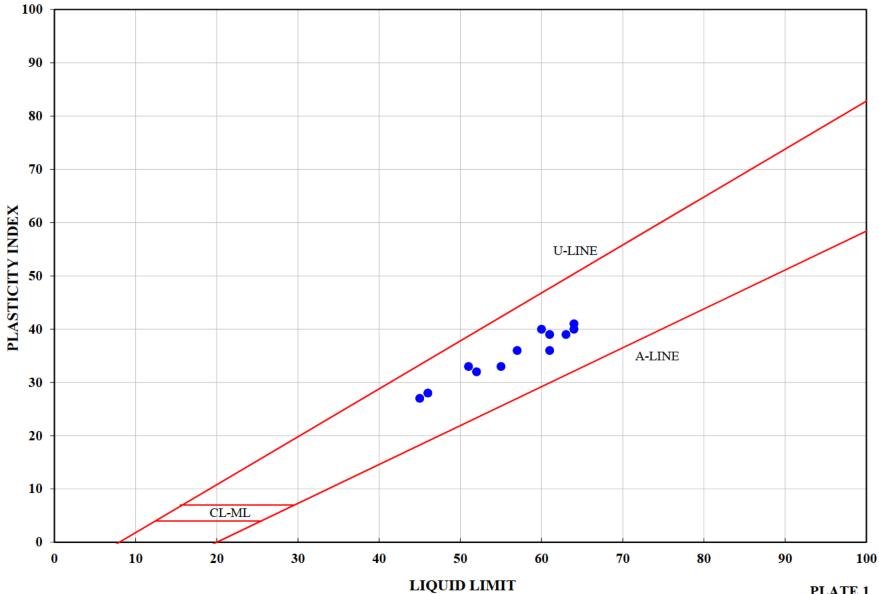
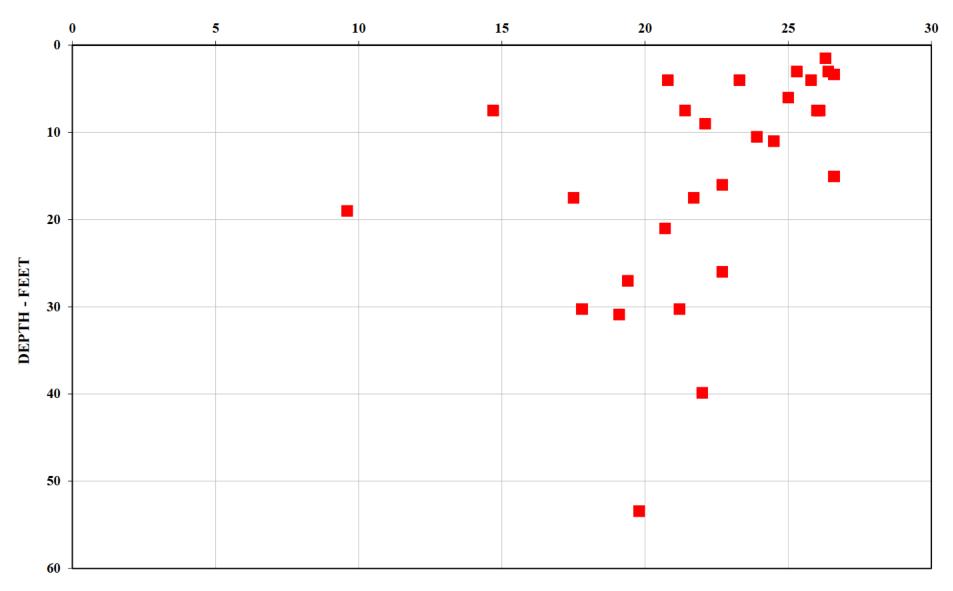


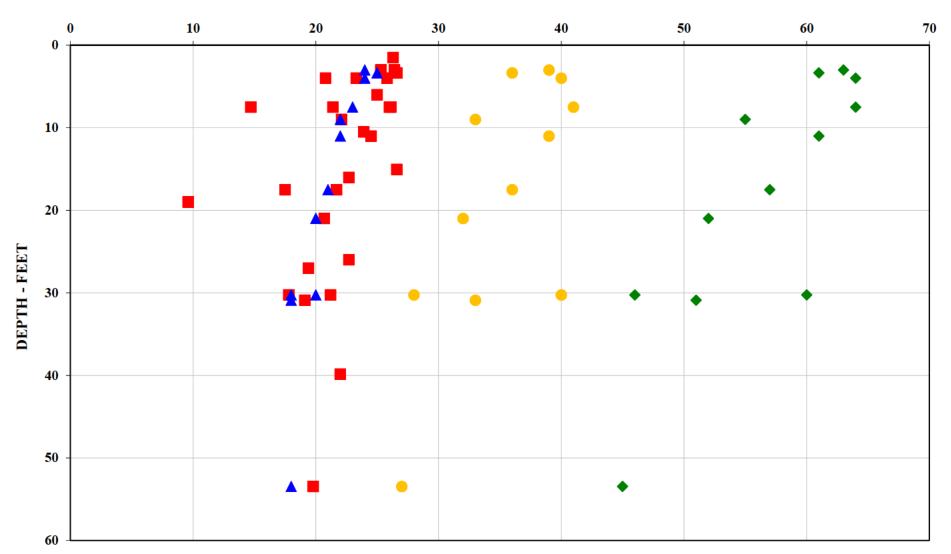
PLATE 1



## ATMOS PIPELINE - DALLAS MOISTURE CONTENT VS DEPTH

**MOISTURE CONTENT - %** 

PLATE 2

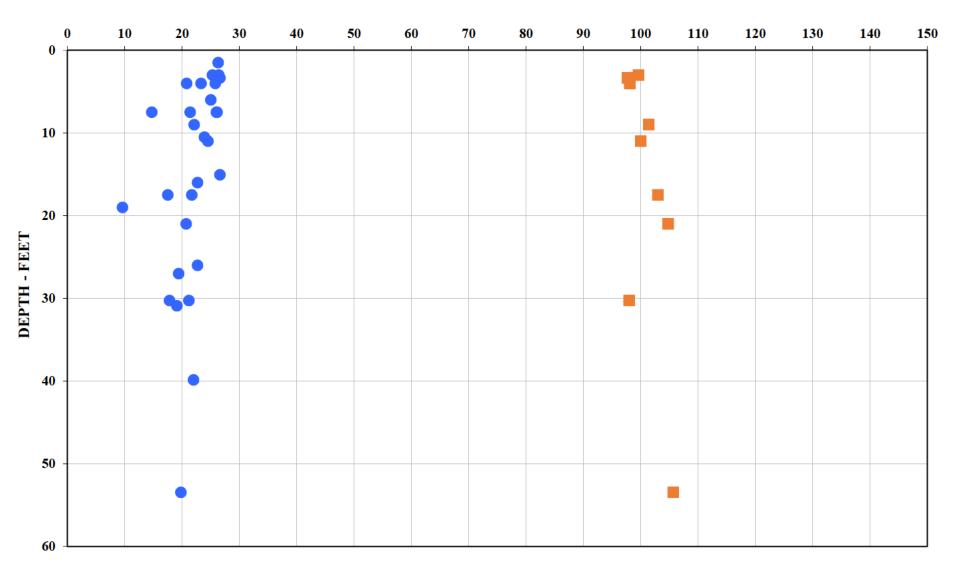


## ATMOS PIPELINE - DALLAS ATTERBERG LIMITS VS DEPTH

**MOISTURE CONTENT - %** 

■MC ◆LL ▲PL ●PI

PLATE 3



## ATMOS PIPELINE - DALLAS MOISTURE CONTENT - DRY DENSITY VS DEPTH

MOISTURE CONTENT - % DRY DENSITY - pcf

**APPENDIX C** 

LABORATORY TESTING DATA

Geotechnical, Environmental, Construction Materials Testing

April 15, 2019 TEAM Project No. 192031 Report No. 1

U.S. Army Corps of Engineers CESWF-EC-DG

Attn: Mr. Faisal Ahmed

Re: Laboratory Testing Services

Dear Mr. Ahmed:

Submitted here is our report of laboratory testing services completed on soil samples received at our materials testing laboratory in Arlington, Texas, on March 13, 2019 for the above referenced project. The laboratory test program authorized March 15, 2019 was finished utilizing the following test methodologies:

Moisture Content Atterberg Limits Grain Size Analysis Classification of Soils Controlled Expansion Consolidation

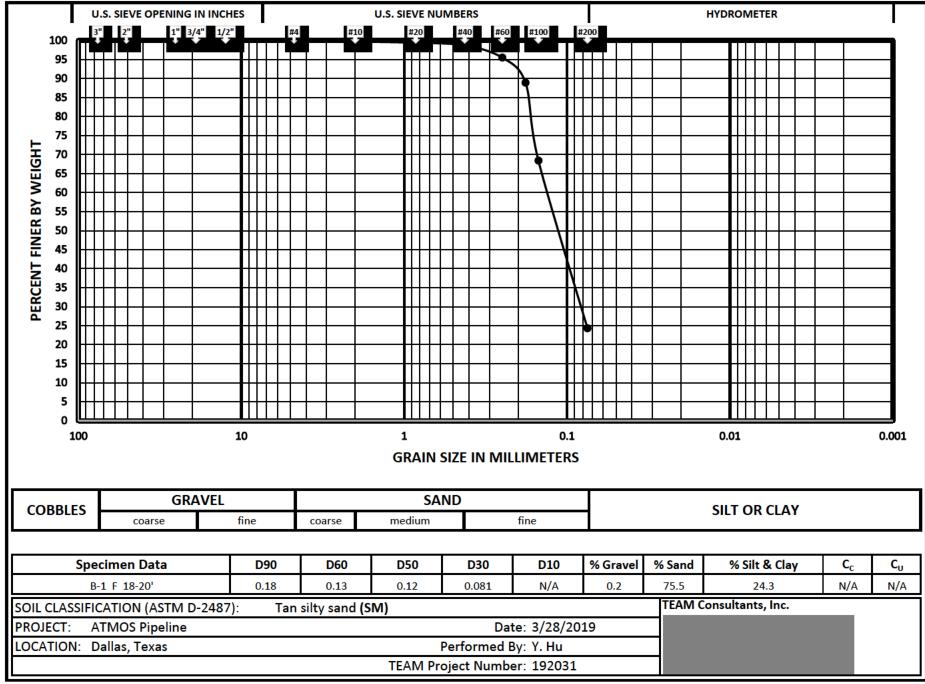
ASTM D-2216 ASTM D-4318 ASTM D-422 ASTM D-2487/D-2488 USACE EM 1110-2-1906, App. VIII

We appreciate the opportunity to be of assistance to you with this project. Should you have any questions, or if we may be of further assistance, please call the undersigned at **Comparison**.

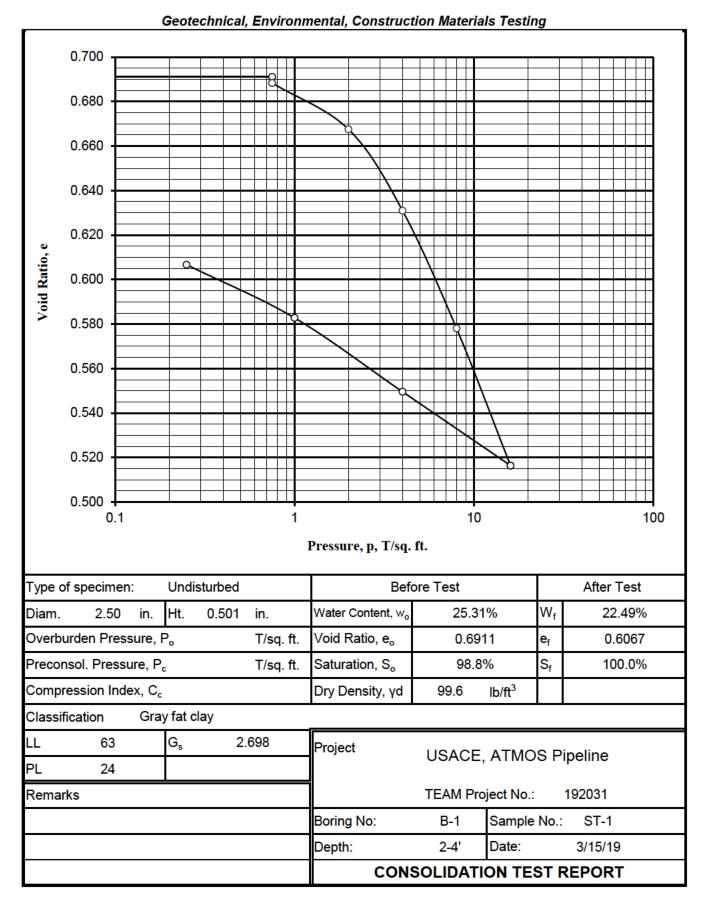
| Very truly yours,                   |  |
|-------------------------------------|--|
| Jason Young, GIT<br>Staff Geologist |  |
| Staff Geologist                     |  |
| James Hutt                          |  |
| Vice President                      |  |

|        |           |               | SUMMARY OF LABORATORY TEST RESULTS             |          |      |      |         |          |          |          |          |      |
|--------|-----------|---------------|--|----------|------|------|---------|----------|----------|----------|----------|------|
|        |           |               | LABORATORY TESTING SERVICES                    |          |      |      |         |          |          |          |          |      |
|        |           |               | NTSB Dallas Pipeline                           |          |      |      |         |          |          |          |          |      |
|        | T T T     | 1 1           | Dallas, Texas                                  | 1 1      | T    | 1    |         | 1        | 1        | 1        |          |      |
|        |           | Sample        |  |          |      |      |         |          |          |          |          |      |
| Boring | Sample    | Depth         | Visual Description &                           |          |      | -    | Percent |          |          | I.       | #400     | #000 |
| No.    | No.       | (ft.)         | Unified Soil Classification (ASTM D-2487/2488) |          | #4   | #10  | #20     | #40      | #60      | #80      | #100     | #200 |
| B-1    | ST-1      | 2-4           | Gray fat clay                                  | СН       | 99.6 | 97.4 | 96.0    | 95.2     | 94.4     | 93.3     | 92.1     | 88.2 |
|        | Α         | 2-4           | Gray fat clay                                  | СН       |      |      |         |          |          |          |          |      |
|        | В         | 4-8           | Light brown fat clay                           | СН       |      |      |         |          |          |          |          |      |
|        | ST-2      | 8-10          | Tan and gray fat clay                          | СН       | 99.4 | 98.0 | 97.0    | 96.5     | 95.9     | 95.2     | 94.4     | 92.0 |
|        | С         | 8-13          | Tan and gray fat clay                          | CH       |      |      |         |          |          |          |          |      |
|        | D         | 13-17.1       | Tan and gray fat clay                          | CH       |      |      |         |          |          |          |          |      |
|        | E         | 17.1-17.9     | Tan and gray lean clay with sand               | CL       |      |      |         |          |          |          |          |      |
|        | F         | 18-20         | Tan silty sand                                 | SM       | 99.8 | 99.7 | 99.4    | 98.7     | 95.5     | 88.9     | 68.4     | 24.3 |
| B-2    | ST-1      | 2-4           | Gray and dark brown fat clay                   | СН       | 100  | 99.6 | 99.2    | 98.9     | 98.4     | 97.6     | 96.7     | 94.3 |
| D-2    | A         | 2-5.7         | Dark gray fat clay                             | СН       |      |      |         |          |          |          |          |      |
|        | ST-2      | 4-6           | Gray and dark gray fat clay                    | СН       | 99.0 | 97.8 | 97.0    | 96.6     | 96.2     | 95.5     | 94.8     | 92.6 |
|        | B         | 5.7-8         | Light gray fat clay                            | СН       |      |      |         |          |          |          |          |      |
|        | ST-3      | 8-10          | Tan and gray lean clay                         | CL       | 99.9 | 99.6 | 98.7    | 97.9     | 97.1     | 96.4     | 95.6     | 93.6 |
|        | с         | 8-11.3        | Tan and gray fat clay                          | СН       |      |      |         |          |          |          |          |      |
|        | D         | 11.3-12.1     | Tan lean clay with sand                        | CL       |      |      |         |          |          |          |          |      |
|        | ST-4      | 13-15         | Tan and gray fat clay                          | СН       | 100  | 100  | 99.8    | 99.6     | 99.2     | 98.7     | 98.2     | 96.5 |
|        | E         | 13-18         | Brown and gray fat clay                        | СН       |      |      |         |          |          |          |          |      |
|        | F         | 18-20         | Brown and gray fat clay                        | СН       |      |      | -       |          |          |          | -        |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
| B-4    | A         | 1-5           | Gray fat clay                                  | СН       |      |      |         |          |          |          |          |      |
|        | ST-1      | 1-3           | Gray and dark brown fat clay                   | СН       | 98.9 | 98.0 | 96.8    | 96.1     | 95.2     | 94.0     | 92.6     | 88.9 |
|        | ST-2      | 3-5           | Gray and brown fat clay                        | СН       | 100  | 99.1 | 98.1    | 97.3     | 96.4     | 95.1     | 93.8     | 90.3 |
|        | ST-3      | 5-7           | Brown and gray fat clay                        | СН       | 98.3 | 95.7 | 94.5    | 93.5     | 92.6     | 91.5     | 90.7     | 87.6 |
|        | B         | 5-7           | Tan and gray fat clay                          | CH       |      |      |         |          |          |          |          |      |
|        | ST-4      | 8-10          | Tan and gray fat clay                          | CH       | 99.9 | 98.6 | 97.4    | 96.5     | 95.7     | 95.1     | 94.7     | 93.0 |
|        | C<br>ST-5 | 8-13<br>13-15 | Tan and gray fat clay                          | CH       |      |      |         |          |          |          |          |      |
|        | 51-5<br>D | 13-15         | Brown and gray fat clay Brown and tan fat clay | СН<br>СН | 100  | 100  | 100     | 99.9<br> | 99.7<br> | 99.4<br> | 99.1<br> | 97.4 |
|        | ST-6      | 18-20         | Tan and gray lean clay                         | CL       | 100  | 99.4 | 99.2    | 99.1     | 98.9     | 98.7     | 98.5     | 97.7 |
|        | 51-0      | 10-20         |  | 0L       | 100  | 33.4 | 33.2    | 33.1     | 30.3     | 30.7     | 30.5     | 51.1 |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |
|        |           |               |  |          |      |      |         |          |          |          |          |      |

|        |        |           | SUMMARY OF LABORATORY TEST RESULTS  |    |          |        |    |       |      |          |
|--------|--------|-----------|---|----|----------|--------|----|-------|------|----------|
|        |        |           | LABORATORY TESTING SERVICES   |    |          | 1      |    |       |      |          |
|        |        |           | NTSB Dallas Pipeline  |    |          |        |    |       |      |          |
|        |        | г г       | Dallas, Texas   |    |          |        | 1  |       |      |          |
|        |        | Sample    |   |    | Moisture |        |    | terbe |      |          |
| Boring | Sample | Depth     | Visual Description &  |    | Content  | Weight |    | _imit |      | <u> </u> |
| No.    | No.    | (ft.)     | Unified Soil Classification (ASTM D-2487/2488)                            |    | (%)      | (pcf)  | LL | PL    | PI   | Remarks  |
| B-1    | ST-1   | 2-4       | Gray fat clay   | СН | 25.3     | 99.6   | 63 | 24    | 39   | (1)      |
|        | Α      | 2-4       | Gray fat clay   | СН | 26.4     |        |    |       |      |          |
|        | В      | 4-8       | Light brown fat clay  | СН | 25.0     |        |    |       |      |          |
|        | ST-2   | 8-10      | Tan and gray fat clay   | СН | 22.1     | 101.4  | 55 | 22    | 33   | (1)      |
|        | C      | 8-13      | Tan and gray fat clay   | СН | 23.9     |        |    |       |      |          |
|        | D      | 13-17.1   | Tan and gray fat clay   | СН | 26.6     |        |    |       |      |          |
|        | E      | 17.1-17.9 | Tan and gray lean clay with sand  | CL | 17.5     |        |    |       |      |          |
|        | F      | 18-20     | Tan silty sand  | SM | 9.6      |        | No | n-Pla | stic |          |
|        |        |           |   |    |          |        |    |       |      |          |
| B-2    | ST-1   | 2-4       | Gray and dark brown fat clay  | СН | 26.6     | 97.7   | 61 | 25    | 36   | (1)      |
|        | A      | 2-5.7     | Dark gray fat clay  | СН | 26.1     |        |    |       |      |          |
|        | ST-2   | 4-6       | Gray and dark gray fat clay   | СН | 21.7     | 103.0  | 57 | 21    | 36   | (1)      |
|        | В      | 5.7-8     | Light gray fat clay   | СН | 19.4     |        |    |       |      |          |
|        | ST-3   | 8-10      | Tan and gray lean clay  | CL | 17.8     |        | 46 | 18    | 28   |          |
|        | C      | 8-11.3    | Tan and gray fat clay   | СН | 20.8     |        |    |       |      |          |
|        | D      | 11.3-12.1 | Tan lean clay with sand   | CL | 14.7     |        |    |       |      |          |
|        | ST-4   | 13-15     | Tan and gray fat clay   | СН | 21.2     | 98.0   | 60 | 20    | 40   | (1)      |
|        | E      | 13-18     | Brown and gray fat clay   | СН | 23.3     |        |    |       |      |          |
|        | F      | 18-20     | Brown and gray fat clay   | СН | 21.4     |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
| B-4    | A      | 1-5       | Gray fat clay   | СН | 26.3     |        |    |       |      |          |
|        | ST-1   | 1-3       | Gray and dark brown fat clay  | СН | 25.8     | 98.1   | 64 | 24    | 40   | (1)      |
|        | ST-2   | 3-5       | Gray and brown fat clay   | СН | 26.0     |        | 64 | 23    | 41   |          |
|        | ST-3   | 5-7       | Brown and gray fat clay   | СН | 24.5     | 100.0  | 61 | 22    | 39   | (1)      |
|        | В      | 5-7       | Tan and gray fat clay   | СН | 22.7     |        |    |       |      |          |
|        | ST-4   | 8-10      | Tan and gray fat clay   | СН | 20.7     | 104.8  | 52 | 20    | 32   | (1)      |
|        | С      | 8-13      | Tan and gray fat clay   | СН | 22.7     |        |    |       |      |          |
|        | ST-5   | 13-15     | Brown and gray fat clay   | СН | 19.1     |        | 51 | 18    | 33   |          |
|        | D      | 13-18     | Brown and tan fat clay  | СН | 22.0     |        |    |       |      |          |
|        | ST-6   | 18-20     | Tan and gray lean clay  | CL | 19.8     | 105.7  | 45 | 18    | 27   | (1)      |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           | (1) See attached "Laboratory Data Sheets" for Consolidation Test results. |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |
|        |        |           |   |    |          |        |    |       |      |          |



PARTICLE SIZE ANALYSIS (ASTM D-422)



TEAM Consultants, Inc.

Geotechnical, Environmental, Construction Materials Testing

|                 |   |                 |                                      |                 | IDATION TE.<br>cimen Data)       | ST                      |          |                 |            |
|-----------------|---|-----------------|--------------------------------------|-----------------|----------------------------------|-------------------------|----------|-----------------|------------|
| Pr              | oject: USAC   | ΈΔΤΜ            | OS Pipeline                          |                 |                                  | TEAM Job I              | No ·     | 1920            | 131        |
|                 | -   | , ∧ ⊓м<br>-1    | Sample No                            | o.: ST-1        | Depth:                           | 2-4'                    | Date:    | 3/15            |            |
| Class           | rification Grav   | fat clay        |                                      |                 |                                  |                         |          |                 |            |
| Class           | ification Gray  | Tat Clay        |                                      | Be              | efore Test                       |                         |          |                 | After Test |
|                 |   |                 | Sr                                   | ecimen          |                                  | Trimmings               |          |                 | Specimen   |
|                 | Tare No.  |                 |                                      | and Plates      |                                  | 625                     |          |                 | 451        |
| S               | Tare plus wet   | soil            |                                      | 191.03          |                                  |                         |          | 113.03          |            |
| jram            | Tare plus dry   |                 |                                      | 74.76           |                                  | 582.91<br>507.24        |          |                 | 98.57      |
| Weight in grams | Water   | Ww              |                                      | 16.27           |                                  | 75.67                   |          | W <sub>wf</sub> | 14.46      |
| eigh            | Tare  |                 |                                      | 10.46           |                                  | 208.30                  |          |                 | 34.27      |
| Š               | Dry soil  | Ws              |                                      | 64.30           |                                  | 298.94                  |          |                 | 64.30      |
| W               | ater Content  | w               | W <sub>O</sub> 2                     | 5.31%           |                                  | 25.31%                  |          | W <sub>f</sub>  | 22.49%     |
| C               | Consolidometer No   |                 |                                      | 5               | Area                             | of specimen, A          | , (sq. c | m.)             | 31.67      |
|                 | Weight of ring, g   |                 |                                      | N/A             | Heig                             | ht of specimen,         | H, (i    | n.)             | 0.501      |
|                 | Weight of plates, g   |                 |                                      | N/A             | Spec                             | ific Gravity of so      | lids, (  | Gs)             | 2.698      |
| Final<br>Net c  | nal height of water<br>height of water, H<br>change in height of<br>ht of specimen at e | wf =<br>specime | $\frac{W_{Wf}}{A \times \gamma_W} =$ | 31<br>est, ΔH = | 14.46<br>.67 x 1 x 2<br>-0.02500 | x 2.54<br>2.54 =<br>in. | 0.1798   | 3 in.           |            |
|                 | ratio before test, e<br>ratio after test, e <sub>f</sub>                                |                 |                                      | 0.2963          |                                  | = 0.6911<br>= 0.6067    |          |                 |            |
|                 | ee of saturation be   |                 |                                      |                 |                                  |                         | 98.8     |                 |            |
|                 | ee of saturation aff  |                 |                                      |                 |                                  |                         |          |                 | .ft.       |
| Rema            | arks  |                 |                                      |                 |                                  |                         |          |                 |            |
| Tech            | nician Jas  | on Youn         | g Co                                 | omputed by      | Jason                            | Young                   | Chec     | ked by _        | James Hutt |

| _             |                 |              | TE                     | AM C                                   | Cons        | sulte        | ants            | s, In          | с.                     |  |             |
|---------------|-----------------|--------------|------------------------|--|-------------|--------------|-----------------|----------------|------------------------|--|-------------|
|               |                 | Ge           | eotechnica             | l, Environn                            |             |              |                 | Materia        | ls Testing             |  |             |
|               |                 |              |                        | CONSO                                  | LIDATI      | ON TES       | Т               |                |                        |  |             |
|               |                 |              |                        | (Time - C                              | onsolid     | ation Da     | ta)             |                |                        |  |             |
|               |                 |              |                        |  |             |              |                 |                |                        |  |             |
| Proje         | ct:             | USA          | CE, ATMOS              | Pipeline                               |             |              |                 | TEA            | M Job No.:             | 192031                                 | _           |
| Borin         | a No.:          |              | B-1                    | Sample No                              | .: ST       | [-1 De       | epth:           | 2-4'           | Consol.No.:            | 5                                      | •           |
|               |                 |              |                        |  |             |              | · -             |                |                        |  |             |
| Date          | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time           | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/15          | 0.25            | 11:00        | 0                      | 2003                                   | 20          | 3/19         | 4               | 8:50           | 0                      | 2098.8                                 | 20          |
| 3/15          | 0.5             | 11:05        | 5                      | 2002                                   |             | 3/19         | 4               | 8:50           | 0.05                   | 2119                                   |             |
| 3/15          | 0.75            | 11:40        | 40                     | 2010                                   |             | 3/19         | 4               | 8:50           | 0.1                    | 2121.5                                 |             |
| 3/18          | 0.75            | 8:00         | 4140                   | 2020                                   | 19          | 3/19         | 4               | 8:50           | 0.2                    | 2124                                   |             |
|               |                 |              |                        |  |             | 3/19         | 4               | 8:50           | 0.33                   | 2126                                   |             |
|               |                 |              |                        |  |             | 3/19         | 4               | 8:50           | 0.5                    | 2128                                   |             |
|               |                 |              |                        |  |             | 3/19         | 4               | 8:50           | 0.75                   | 2130                                   |             |
|               |                 |              | _                      |  | 10          | 3/19         | 4               | 8:51           | 1                      | 2132                                   |             |
| 3/18          | 2               | 8:45         | 0                      | 2020                                   | 19          | 3/19         | 4               | 8:52           | 2                      | 2136.5                                 |             |
| 3/18          | 2               | 8:45         | 0.05                   | 2043.5                                 |             | 3/19         | 4               | 8:54           | 4                      | 2143.2                                 |             |
| 3/18          | 2               | 8:45         | 0.1                    | 2045                                   |             | 3/19         | 4               | 8:58           | 8                      | 2151                                   |             |
| 3/18          | 2               | 8:45         | 0.2                    | 2046.2                                 |             | 3/19         | 4               | 9:05           | 15                     | 2162.5                                 |             |
| 3/18          | 2               | 8:45         | 0.33                   | 2047.2                                 |             | 3/19         | 4               | 9:20           | 30                     | 2174.2                                 |             |
| 3/18          | 2               | 8:45         | 0.5                    | 2049                                   |             | 3/19         | 4               | 9:50           | 60                     | 2188                                   |             |
| 3/18          | 2               | 8:45         | 0.75                   | 2050.5                                 |             | 3/19<br>3/19 | 4               | 10:30          | 100                    | 2197                                   |             |
| 3/18          | 2               | 8:46<br>8:47 | 1                      | 2052                                   |             | 3/19         | 4               | 12:10<br>13:50 | 200                    | 2207.2                                 |             |
| 3/18<br>3/18  | 2               | 8:49         | 2                      | 2055                                   |             | 3/19         | 4               |                | 300                    | 2212                                   |             |
| 3/18          | 2               | 8:53         | 4                      | 2059.5                                 |             | 3/19         | 4               | 17:15<br>9:05  | 505<br>1455            | 2216                                   | 20          |
| 3/18          | 2               | 9:00         | <u>ہ</u><br>15         | 2065<br>2070.5                         |             | 3/20         | 4               | 9.05           | 1400                   | 2219                                   | 20          |
| 3/18          | 2               | 9:15         | 30                     | 2070.3                                 |             |              |                 |                |                        |  |             |
| 3/18          | 2               | 9:50         | <u> </u>               | 2077.8                                 |             |              |                 |                |                        |  |             |
| 3/18          | 2               | 10:35        | 110                    | 2084.8                                 |             |              |                 |                |                        |  |             |
| 3/18          | 2               | 12:05        | 200                    | 2000.2                                 |             |              |                 |                |                        |  |             |
| 3/18          | 2               | 13:45        | 300                    | 2094.2                                 |             |              |                 |                |                        |  |             |
| 3/18          | 2               | 18:15        | 570                    | 2094.2                                 |             |              |                 |                |                        |  |             |
| 3/19          | 2               | 8:50         | 1445                   | 2098.8                                 | 20          |              |                 |                |                        |  |             |
|               | _               |              | 1410                   | 2000.0                                 |             |              |                 |                |                        |  |             |
|               |                 |              |                        |  |             |              |                 |                |                        |  |             |
|               |                 |              |                        |  |             |              |                 |                |                        |  |             |
|               |                 |              |                        |  |             |              |                 |                |                        |  |             |
|               |                 |              |                        |  |             |              |                 | 1              |                        | 1                                      |             |
| $\rightarrow$ |                 |              |                        |  |             |              |                 |                |                        | 1                                      |             |
|               |                 |              |                        |  | -           | Te           | echnicia        | n <u>Jaso</u>  | n Young                | -                                      |             |

|              |                 |              |                        | AM C                                   |                         |               |                 |              |                        |  |             |
|--------------|-----------------|--------------|------------------------|--|-------------------------|---------------|-----------------|--------------|------------------------|--|-------------|
|              |                 | Ge           | eotechnica             | l, Environn<br>CONSO                   | -                       |               |                 | Materia      | ls Testing             |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        | (Time - C                              | onsolida                | ation Da      | ta)             |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
| Proje        | ect:            | USA          | CE, ATMOS              | Pipeline                               |                         |               |                 | TEA          | M Job No.:             | 192031                                 |             |
| Borin        | g No.:          |              | B-1                    | Sample No                              | .: S                    | <u>Г-1</u> De | epth:           | 2-4'         | Consol.No.:            | 5                                      |             |
|              |                 |              |                        |  |                         |               |                 |              |                        | 1                                      |             |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C | Date          | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/20         | 8               | 9:05         | 0                      | 2219                                   | 20                      | 3/21          | 16              | 8:50         | 0                      | 2388.8                                 | 20          |
| 3/20         | 8               | 9:05         | 0.05                   | 2240                                   |                         | 3/21          | 16              | 8:50         | 0.05                   | 2408                                   |             |
| 3/20         | 8               | 9:05         | 0.1                    | 2242.5                                 |                         | 3/21          | 16              | 8:50         | 0.1                    | 2410                                   |             |
| 3/20         | 8               | 9:05         | 0.2                    | 2244.5                                 |                         | 3/21          | 16              | 8:50         | 0.2                    | 2412                                   |             |
| 3/20         | 8               | 9:05         | 0.33                   | 2246.8                                 |                         | 3/21          | 16              | 8:50         | 0.33                   | 2414                                   |             |
| 3/20<br>3/20 | 8<br>8          | 9:05<br>9:05 | 0.5                    | 2249                                   |                         | 3/21<br>3/21  | 16<br>16        | 8:50<br>8:50 | 0.5                    | 2416.5                                 |             |
| 3/20         | 8               | 9:05         | 0.75                   | 2251.2<br>2253                         |                         | 3/21          | 16              | 8:51         | 0.75<br>1              | 2418.8<br>2420.8                       |             |
| 3/20         | 8               | 9:00         | 1 2                    | 2255                                   |                         | 3/21          | 16              | 8:52         | 2                      | 2420.8                                 |             |
| 3/20         | 8               | 9:09         | 4                      | 2266.8                                 |                         | 3/21          | 16              | 8:54         | 4                      | 2420.5                                 |             |
| 3/20         | 8               | 9:13         | 8                      | 2200.0                                 |                         | 3/21          | 16              | 8:58         | 8                      | 2434                                   |             |
| 3/20         | 8               | 9:20         | 15                     | 2292.8                                 |                         | 3/21          | 16              | 9:05         | 15                     | 2458.8                                 |             |
| 3/20         | 8               | 9:35         | 30                     | 2312                                   |                         | 3/21          | 16              | 9:20         | 30                     | 2481                                   |             |
| 3/20         | 8               | 10:05        | 60                     | 2336                                   |                         | 3/21          | 16              | 9:50         | 60                     | 2510                                   |             |
| 3/20         | 8               | 10:45        | 100                    | 2353                                   |                         | 3/21          | 16              | 10:30        | 100                    | 2530                                   |             |
| 3/20         | 8               | 12:25        | 200                    | 2369.8                                 |                         | 3/21          | 16              | 12:10        | 200                    | 2557.5                                 |             |
| 3/20         | 8               | 14:05        | 300                    | 2376.2                                 |                         | 3/21          | 16              | 13:50        | 300                    | 2568                                   |             |
| 3/20         | 8               | 17:45        | 520                    | 2383.5                                 |                         | 3/21          | 16              | 19:00        | 610                    | 2578.8                                 |             |
| 3/21         | 8               | 8:50         | 1425                   | 2388.8                                 | 20                      | 3/22          | 16              | 9:25         | 1475                   | 2584.5                                 | 20          |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         | <u> </u>      |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         | <u> </u>      |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |               |                 |              |                        |  |             |
|              |                 |              |                        |  |                         | Te            | echnicia        | n Jaso       | n Young                |  |             |

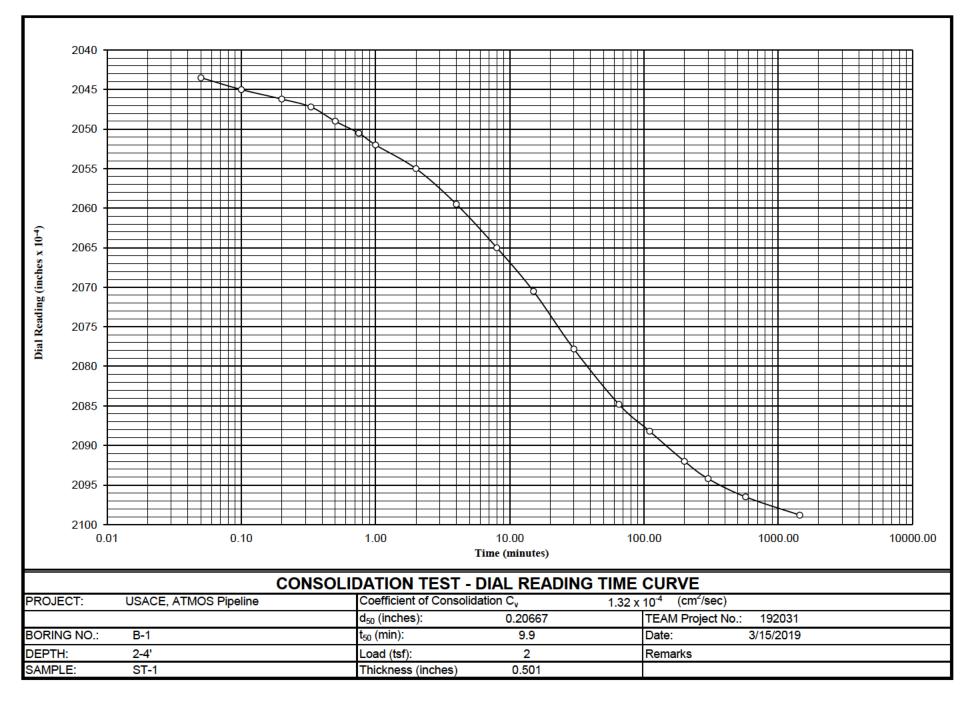
|       |                 |      | TE                     | AM C                                   | Cons          | sulta        | ants            | , In           | С.                     |  |          |
|-------|-----------------|------|------------------------|--|---------------|--------------|-----------------|----------------|------------------------|--|----------|
|       |                 | G    | eotechnica             | l, Environn                            | nental,       | Constru      | uction          | Materia        | ls Testing             |  |          |
|       |                 |      |                        | CONSO                                  |               |              |                 |                |                        |  |          |
|       |                 |      |                        | (Time - C                              | onsolida      | ation Da     | ta)             |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
| Proje | ect:            | USA  | CE, ATMOS              | Pipeline                               |               |              |                 | TEA            | M Job No.:             | 192031                                 |          |
| Borin | ng No.:         |      | B-1                    | Sample No                              | .: <u>S</u> T | <u>-1</u> D€ | epth:           | 2-4'           | Consol.No.:            | 5                                      |          |
|       | Deces           |      | <b>E</b> 1 1           | Dial Deading                           | Tomp          |              | Deres           |                | <b>E</b> 1 1           | Dial Deading                           | Temp.    |
| Date  | Press.<br>(tsf) | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C   | Date         | Press.<br>(tsf) | Time           | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | °C       |
|       |                 |      |                        |  |               |              |                 | RFBO           |                        | )S                                     |          |
|       |                 |      |                        |  |               | 2/22         | 4               |                |                        |  | 20       |
|       |                 |      |                        |  |               | 3/22<br>3/24 | 4               | 9:25<br>14:15  | Rebound<br>3170        | 2584.5<br>2469.2                       | 20<br>20 |
|       |                 |      |                        |  |               | 5/24         | -+              | 14.13          | 5170                   | 2409.2                                 | 20       |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               | 3/24         | 1               | 14:15          | Rebound                | 2469.2                                 | 20       |
|       |                 |      |                        |  |               | 3/25         | 1               | 17:30          | 1635                   | 2348.8                                 | 21       |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               | 2/25         | 0.05            | 47.00          | D.I.                   | 00.40.0                                | 24       |
|       |                 |      |                        |  |               | 3/25<br>3/26 | 0.25            | 17:30<br>15:30 | Rebound<br>1320        | 2348.8<br>2260                         | 21<br>20 |
|       |                 |      |                        |  |               | 3/20         | 0.25            | 15.50          | 1320                   | 2200                                   | 20       |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              | M               | achine D       | eflection Re           | eadings                                |          |
|       |                 |      |                        |  |               |              | 0.25            |                |                        | 2003                                   |          |
|       |                 |      |                        |  |               |              | 0.75            |                |                        | 2012                                   |          |
|       |                 |      |                        |  |               |              | 2               |                |                        | 2029                                   |          |
|       |                 |      |                        |  |               |              | 4               |                |                        | 2041                                   |          |
|       |                 |      |                        |  |               |              | 8               |                |                        | 2054                                   |          |
|       |                 |      |                        |  |               |              | 16              |                |                        | 2067                                   |          |
|       |                 |      |                        |  |               |              | 4               |                |                        | 2050<br>2028                           |          |
|       |                 |      |                        |  |               |              | 0.25            |                |                        | 2028                                   |          |
|       |                 |      |                        |  |               |              | 0.20            |                |                        | 2010                                   |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               |              |                 |                |                        |  |          |
|       |                 |      |                        |  |               | Te           | echniciar       | n <u>Jaso</u>  | n Young                |  |          |

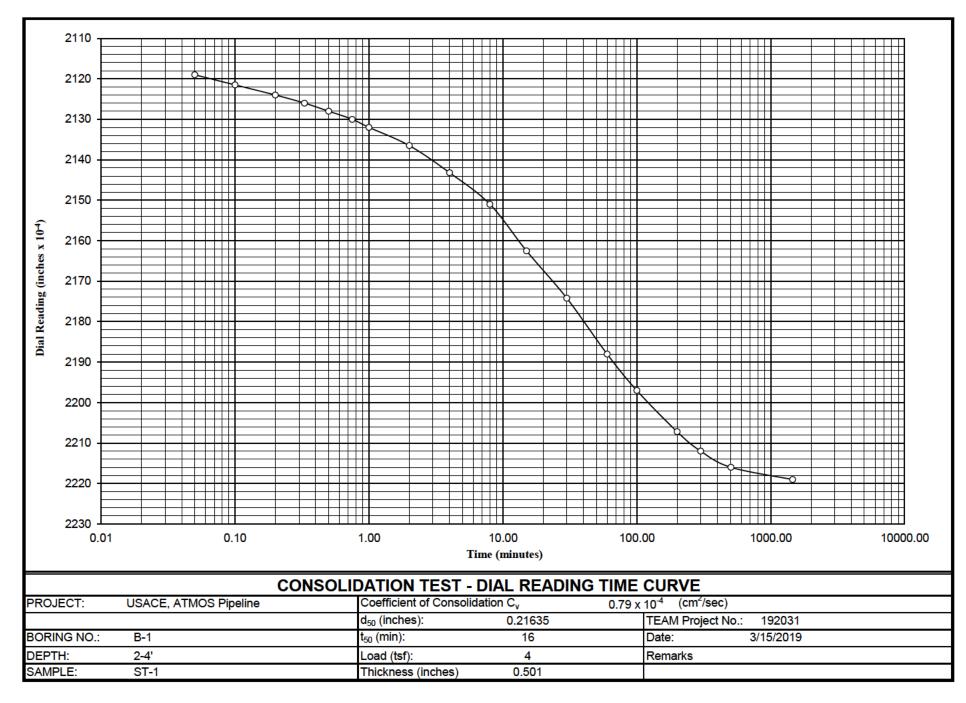
Geotechnical, Environmental, Construction Materials Testing

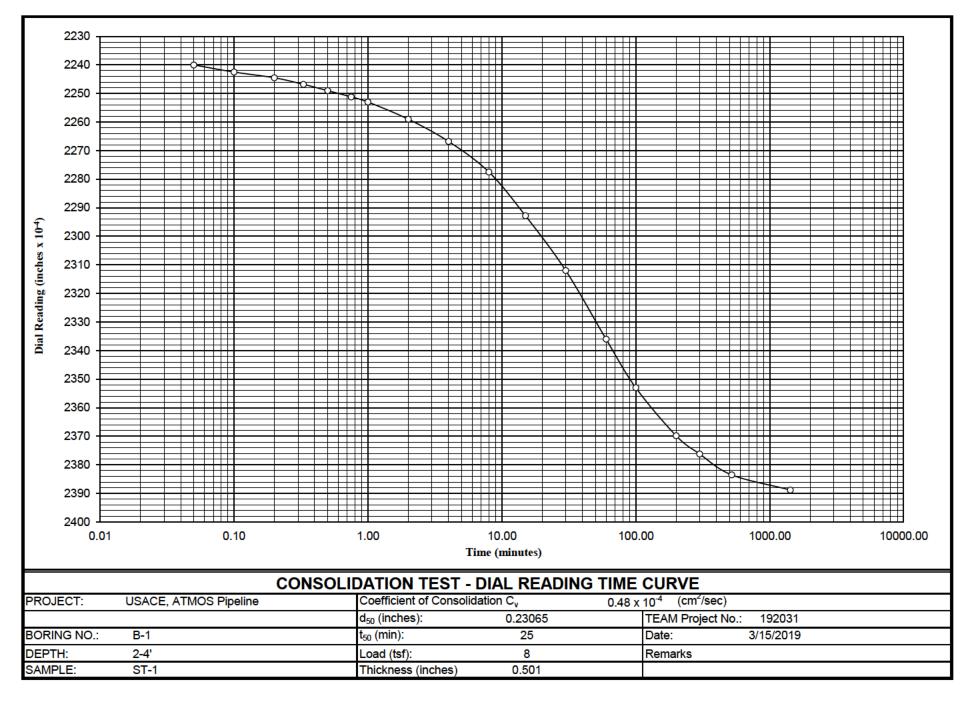
#### CONSOLIDATION TEST

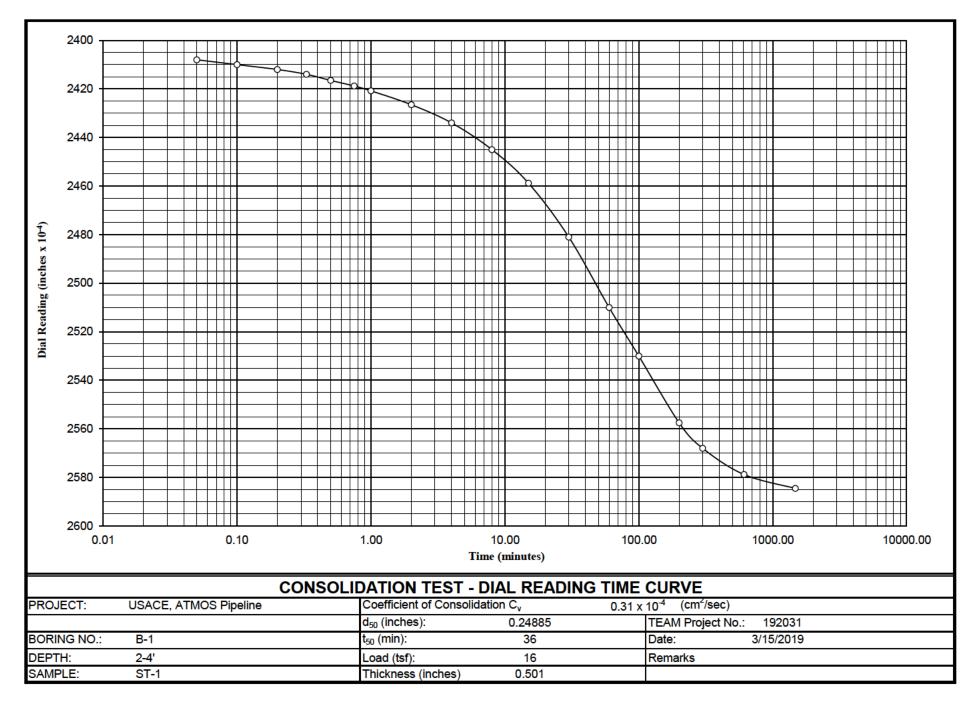
(Computation of Void Ratio)

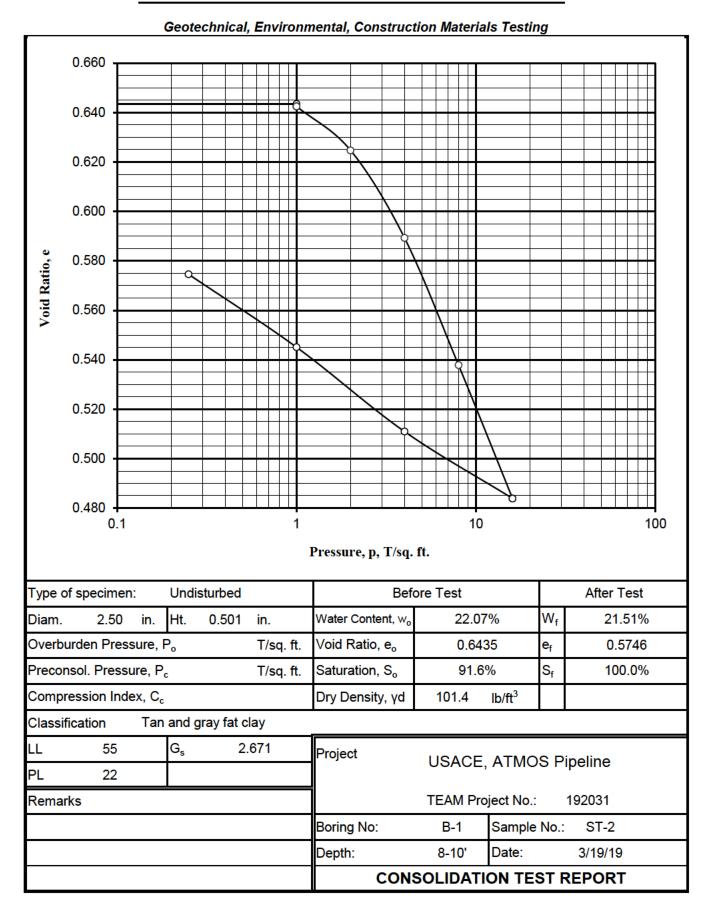
| PROJECT                  | USACE, A   | TMOS Pipeline                          | TEA                               | M Job No.:                         | 192031                                      | DATE:                   | 3/15/19       |
|--------------------------|--|--|-----------------------------------|------------------------------------|---|-------------------------|---------------|
|                          | B-1  | SAMP                                   | PLE NO. ST-1                      | DEPTH                              | 2-4'  | CONSOLIDOMETER NO.      | 5             |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied                     | Time in Min.<br>Increment<br>Effective | Dial Reading 10 <sup>-4</sup> in. | Correction<br>10 <sup>-4</sup> in. | Change<br>Height, Δ<br>10 <sup>-4</sup> in. | H Voids, H <sub>V</sub> | Void Ratio, e |
| 0.1                      | 3/15   | Zero Point                             | 2000                              | 2000                               | 0   | 2047                    | 0.6911        |
| 0.75                     | 3/15   | Initial Load                           | 2012                              | 2012                               | 0   | 2047                    | 0.6911        |
| 0.75                     | 3/15   | 4140                                   | 2020                              | 2012                               | -8  | 2039                    | 0.6884        |
| 2                        | 3/18   | 1445                                   | 2098.8                            | 2029                               | -69.8                                       | 1978                    | 0.6675        |
| 4                        | 3/19   | 1455                                   | 2219                              | 2041                               | -178  | 1869                    | 0.6310        |
| 8                        | 3/20   | 1425                                   | 2388.8                            | 2054                               | -334.8                                      | 1713                    | 0.5781        |
| 16                       | 3/21   | 1475                                   | 2584.5                            | 2067                               | -517.5                                      | 1530                    | 0.5164        |
| 4                        | 3/22   | 3170                                   | 2469.2                            | 2050                               | -419.2                                      | 1628                    | 0.5496        |
| 1                        | 3/24   | 1635                                   | 2348.8                            | 2028                               | -320.8                                      | 1727                    | 0.5828        |
| 0.25                     | 3/25   | 1320                                   | 2260                              | 2010                               | -250  | 1797                    | 0.6067        |
| Note:                    |  |  |                                   |                                    |   |                         |               |
|                          | bids, $H_V = (H - H_S)$<br>$e = \frac{H_V}{H_S}$ |  | H <sub>S</sub> = 0.2963           |                                    | hv. Jason Youn                              | g Checked by James      | Hutt          |











Geotechnical, Environmental, Construction Materials Testing

|  |                     |                       |   | SOLIDATION TE<br>Specimen Data) | EST                              |          |            |  |
|--|---------------------|-----------------------|---|---------------------------------|----------------------------------|----------|------------|--|
| Project: USACE, ATMOS Pipeline TEAM Job No.:   |                     |                       |   |                                 |                                  |          | 192031     |  |
|  |                     | -1                    | Sample No.: <u>ST-2</u> Depth: <u>8-10'</u> Dat   |                                 |                                  |          |            |  |
| Class  | sification Tan      | and drav              | / fat clay  |                                 |                                  |          |            |  |
| 01033  |                     | and gray              | lat day   | Before Test                     |                                  |          | After Test |  |
|  |                     |                       | Specimen  | Delote rest                     | Trimmings                        |          | Specimen   |  |
| Tare No.   |                     |                       | Ring and Plates                                   |                                 | 626                              |          | 430        |  |
| Weight in grams  | Tare plus wet soil  |                       | 189.96  |                                 | 532.47                           |          | 114.99     |  |
|  | Tare plus dry soil  |                       | 175.50  |                                 | 472.29                           |          | 100.90     |  |
|  | Water               | Ww                    | W <sub>WO</sub> 14.46                             |                                 |                                  | Wwf      | 14.09      |  |
| aight  | Tare                |                       | 110.00  |                                 | 199.63                           |          | 35.40      |  |
| Ň  | Dry soil            | Ws                    | 65.50   |                                 | 272.66                           |          | 65.50      |  |
| Water Content w  |                     | W <sub>0</sub> 22.07% |   | 22.07%                          |                                  | 21.51%   |            |  |
| Consolidometer No .:   |                     |                       | 3   | Area                            | Area of specimen, A, (sq. c      |          | 31.67      |  |
| Weight of ring, g  |                     |                       | N/A   | Heig                            | Height of specimen, H, (in.)     |          | 0.501      |  |
| Weight of plates, g  |                     |                       | N/A   | Spec                            | Specific Gravity of solids, (Gs) |          | 2.671      |  |
| Final height of water, $H_{Wf} = \frac{W_{Wf}}{A \times \gamma_W} = \frac{14.09}{31.67 \times 1 \times 2.54} = 0.1752$ in.<br>Net change in height of specimen at end of test, $\Delta H = -0.02100$ in.<br>Height of specimen at end of test, $H_f = H - \Delta H = 0.4800$ in. |                     |                       |   |                                 |                                  |          |            |  |
| Void ratio before test, $e_0 = = \frac{H - H_s}{H_s} = \frac{0.501 - 0.3048}{0.3048} = 0.6435$<br>Void ratio after test, $e_f = \frac{H_f - H_s}{H_s} = \frac{0.48 - 0.3048}{0.3048} = 0.5746$   |                     |                       |   |                                 |                                  |          |            |  |
|  |                     |                       | $H_{\rm WO} = \frac{H_{\rm WO}}{H - H_{\rm S}} =$ |                                 |                                  | .6%      |            |  |
| Degr   | ee of saturation af | ter test,             | $S_{f} = \frac{H_{wf}}{H_{f} - H_{S}} = -$        | 0.1752                          | 3048 = 100.0                     | %        |            |  |
|  |                     |                       | $\frac{W_s}{H x A} = \frac{65}{0.507}$            |                                 |                                  | 4 lb./cu | ı.ft.      |  |
| Rema   | arks                |                       |   |                                 |                                  |          |            |  |
| Tech   | nician Jas          | on Your               | g Computed by                                     | Jason                           | Young Che                        | cked by  | James Hutt |  |

| Projec       | at:             | Ge            | eotechnica             | l, Environn                            | nental,     | Consta       |                 | 1 4           | 1 T                    |  |             |
|--------------|-----------------|---------------|------------------------|--|-------------|--------------|-----------------|---------------|------------------------|--|-------------|
| -            | st:             |               |                        |  |             |              |                 | Maleria       | ls Testing             |  |             |
| -            | et:             |               |                        | CONSO                                  |             | ON TES       |                 |               |                        |  |             |
| -            | ot:             |               |                        | (Time - C                              | onsolida    | ation Da     | ta)             |               |                        |  |             |
| -            | et:             |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 | USA           | CE, ATMOS              | Pipeline                               |             |              |                 | TEA           | M Job No.:             | 192031                                 |             |
| Boring       | No.:            |               | B-1                    | Sample No                              | .: S1       | [-2 De       | epth: 8         | 8-10'         | Consol.No.:            | 3                                      |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
| Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/19         | 0.125           | 10:30         | 0                      | 2003                                   | 20          | 3/21         | 4               | 8:40          | 0                      | 2099.2                                 |             |
| 3/19         | 0.25            | 10:31         | 1                      | 1998                                   |             | 3/21         | 4               | 8:40          | 0.05                   | 2140.5                                 |             |
| 3/19         | 0.5             | 10:32         | 2                      | 2006                                   |             | 3/21         | 4               | 8:40          | 0.1                    | 2144.8                                 |             |
| 3/19         | 0.75            | 12:00         | 90                     | 2008                                   |             | 3/21         | 4               | 8:40          | 0.2                    | 2149.8                                 |             |
| 3/19         | 1               | 12:30         | 120                    | 2019                                   |             | 3/21         | 4               | 8:40          | 0.33                   | 2153.5                                 |             |
| 3/20         | 1               | 8:55          | 1345                   | 2031                                   | 20          | 3/21         | 4               | 8:40          | 0.5                    | 2157                                   |             |
|              |                 |               |                        |  |             | 3/21         | 4               | 8:40          | 0.75                   | 2160.2                                 |             |
|              |                 |               |                        |  |             | 3/21         | 4               | 8:41          | 1                      | 2162.5                                 |             |
| 3/20         | 2               | 8:55          | 0                      | 2031                                   | 20          | 3/21         | 4               | 8:42          | 2                      | 2168.8                                 |             |
| 3/20         | 2               | 8:55          | 0.05                   | 2053.5                                 |             | 3/21         | 4               | 8:44          | 4                      | 2175.5                                 |             |
| 3/20         | 2               | 8:55          | 0.1                    | 2057                                   |             | 3/21         | 4               | 8:48          | 8                      | 2183.2                                 |             |
| 3/20         | 2               | 8:55          | 0.2                    | 2059                                   |             | 3/21         | 4               | 8:55          | 15                     | 2191.2                                 |             |
| 3/20         | 2               | 8:55          | 0.33                   | 2061.5                                 |             | 3/21         | 4               | 9:10          | 30                     | 2199.2                                 |             |
| 3/20         | 2               | 8:55          | 0.5                    | 2063                                   |             | 3/21         | 4               | 9:40          | 60                     | 2206                                   |             |
| 3/20         | 2               | 8:55          | 0.75                   | 2065                                   |             | 3/21         | 4               | 10:20         | 100                    | 2210.8                                 |             |
| 3/20         | 2               | 8:56          | 1                      | 2066.5                                 |             | 3/21         | 4               | 12:00         | 200                    | 2215                                   |             |
| 3/20         | 2               | 8:57          | 2                      | 2070                                   |             | 3/21         | 4               | 13:40         | 300                    | 2217.5                                 |             |
| 3/20<br>3/20 | 2               | 8:59<br>9:03  | 4                      | 2074                                   |             | 3/21<br>3/22 | 4               | 19:00<br>9:35 | 620                    | 2221                                   | 20          |
| 3/20         | 2               | 9:03<br>9:10  | 8<br>15                | 2078                                   |             | 3/22         | 4               | 9.35          | 1495                   | 2224.2                                 | 20          |
| 3/20         | 2               | 9:10          | 30                     | 2081.8<br>2085.5                       |             |              |                 |               |                        |  |             |
| 3/20         | 2               | 9.25<br>9:55  | <u> </u>               | 2085.5                                 |             |              |                 |               |                        |  |             |
| 3/20         | 2               | 9.33<br>10:35 | 100                    | 2009                                   |             |              |                 |               |                        |  |             |
| 3/20         | 2               | 12:15         | 200                    | 2091.5                                 |             |              |                 |               |                        |  |             |
| 3/20         | 2               | 13:55         | 300                    | 2094                                   |             |              |                 |               |                        |  |             |
| 3/20         | 2               | 17:45         | 530                    | 2093.5                                 |             |              |                 |               |                        |  |             |
| 3/21         | 2               | 8:40          | 1425                   | 2097.3                                 | 20          |              |                 |               |                        |  |             |
|              | -               | 0.10          | 1720                   | 2000.2                                 |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             |              |                 |               |                        |  |             |
|              |                 |               |                        |  |             | Te           | echnicia        | n Jasoi       | n Young                |  |             |

|              |                 |              |                        | AM C                                   |                         |                |                 | -            |                        |  |             |
|--------------|-----------------|--------------|------------------------|--|-------------------------|----------------|-----------------|--------------|------------------------|--|-------------|
|              |                 | Ge           | eotechnica             | l, Environn                            | _                       |                |                 | Materia      | ls Testing             |  |             |
|              |                 |              |                        | CONSO                                  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        | (Time - C                              | onsolid                 | ation Da       | ta)             |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
| Proje        | ect:            | USA          | CE, ATMOS              | Pipeline                               |                         |                |                 | TEA          | M Job No.:             | 192031                                 |             |
| Borin        | ng No.:         |              | B-1                    | Sample No                              | .: <u>S</u>             | Г <u>-2</u> De | epth: 8         | 8-10'        | Consol.No.:            | 3                                      |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C | Date           | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/22         | 8               | 9:35         | 0                      | 2224.2                                 | 20                      | 3/25           | 16              | 8:45         | 0                      | 2402                                   | 21          |
| 3/22         | 8               | 9:35         | 0.05                   | 2281                                   |                         | 3/25           | 16              | 8:45         | 0.05                   | 2445.5                                 |             |
| 3/22         | 8               | 9:35         | 0.1                    | 2285.5                                 |                         | 3/25           | 16              | 8:45         | 0.1                    | 2448.8                                 |             |
| 3/22         | 8               | 9:35         | 0.2                    | 2290                                   |                         | 3/25           | 16              | 8:45         | 0.2                    | 2452.5                                 |             |
| 3/22         | 8               | 9:35         | 0.33                   | 2293.8                                 |                         | 3/25           | 16              | 8:45         | 0.33                   | 2455.8                                 |             |
| 3/22         | 8<br>8          | 9:35<br>9:35 | 0.5                    | 2298                                   |                         | 3/25<br>3/25   | 16<br>16        | 8:45<br>8:45 | 0.5                    | 2458.8                                 |             |
| 3/22<br>3/22 | 8               | 9:35<br>9:36 | 0.75<br>1              | 2300.8<br>2303                         |                         | 3/25           | 16              | 8:45<br>8:46 | 0.75<br>1              | 2462<br>2464.5                         |             |
| 3/22         | 8<br>8          | 9:30         | 1                      | 2303                                   |                         | 3/25           | 16              | 8:46         | 2                      | 2464.5                                 |             |
| 3/22         | 0<br>8          | 9.37<br>9:40 | 2<br>5                 | 2309.8                                 |                         | 3/25           | 16              | 8:49         | 4                      | 2472                                   |             |
| 3/22         | 8               | 9:45         | 10                     | 2321.0                                 |                         | 3/25           | 16              | 8:53         | 8                      | 2496.2                                 |             |
| 3/22         | 8               | 9:50         | 15                     | 2332.5                                 |                         | 3/25           | 16              | 9:00         | 15                     | 2512.8                                 |             |
| 3/22         | 8               | 10:05        | 30                     | 2355                                   |                         | 3/25           | 16              | 9:15         | 30                     | 2534                                   |             |
| 3/22         | 8               | 10:35        | 60                     | 2368.5                                 |                         | 3/25           | 16              | 9:45         | 60                     | 2552                                   |             |
| 3/22         | 8               | 11:15        | 100                    | 2376                                   |                         | 3/25           | 16              | 10:25        | 100                    | 2564.5                                 |             |
| 3/22         | 8               | 12:55        | 200                    | 2383                                   |                         | 3/25           | 16              | 12:05        | 200                    | 2576                                   |             |
| 3/22         | 8               | 14:55        | 320                    | 2387                                   |                         | 3/25           | 16              | 13:45        | 300                    | 2580.2                                 |             |
| 3/22         | 8               | 19:00        | 565                    | 2391                                   |                         | 3/25           | 16              | 17:30        | 525                    | 2585.2                                 |             |
| 3/25         | 8               | 8:45         | 4270                   | 2402                                   | 21                      | 3/26           | 16              | 8:30         | 1425                   | 2592.5                                 | 20          |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         |                |                 |              |                        |  |             |
|              |                 |              |                        |  |                         | Т.             | obnisis         |              | n Voung                |  |             |
|              |                 |              |                        |  |                         | 16             | cnnicial        | n Jaso       | n Young                |  |             |

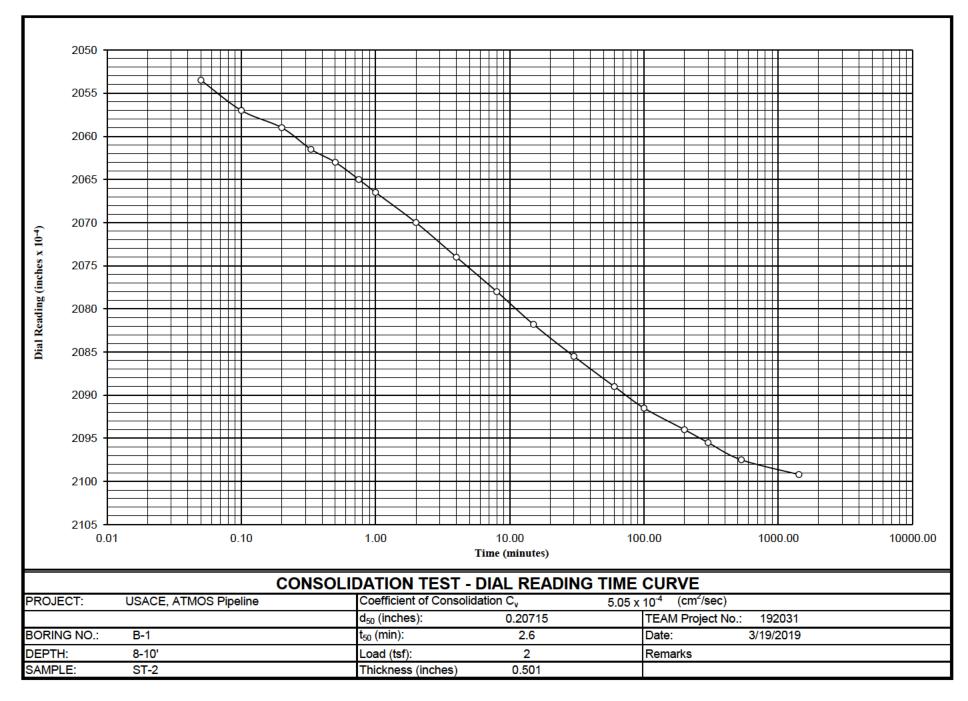
|       |                 |      | TE                     | AM C                                   | Cons                    | sulta        | ants            | , In          | С.                     |  |                         |
|-------|-----------------|------|------------------------|--|-------------------------|--------------|-----------------|---------------|------------------------|--|-------------------------|
|       |                 | G    | eotechnica             | l, Environn                            | iental,                 | Constru      | uction 1        | Materia       | ls Testing             |  |                         |
|       |                 |      |                        | CONSO                                  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        | (Time - C                              | onsolida                | ation Da     | ta)             |               |                        |  |                         |
|       |                 |      |                        | ,                                      |                         |              | ,               |               |                        |  |                         |
| Proje | ect:            | USA  | CE, ATMOS              | Pipeline                               |                         |              |                 | TEA           | M Job No.:             | 192031                                 |                         |
| -     |                 |      |                        |  |                         |              |                 |               |                        | 3                                      | •                       |
|       | <u> </u>        |      |                        |  |                         |              | <u> </u>        |               |                        |  | ·                       |
| Date  | Press.<br>(tsf) | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>O</sup> C | Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>O</sup> C |
|       |                 |      |                        |  |                         |              |                 | REBO          | DUND LOAD              |  |                         |
|       |                 |      |                        |  |                         |              |                 |               | -                      |  |                         |
|       |                 |      |                        |  |                         | 3/26         | 4               | 8:30          | Rebound                | 2592.5                                 | 20                      |
|       |                 |      |                        |  |                         | 3/27         | 4               | 7:30          | 1380                   | 2475                                   | 20                      |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         | 3/27         | 1               | 7:30          | Rebound                | 2475                                   | 20                      |
|       |                 |      |                        |  |                         | 3/28         | 1               | 8:45          | 1515                   | 2343                                   | 20                      |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         | 0/00         | 0.05            | 0.45          |                        |  |                         |
|       |                 |      |                        |  |                         | 3/28<br>3/29 | 0.25            | 8:45<br>12:30 | Rebound                | 2343<br>2232                           | 20<br>20                |
|       |                 |      |                        |  |                         | 3/29         | 0.25            | 12.30         | 1665                   | 2232                                   | 20                      |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              | Ma              | achine D      | Deflection Re          | adings                                 |                         |
|       |                 |      |                        |  |                         |              | 0.125           |               |                        | 2003                                   |                         |
|       |                 |      |                        |  |                         |              | 1               |               |                        | 2028                                   |                         |
|       |                 |      |                        |  |                         |              | 2               |               |                        | 2042                                   |                         |
|       |                 |      |                        |  |                         |              | 4               |               |                        | 2059                                   |                         |
|       |                 |      |                        |  |                         |              | 8<br>16         |               |                        | 2080<br>2106                           |                         |
|       |                 |      |                        |  |                         |              | 4               |               |                        | 2106                                   |                         |
|       |                 |      |                        |  |                         |              | 1               |               |                        | 2043                                   |                         |
|       |                 |      |                        |  |                         |              | 0.25            |               |                        | 2022                                   |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         |              |                 |               |                        |  |                         |
|       |                 |      |                        |  |                         | Τe           | echniciar       | n <u>Jaso</u> | n Young                |  |                         |

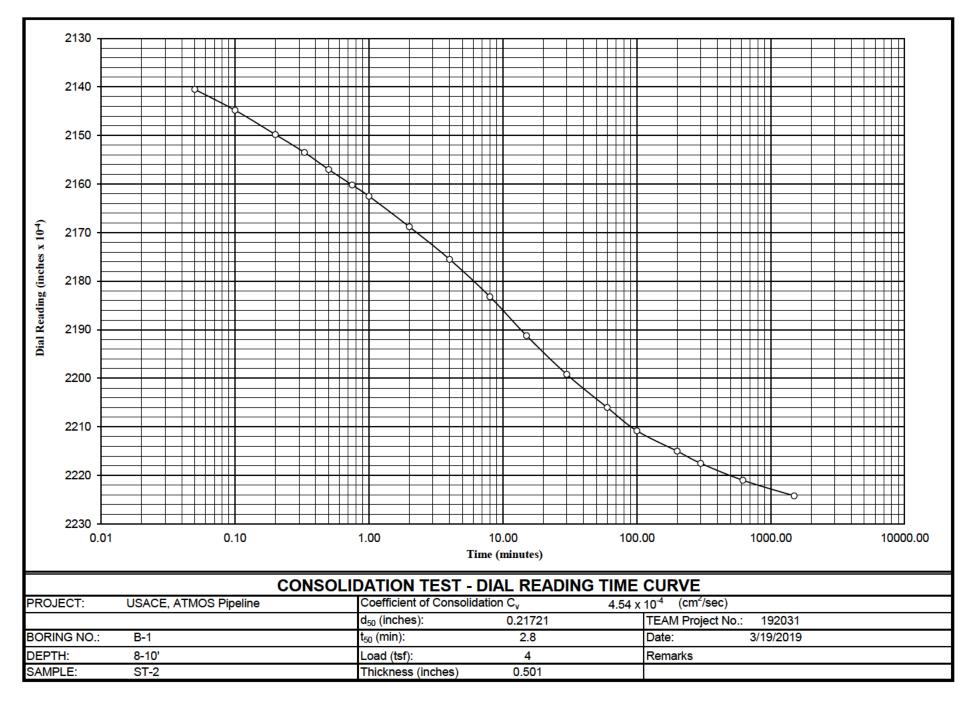
Geotechnical, Environmental, Construction Materials Testing

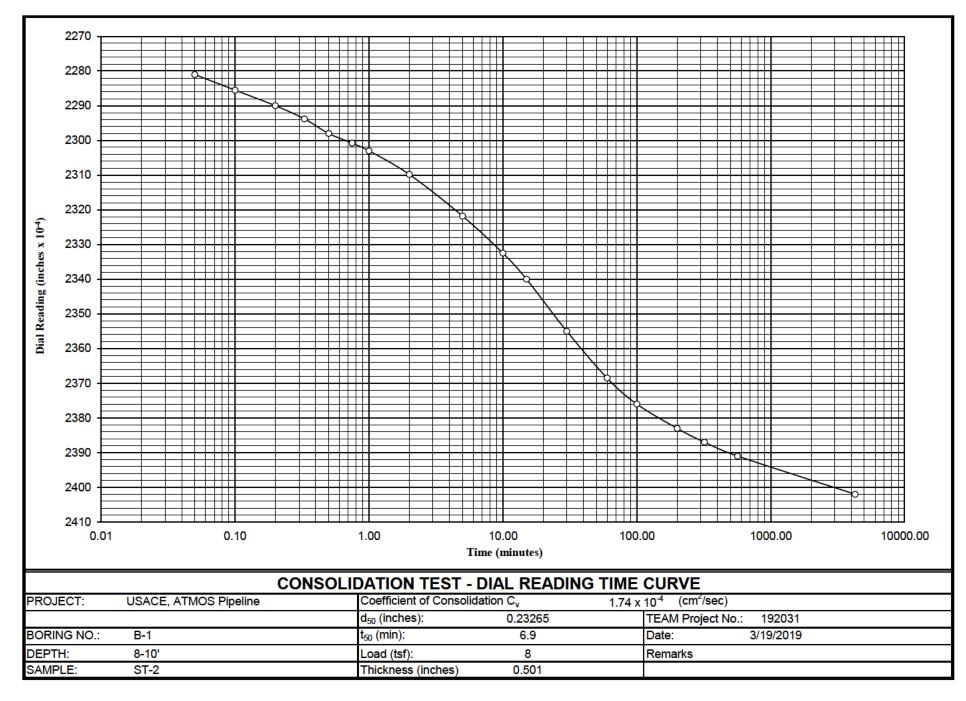
#### CONSOLIDATION TEST

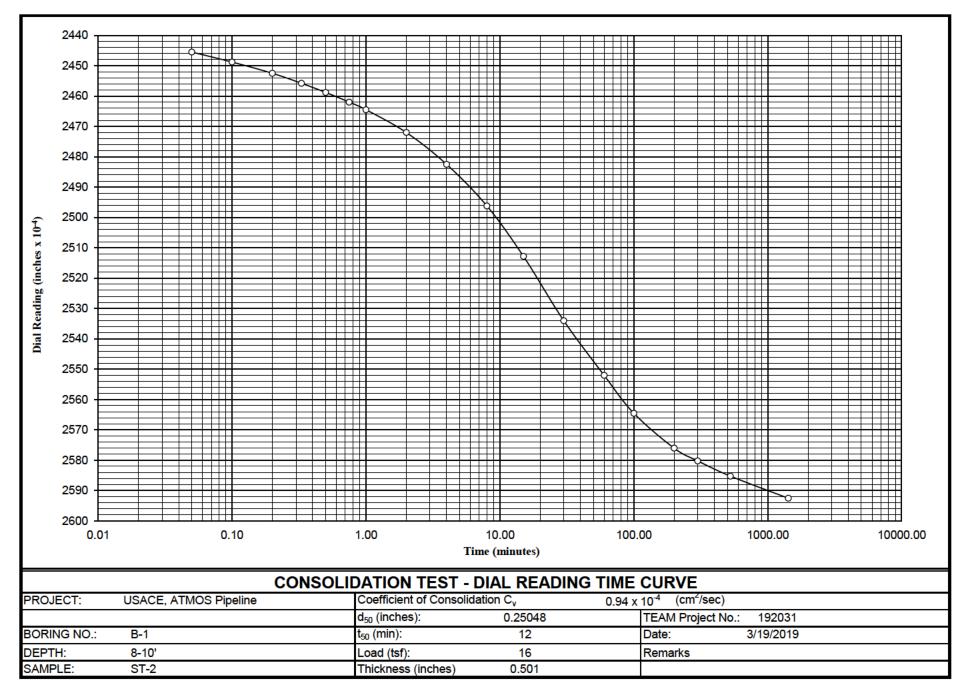
(Computation of Void Ratio)

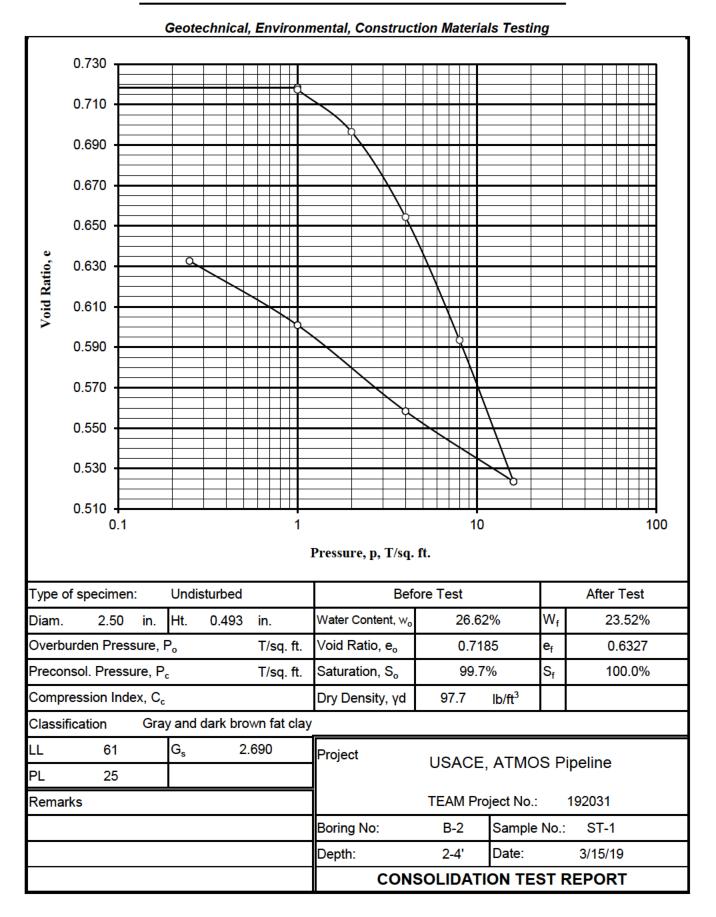
| PROJECT                  | USACE, AT   | TMOS Pipeline                          | TEA                               | M Job No.:                      | 192031                              | DATE:                       | 3/19/19       |
|--------------------------|---|--|-----------------------------------|---------------------------------|-------------------------------------|-----------------------------|---------------|
|                          | B-1   | SAMP                                   | LE NO. ST-2                       | DEPTH                           | 8-10'                               | CONSOLIDOMETER NO.          | . 3           |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied  | Time in Min.<br>Increment<br>Effective | Dial Reading 10 <sup>-4</sup> in. | Correction 10 <sup>-4</sup> in. | Chang<br>Height<br>10 <sup>-4</sup> | t, ∆H Voids, H <sub>V</sub> | Void Ratio, e |
| 0.1                      | 3/19  | Zero Point                             | 2000                              | 2000                            | 0                                   |                             | 0.6435        |
| 1                        | 3/19  | Initial Load                           | 2028                              | 2028                            | 0                                   | 1962                        | 0.6435        |
| 1                        | 3/19  | 1345                                   | 2031                              | 2028                            | -3                                  | 3 1959                      | 0.6425        |
| 2                        | 3/20  | 1425                                   | 2099.2                            | 2042                            | -57                                 | .2 1904                     | 0.6247        |
| 4                        | 3/21  | 1495                                   | 2224.2                            | 2059                            | -16                                 | 5.2 1796                    | 0.5893        |
| 8                        | 3/22  | 4270                                   | 2402                              | 2080                            | -32                                 | 22 1640                     | 0.5379        |
| 16                       | 3/25  | 1425                                   | 2592.5                            | 2106                            | -486                                | 6.5 1475                    | 0.4839        |
| 4                        | 3/26  | 1380                                   | 2475                              | 2071                            | -40                                 | 04 <b>1</b> 558             | 0.5110        |
| 1                        | 3/27  | 1515                                   | 2343                              | 2043                            | -30                                 | 00 1662                     | 0.5451        |
| 0.25                     | 3/28  | 1665                                   | 2232                              | 2022                            | -21                                 | 10 1752                     | 0.5746        |
| Note:                    |   |  |                                   |                                 |                                     |                             |               |
|                          | pids, H <sub>V</sub> = (H - H <sub>S</sub> )<br>e = $\frac{H_V}{H_T}$ |  | H <sub>S</sub> = 0.3048           | Computed                        | by Jason Vo                         | ung Checked by Jame         | se Hutt       |











Geotechnical, Environmental, Construction Materials Testing

|  |  |         |  | DLIDATION TE<br>ecimen Data) | ST                      |                 |            |  |  |
|--|--|---------|--|------------------------------|-------------------------|-----------------|------------|--|--|
| Pr   | oject: USAC                                | E ATM   | OS Pipeline  |                              | TEAM Job No.:           | 192             | 031        |  |  |
|  | -  | -2      | Sample No.: ST-1   | Depth:                       | 2-4' Date               |                 |            |  |  |
| Class  | sification Gray                            | and da  | k brown fat clay   |                              |                         |                 |            |  |  |
|  |  |         |  | Before Test                  |                         |                 | After Test |  |  |
|  |  |         | Specimen   |                              | Trimmings               |                 | Specimen   |  |  |
|  | Tare No.                                   |         | Ring and Plates  |                              | 632                     |                 | 409        |  |  |
| ns   | Tare plus wet                              | soil    | 183.08   |                              | 566.37                  |                 | 111.10     |  |  |
| gran   | Tare plus dry                              | soil    | 166.56   |                              | 491.19                  |                 | 96.50      |  |  |
| Weight in grams  | Water                                      | Ww      | W <sub>WO</sub> 16.52  |                              | 75. <mark>1</mark> 8    | W <sub>wf</sub> | 14.60      |  |  |
| eigh   | Tare                                       |         | 104.49   |                              | 208.78                  |                 | 34.43      |  |  |
| 8  | Dry soil                                   | Ws      | 62.07  |                              | 282.41                  |                 | 62.07      |  |  |
| W  | ater Content                               | w       | W <sub>O</sub> 26.62%  |                              | 26.62%                  | W <sub>f</sub>  | 23.52%     |  |  |
| Consolidometer No.: 4 Area of specimen, A, (sq. cm.) 31.67                       |  |         |  |                              |                         |                 |            |  |  |
| Weight of ring, g         N/A         Height of specimen, H, (in.)         0.493 |  |         |  |                              |                         |                 |            |  |  |
|  | Weight of plates, g                        |         | N/A  | Spec                         | ific Gravity of solids, | (Gs)            | 2.690      |  |  |
| Net o<br>Heigl   | change in height of<br>ht of specimen at e | specime | en at end of test, ΔH =  | ).4684 ii                    | n.<br>= 0.7185          | 5 in.           |            |  |  |
| Void   | ratio after test, e <sub>f</sub>           | = H     | $\frac{H_{s}}{H_{s}} = \frac{0.4684}{0.280}$   | 0.2869<br>59                 |                         |                 |            |  |  |
|  |  |         | $t, S_0 = \frac{H_{WO}}{H - H_S} = \frac{H_{WO}}{H}$   |                              |                         | .7%             |            |  |  |
|  |  |         | $S_{f} = \frac{H_{wf}}{H_{f} - H_{S}} = \frac{0}{0}$ $\frac{W_{S}}{H \times A} = \frac{62.0}{0.493}$ |                              |                         |                 | I.ft.      |  |  |
| Rem  | arks                                       |         |  |                              |                         |                 |            |  |  |
| Tech   | nician Jas                                 | on Youn | g Computed by  | Jason                        | Young Che               | cked by         | James Hutt |  |  |

|              |                 |               | TE                     | AM C                                   | Cons        | sulte        | ants            | s, In         | с.                     |                                     |             |
|--------------|-----------------|---------------|------------------------|--|-------------|--------------|-----------------|---------------|------------------------|-------------------------------------|-------------|
|              |                 | Ge            | eotechnica             | l, Environn                            |             |              |                 | Materia       | ls Testing             |                                     | _           |
|              |                 |               |                        | CONSO                                  | LIDATI      | ON TES       | Т               |               |                        |                                     |             |
|              |                 |               |                        | (Time - C                              | onsolida    | ation Da     | ta)             |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
| Proje        | ct:             | USA           | CE, ATMOS              | Pipeline                               |             |              |                 | TEA           | M Job No.:             | 192031                              |             |
| -            |                 |               |                        | Sample No                              |             |              | anth:           |               |                        |                                     | •           |
| Donn         | y No            |               | D-2                    | Sample No                              |             | <u>-1</u> _D | -pui            | 2-4           | CONSOLINO              | 4                                   | •           |
| Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/15         | 0.25            | 10:15         | 0                      | 2003.0                                 | 20          | 3/19         | 4               | 8:45          | 0                      | 2095                                |             |
| 3/15         | 0.5             | 10:20         | 5                      | 2005.0                                 |             | 3/19         | 4               | 8:45          | 0.05                   | 2113                                |             |
| 3/15         | 1               | 11:15         | 60                     | 2017.0                                 |             | 3/19         | 4               | 8:45          | 0.1                    | 2115                                |             |
| 3/18         | 1               | 8:00          | 4185                   | 2021.0                                 | 19          | 3/19         | 4               | 8:45          | 0.2                    | 2117.5                              |             |
|              |                 |               |                        |  |             | 3/19         | 4               | 8:45          | 0.33                   | 2119.2                              |             |
|              |                 |               |                        |  |             | 3/19         | 4               | 8:45          | 0.5                    | 2121.2                              |             |
|              |                 |               |                        |  |             | 3/19         | 4               | 8:45          | 0.75                   | 2123.2                              |             |
|              |                 |               |                        |  |             | 3/19         | 4               | 8:46          | 1                      | 2125                                |             |
| 3/18         | 2               | 8:40          | 0                      | 2021                                   | 19          | 3/19         | 4               | 8:47          | 2                      | 2129.5                              |             |
| 3/18         | 2               | 8:40          | 0.05                   | 2034                                   |             | 3/19         | 4               | 8:49          | 4                      | 2136                                |             |
| 3/18         | 2               | 8:40          | 0.1                    | 2035.5                                 |             | 3/19         | 4               | 8:53          | 8                      | 2144.8                              |             |
| 3/18         | 2               | 8:40          | 0.2                    | 2037                                   |             | 3/19         | 4               | 9:00          | 15                     | 2154.5                              |             |
| 3/18         | 2               | 8:40          | 0.33                   | 2038                                   |             | 3/19         | 4               | 9:15          | 30                     | 2172.5                              |             |
| 3/18         | 2               | 8:40          | 0.5                    | 2039.2                                 |             | 3/19         | 4               | 9:45          | 60                     | 2189                                |             |
| 3/18         | 2               | 8:40          | 0.75                   | 2040.5                                 |             | 3/19         | 4               | 10:25         | 100                    | 2200                                |             |
| 3/18         | 2               | 8:41          | 1                      | 2042                                   |             | 3/19         | 4               | 12:05         | 200                    | 2214.5                              |             |
| 3/18         | 2               | 8:42          | 2                      | 2044.5                                 |             | 3/19         | 4               | 13:45         | 300                    | 2220                                |             |
| 3/18         | 2               | 8:44          | 4                      | 2048.2                                 |             | 3/19         | 4               | 17:15         | 510                    | 2225.8                              |             |
| 3/18         | 2               | 8:48          | 8                      | 2053                                   |             | 3/20         | 4               | 9:00          | 1455                   | 2230                                | 20          |
| 3/18         | 2               | 8:55          | 15                     | 2058.5                                 |             |              |                 |               |                        |                                     |             |
| 3/18         | 2               | 9:10          | 30                     | 2066.5                                 |             |              |                 |               |                        |                                     |             |
| 3/18<br>3/18 | 2               | 9:45<br>10:20 | 65                     | 2075.2                                 |             |              |                 |               |                        |                                     |             |
| 3/18         | 2               | 10:20         | 100<br>200             | 2080                                   |             |              |                 |               |                        |                                     |             |
| 3/18         | 2               | 12:00         | 300                    | 2085.8<br>2089                         |             |              |                 |               |                        |                                     |             |
| 3/18         | 2               | 13:40         | 300<br>575             |  |             |              |                 |               |                        |                                     |             |
| 3/10         | 2               | 8:45          | 1445                   | 2092.2<br>2095                         | 20          |              |                 |               |                        |                                     |             |
| 5/18         | 2               | 0.40          | 1440                   | 2080                                   | 20          |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             |              |                 |               |                        |                                     |             |
|              |                 |               |                        |  |             | Τe           | echnicia        | n <u>Jaso</u> | n Young                | •                                   |             |
|              |                 |               |                        |  |             | Te           | echnicia        | n Jaso        | n Young                |                                     | •           |

| Projec<br>Boring<br>Date |                  | USA          | CE, ATMOS   |                                    | CIDATI   | ON TES       | Т        | Muteriu       | is Testing  |                        |       |
|--------------------------|------------------|--------------|-------------|------------------------------------|----------|--------------|----------|---------------|-------------|------------------------|-------|
| Boring                   | g No.:<br>Press. |              |             | (Time - C                          | onsolida |              |          |               |             |                        |       |
| Boring                   | g No.:<br>Press. |              |             | Pipeline                           |          | ation Da     | ita)     |               |             |                        |       |
| Boring                   | g No.:<br>Press. |              |             |                                    |          |              |          |               |             |                        |       |
| Boring                   | g No.:<br>Press. |              |             |                                    |          |              |          |               |             |                        |       |
|                          | Press.           |              | B-2         | Sample No                          |          |              |          |               | M Job No.:  |                        |       |
| Date                     |                  | Time         |             | _ Sample No.: <u>ST-1</u> Depth: _ |          |              |          | 2-4'          | Consol.No.: | 4                      | ı     |
| Date                     | (tsf)            | lime         | Elapsed     | Dial Reading                       | Temp.    | Dete         | Press.   | <b>T</b> i    | Elapsed     | Dial Reading           | Temp. |
|                          |                  |              | Time, (min) | (10 <sup>-4</sup> in.)             | °C       | Date         | (tsf)    | Time          | Time, (min) | (10 <sup>-4</sup> in.) | °C    |
| 3/20                     | 8                | 9:00         | 0           | 2230                               | 20       | 3/21         | 16       | 8:45          | 0           | 2420.5                 | 20    |
| 3/20                     | 8                | 9:00         | 0.05        | 2250                               |          | 3/21         | 16       | 8:45          | 0.05        | 2439.8                 |       |
| 3/20                     | 8                | 9:00         | 0.1         | 2251.5                             |          | 3/21         | 16       | 8:45          | 0.1         | 2441.8                 |       |
| 3/20                     | 8                | 9:00         | 0.2         | 2253                               |          | 3/21         | 16       | 8:45          | 0.2         | 2443.8                 |       |
| 3/20                     | 8                | 9:00         | 0.33        | 2255.2                             |          | 3/21         | 16       | 8:45          | 0.33        | 2445.8                 |       |
| 3/20                     | 8                | 9:00         | 0.5         | 2257                               |          | 3/21         | 16       | 8:45          | 0.5         | 2447.8                 |       |
| 3/20                     | 8                | 9:00         | 0.75        | 2259.5                             |          | 3/21         | 16       | 8:45          | 0.75        | 2450                   |       |
| 3/20                     | 8                | 9:01         | 1           | 2261.5                             |          | 3/21         | 16       | 8:46          | 1           | 2452                   |       |
| 3/20                     | 8                | 9:02         | 2           | 2266.5                             |          | 3/21         | 16       | 8:47          | 2           | 2458                   |       |
| 3/20                     | 8                | 9:04         | 4           | 2274.5                             |          | 3/21         | 16       | 8:49          | 4           | 2466                   |       |
| 3/20                     | 8                | 9:08         | 8           | 2285.5                             |          | 3/21         | 16       | 8:53          | 8           | 2477                   |       |
| 3/20<br>3/20             | 8<br>8           | 9:15<br>9:30 | 15          | 2300                               |          | 3/21         | 16<br>16 | 9:00<br>9:15  | 15          | 2493.5                 |       |
| 3/20                     | 0<br>8           | 9.30         | 30<br>60    | 2320.8<br>2347.5                   |          | 3/21<br>3/21 | 16       | 9:15          | 30<br>60    | 2514.8<br>2546         |       |
| 3/20                     | 8                | 10:00        | 100         | 2368.8                             |          | 3/21         | 16       | 9.45<br>10:25 | 100         | 2540                   |       |
| 3/20                     | 8                | 12:20        | 200         | 2308.8                             |          | 3/21         | 16       | 12:05         | 200         | 2602.5                 |       |
| 3/20                     | 8                | 14:00        | 300         | 2403                               |          | 3/21         | 16       | 13:45         | 300         | 2615.5                 |       |
| 3/20                     | 8                | 17:45        | 525         | 2403                               |          | 3/21         | 16       | 19:00         | 615         | 2629.5                 |       |
| 3/21                     | 8                | 8:45         | 1425        | 2420.5                             | 20       | 3/22         | 16       | 9:25          | 1480        | 2637                   | 20    |
| 0,21                     | <u> </u>         | 0.40         | 1420        | 2420.0                             | 20       | 0,22         | 10       | 0.20          | 1400        | 2007                   | 20    |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          |              |          |               |             |                        |       |
|                          |                  |              |             |                                    |          | Те           | echnicia | n Jasoi       | n Young     |                        |       |

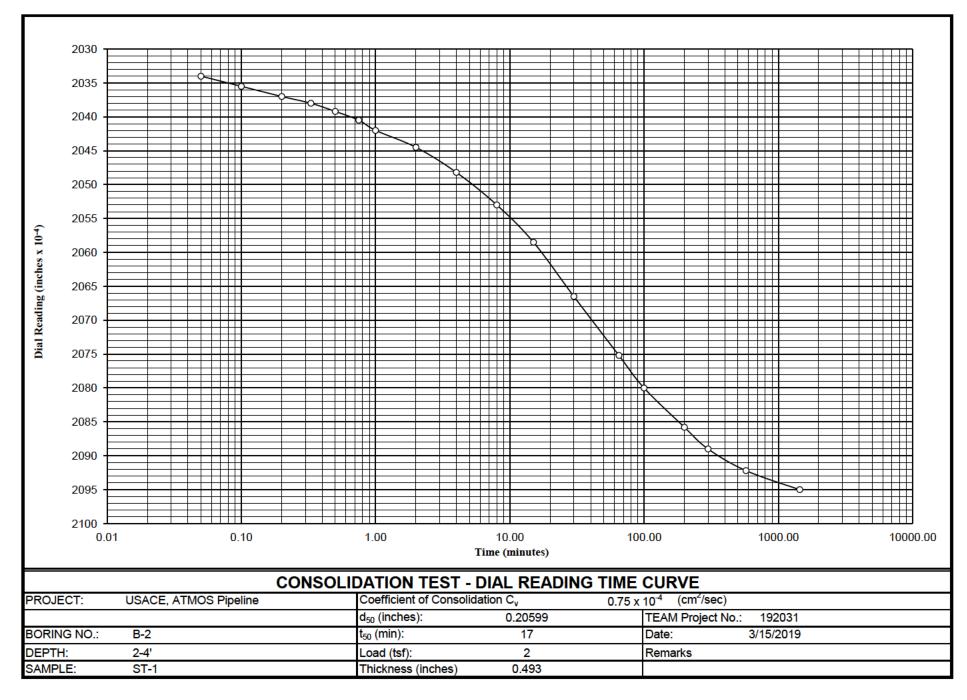
|       |                 |      | TE                     | AM C                                   | Cons                    | sulta         | ints            | , In           | с.                     |                                     |                         |
|-------|-----------------|------|------------------------|--|-------------------------|---------------|-----------------|----------------|------------------------|-------------------------------------|-------------------------|
|       |                 | G    | eotechnica             | l, Environn                            | iental,                 | Constru       | uction          | Materia        | ls Testing             |                                     |                         |
|       |                 |      |                        | CONSO                                  |                         | ON TES        | Т               |                |                        |                                     |                         |
|       |                 |      |                        | (Time - C                              | onsolida                | ation Da      | ta)             |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
| -     |                 |      | CE, ATMOS              |  |                         |               |                 |                | M Job No.:             |                                     |                         |
| Borin | ng No.:         |      | B-2                    | Sample No                              | .: <u>S</u> T           | <u>Γ-1</u> D€ | epth:           | 2-4'           | Consol.No.:            | 4                                   |                         |
| Date  | Press.<br>(tsf) | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C | Date          | Press.<br>(tsf) | Time           | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C |
|       |                 |      |                        |  |                         |               |                 | REBO           |                        | DS                                  |                         |
|       |                 |      |                        |  |                         | 3/22          | 4               | 9:25           | Rebound                | 2637                                | 20                      |
|       |                 |      |                        |  |                         | 3/24          | 4               | 14:15          | 3170                   | 2514.2                              | 20                      |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         | 3/24          | 1               | 14:15          | Rebound                | 2514.2                              | 20                      |
|       |                 |      |                        |  |                         | 3/25          | 1               | 17:30          | 1635                   | 2369.2                              | 21                      |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         | 2/25          | 0.05            | 47.00          | Delevel                | 0000.0                              | 24                      |
|       |                 |      |                        |  |                         | 3/25<br>3/26  | 0.25            | 17:30<br>15:30 | Rebound<br>1320        | 2369.2<br>2257                      | 21<br>20                |
|       |                 |      |                        |  |                         | 0,20          | 0.20            | 10.00          | 1320                   | 2251                                | 20                      |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               | M               | achine D       | eflection Re           | eadings                             |                         |
|       |                 |      |                        |  |                         |               | 0.25            |                |                        | 2003                                |                         |
|       |                 |      |                        |  |                         |               | 1               |                |                        | 2018                                |                         |
|       |                 |      |                        |  |                         |               | 2               |                |                        | 2032                                |                         |
|       |                 |      |                        |  |                         |               | 4               |                |                        | 2046                                |                         |
|       |                 |      |                        |  |                         |               | 8<br>16         |                |                        | 2062<br>2078                        |                         |
|       |                 |      |                        |  |                         |               | 4               |                |                        | 2078                                |                         |
|       |                 |      |                        |  |                         |               | 1               |                |                        | 2032                                |                         |
|       |                 |      |                        |  |                         |               | 0.25            |                |                        | 2011                                |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         |               |                 |                |                        |                                     |                         |
|       |                 |      |                        |  |                         | Τe            | echniciar       | n <u>Jaso</u>  | n Young                |                                     |                         |

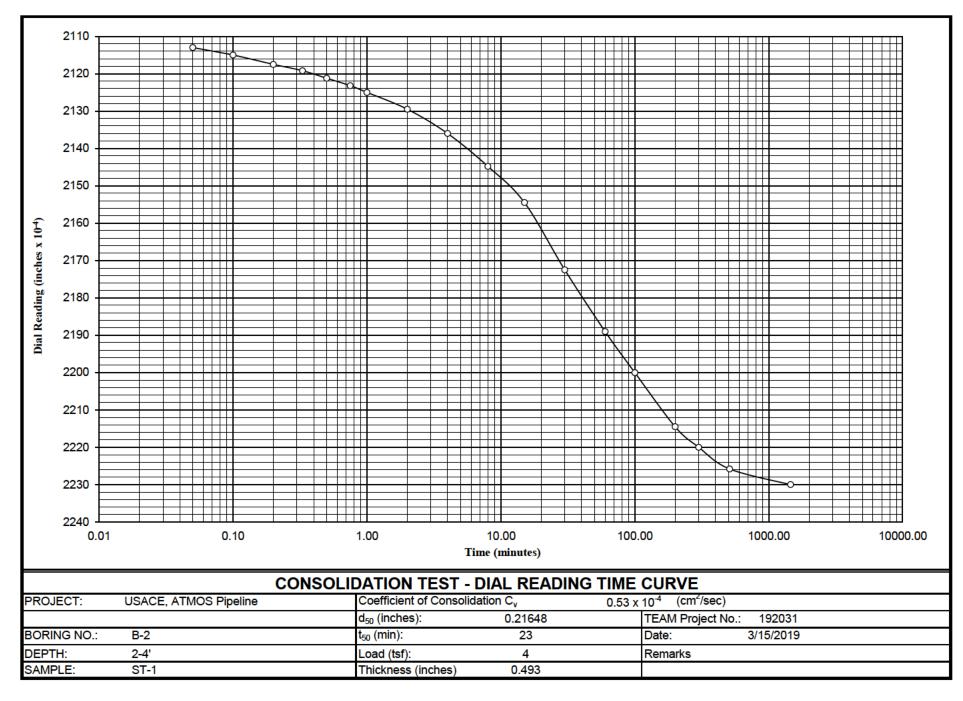
Geotechnical, Environmental, Construction Materials Testing

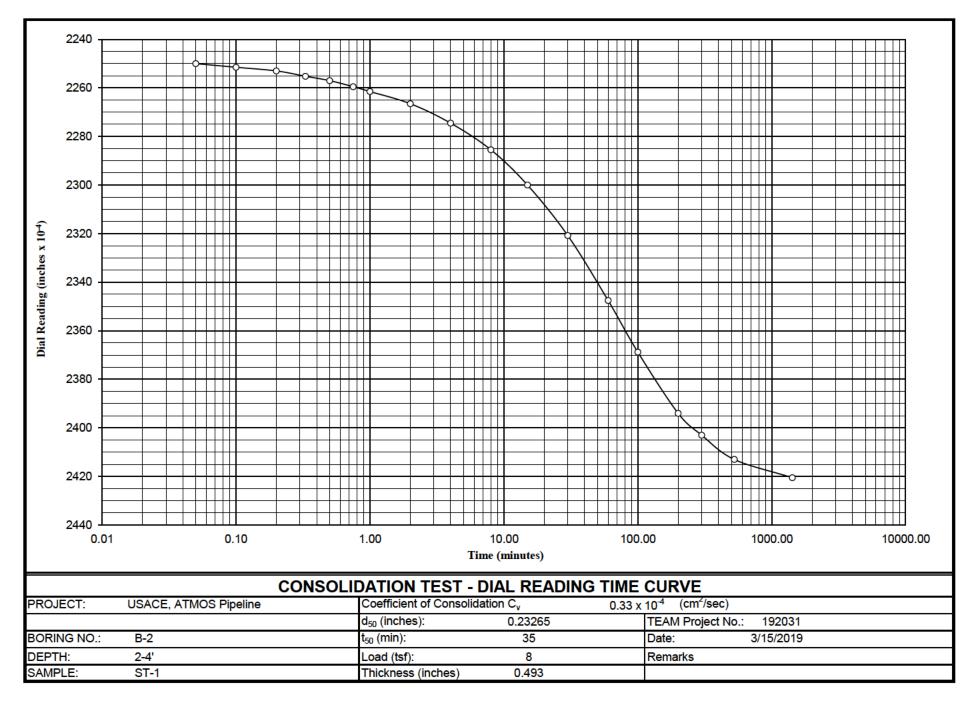
#### CONSOLIDATION TEST

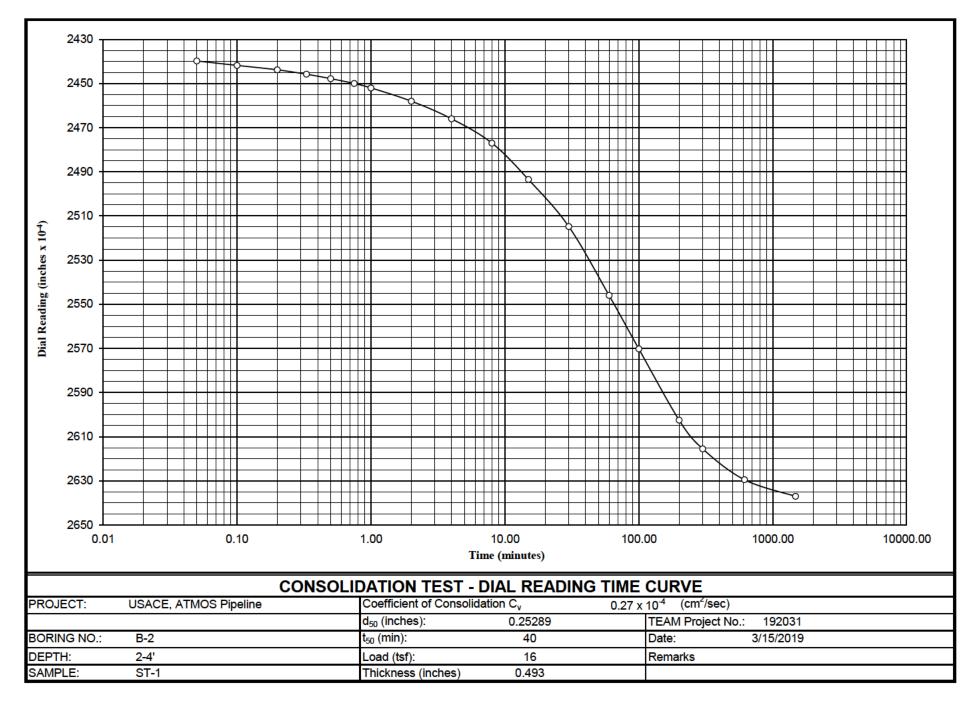
(Computation of Void Ratio)

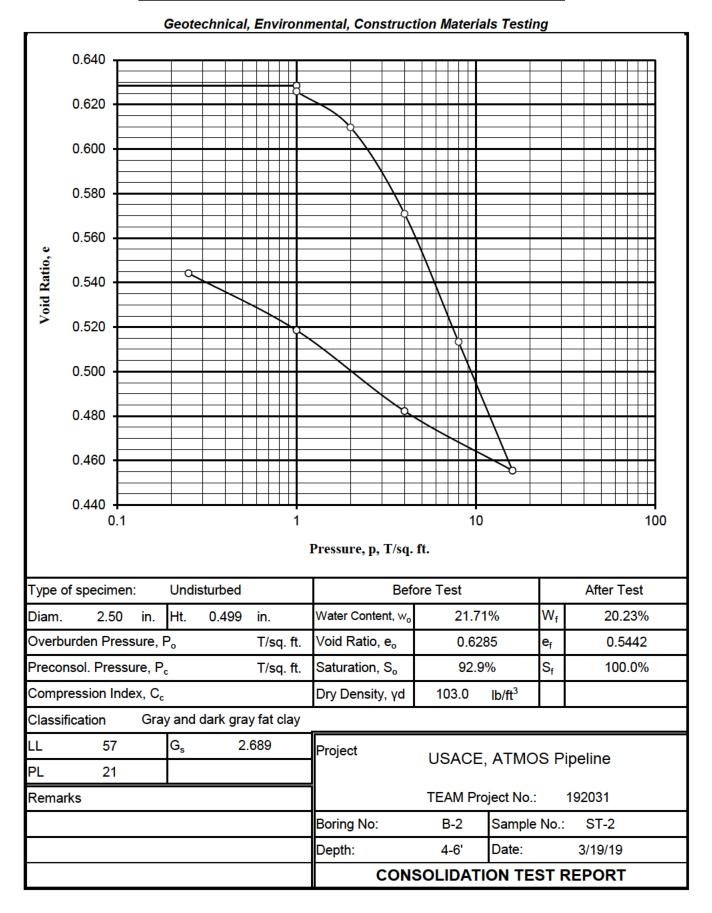
| PROJECT                  | USACE, A                     | TMOS Pipeline                          | TEA                               | M Job No.:                      | 192031      | DATE:  | 3/15/19       |
|--------------------------|------------------------------|--|-----------------------------------|---------------------------------|-------------|--|---------------|
| BORING NO.               | B-2                          | SAMP                                   | LE NO. ST-1                       | DEPTH                           | 2-4'        | CONSOLIDOMETER NO  | 0. 4          |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied | Time in Min.<br>Increment<br>Effective | Dial Reading 10 <sup>-4</sup> in. | Correction 10 <sup>-4</sup> in. | Heigh       | the second sec | Void Ratio, e |
| 0.1                      | 3/15                         | Zero Point                             | 2000                              | 2000                            |             | 2061   | 0.7185        |
| 1                        | 3/15                         | Initial Load                           | 2018                              | 2018                            | (           | 2061   | 0.7185        |
| 1                        | 3/15                         | 4185                                   | 2021                              | 2018                            |             | 3 2058   | 0.7174        |
| 2                        | 3/18                         | 1445                                   | 2095                              | 2032                            | -6          | 53 1998  | 0.6965        |
| 4                        | 3/19                         | 1455                                   | 2230                              | 2046                            | -1          | 84 1877  | 0.6543        |
| 8                        | 3/20                         | 1425                                   | 2420.5                            | 2062                            | -35         | 8.5 1703   | 0.5935        |
| 16                       | 3/21                         | 1480                                   | 2637                              | 2078                            | -5          | 59 1502  | 0.5236        |
| 4                        | 3/22                         | 3170                                   | 2514.2                            | 2055                            | -45         | 9.2 1602   | 0.5584        |
| 1                        | 3/24                         | 1635                                   | 2369.2                            | 2032                            | -33         | 7.2 1724   | 0.6009        |
| 0.25                     | 3/25                         | 1320                                   | 2257                              | 2011                            | -24         | 46 1815  | 0.6327        |
| Note:<br>Height of vo    | oids, $H_V$ = ( H - $H_S$ )  | - ΔH                                   | H <sub>S</sub> = 0.2869           |                                 |             |  |               |
| Void Ratio, ₀            | $e = \frac{H_V}{H_S}$        | Tech                                   | nician Jason Young                | computed                        | by Jason Yo | oung Checked by Jan  | nes Hutt      |











Geotechnical, Environmental, Construction Materials Testing

|  |   |                             |   | DATION TEST<br>men Data)  |                 |            |  |  |  |  |  |
|--|---|-----------------------------|---|---|-----------------|------------|--|--|--|--|--|
|  | oject: USAC   |                             | OS Pipeline<br>Sample No.: ST-2   | TEAM Job No.:<br>Depth: 4-6' Date:                                      | 192             |            |  |  |  |  |  |
|  |   |                             |   |   |                 |            |  |  |  |  |  |
| Class  | Silication Gray   | anu uai                     | rk gray fat clay<br>Befo  | pre Test  |                 | After Test |  |  |  |  |  |
|  |   |                             | Specimen  | Trimmings   |                 | Specimen   |  |  |  |  |  |
|  | Tare No.  |                             | Ring and Plates   | 663   |                 | 417        |  |  |  |  |  |
| ns   | Tare plus wet   | soil                        | 190.67  | 569.55  |                 | 114.75     |  |  |  |  |  |
| grar   | Tare plus dry   | soil                        | 176.28  | 505.23  |                 | 101.34     |  |  |  |  |  |
| Weight in grams  | Water   | Ww                          | W <sub>WO</sub> 14.39   | 64.32   | W <sub>wf</sub> | 13.41      |  |  |  |  |  |
| /eigh  | Tare  |                             | 110.00  | 209.00  |                 | 35.06      |  |  |  |  |  |
| -  | Dry soil  | Ws                          | 66.28   | 296.23  |                 | 66.28      |  |  |  |  |  |
| W  | ater Content  | W                           | W <sub>0</sub> 21.71%   | 21.71%  | W <sub>f</sub>  | 20.23%     |  |  |  |  |  |
| Consolidometer No.:     2     Area of specimen, A, (sq. cm.)     31.67   |   |                             |   |   |                 |            |  |  |  |  |  |
| Weight of ring, g         N/A         Height of specimen, H, (in.)         0.499   |   |                             |   |   |                 |            |  |  |  |  |  |
|  | Weight of plates, g   |                             | N/A   | Specific Gravity of solids, (   | Gs)             | 2.689      |  |  |  |  |  |
| Final<br>Net o<br>Heigl  | height of water, H <sub>v</sub><br>change in height of<br>ht of specimen at e | wf =<br>specime<br>nd of te | st, $H_f = H - \Delta H = 0.47$   | $\frac{13.41}{7 \times 1 \times 2.54} = 0.166$<br>0.02585 in.<br>32 in. | 7 in.           |            |  |  |  |  |  |
| Void   | ratio after test, e <sub>f</sub>  | = <u>H</u>                  | $\frac{H_{s}}{H_{s}} = \frac{0.3064}{0.47315 - 0.0000}$ $\frac{H_{s}}{H_{s}} = \frac{0.47315 - 0.0000}{0.3064}$ |   |                 |            |  |  |  |  |  |
| Degree of saturation before test, $S_0 = \frac{H_{WO}}{H - H_S} = \frac{0.1789}{0.4990 - 0.3064} = 92.9\%$   |   |                             |   |   |                 |            |  |  |  |  |  |
| Degree of saturation after test, $S_f = \frac{H_{wf}}{H_f - H_S} = \frac{0.1667}{0.4732 - 0.3064} = 100.0\%$<br>Dry density before test, $\gamma_d = \frac{W_S}{H \times A} = \frac{66.28 \times 62.4}{0.499 \times 31.67 \times 2.54} = 103.0$ lb./cu.ft. |   |                             |   |   |                 |            |  |  |  |  |  |
| Rem  | Remarks   |                             |   |   |                 |            |  |  |  |  |  |
| Tech   | Technician Jason Young Computed by Jason Young Checked by James Hutt          |                             |   |   |                 |            |  |  |  |  |  |

|              |                 |                |                        | AM C                                   |               |              |                 | -       |                        |                                     |             |
|--------------|-----------------|----------------|------------------------|--|---------------|--------------|-----------------|---------|------------------------|-------------------------------------|-------------|
|              |                 | Ge             | eotechnica             | l, Environn                            | -             |              |                 | Materia | ls Testing             |                                     |             |
|              |                 |                |                        | CONSO                                  | LIDATI        | ON TES       | T               |         |                        |                                     |             |
|              |                 |                |                        | (Time - C                              | onsolida      | ation Da     | ta)             |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
| Proje        | ect:            | USA            | CE, ATMOS              | Pipeline                               |               |              |                 | TEA     | M Job No.:             | 192031                              |             |
| Borin        | ng No.:         |                | B-2                    | Sample No                              | .: <u>S</u> T | <u>-2</u> De | epth:           | 4-6'    | Consol.No.:            | 2                                   |             |
| Date         | Press.<br>(tsf) | Time           | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C   | Date         | Press.<br>(tsf) | Time    | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/19         | 0.125           | 10:10          | 0                      | 2003                                   | 20            | 3/21         | 4               | 8:35    | 0                      | 2104.5                              | 20          |
| 3/19         | 0.25            | 10:11          | 1                      | 1996                                   |               | 3/21         | 4               | 8:35    | 0.05                   | 2143.5                              |             |
| 3/19         | 0.5             | 10:12          | 2                      | 2007                                   |               | 3/21         | 4               | 8:35    | 0.1                    | 2147.8                              |             |
| 3/19         | 0.75            | 11:20          | 70                     | 2015                                   |               | 3/21         | 4               | 8:35    | 0.2                    | 2153                                |             |
| 3/19         | 1               | 13:00          | 170                    | 2028                                   |               | 3/21         | 4               | 8:35    | 0.33                   | 2156                                |             |
| 3/20         | 1               | 8:50           | 1360                   | 2039                                   | 20            | 3/21         | 4               | 8:35    | 0.5                    | 2160                                |             |
|              |                 |                |                        |  |               | 3/21         | 4               | 8:35    | 0.75                   | 2162.8                              |             |
|              |                 |                |                        |  |               | 3/21         | 4               | 8:36    | 1                      | 2166.2                              |             |
| 3/20         | 2               | 8:50           | 0                      | 2039                                   | 20            | 3/21         | 4               | 8:37    | 2                      | 2173                                |             |
| 3/20         | 2               | 8:50           | 0.05                   | 2063.5                                 |               | 3/21         | 4               | 8:39    | 4                      | 2179.8                              |             |
| 3/20         | 2               | 8:50           | 0.1                    | 2065                                   |               | 3/21         | 4               | 8:43    | 8                      | 2187.5                              |             |
| 3/20         | 2               | 8:50           | 0.2                    | 2067.2                                 |               | 3/21         | 4               | 8:50    | 15                     | 2196                                |             |
| 3/20         | 2               | 8:50           | 0.33                   | 2069                                   |               | 3/21         | 4               | 9:05    | 30                     | 2204.2                              |             |
| 3/20         | 2               | 8:50           | 0.5                    | 2070.5                                 |               | 3/21         | 4               | 9:35    | 60                     | 2214                                |             |
| 3/20         | 2               | 8:50           | 0.75                   | 2072.2                                 |               | 3/21         | 4               | 10:25   | 110                    | 2222                                |             |
| 3/20         | 2               | 8:51           | 1                      | 2073.2                                 |               | 3/21         | 4               | 11:55   | 200                    | 2229.5                              |             |
| 3/20         | 2               | 8:52           | 2                      | 2076.2                                 |               | 3/21         | 4               | 13:35   | 300                    | 2232.8                              |             |
| 3/20         | 2               | 8:54           | 4                      | 2079.2                                 |               | 3/21         | 4               | 19:00   | 625                    | 2237.5                              |             |
| 3/20         | 2               | 8:58           | 8                      | 2082.5                                 |               | 3/22         | 4               | 9:30    | 1495                   | 2241.5                              | 20          |
| 3/20         | 2               | 9:05           | 15                     | 2085.5                                 |               |              |                 |         |                        |                                     |             |
| 3/20         | 2               | 9:20           | 30                     | 2088.8                                 |               |              |                 |         |                        |                                     |             |
| 3/20         | 2               | 9:50           | 60                     | 2092                                   |               |              |                 |         |                        |                                     |             |
| 3/20         | 2               | 10:30          | 100                    | 2094                                   |               |              |                 |         |                        |                                     |             |
| 3/20         | 2               | 12:10          | 200                    | 2097                                   |               |              |                 |         |                        |                                     |             |
| 3/20<br>3/20 | 2               | 13:50<br>17:45 | 300                    | 2098.8                                 |               |              |                 |         |                        |                                     |             |
|              |                 |                | 535                    | 2101.8                                 | 20            |              |                 |         |                        |                                     |             |
| 3/21         | 2               | 8:35           | 1425                   | 2104.5                                 | 20            |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |
|              |                 |                |                        |  |               | Te           | echnicia        | n Jaso  | n Young                |                                     |             |
|              |                 |                |                        |  |               |              |                 |         |                        |                                     |             |

|              |                 |              |                        | AM C                                   |             |              |                 |               |                        |  |             |
|--------------|-----------------|--------------|------------------------|--|-------------|--------------|-----------------|---------------|------------------------|--|-------------|
|              |                 | Ge           | eotechnica             | l, Environn                            | _           |              |                 | Materia       | ls Testing             |  |             |
|              |                 |              |                        | CONSO                                  |             |              |                 |               |                        |  |             |
|              |                 |              |                        | (Time - C                              | onsolid     | ation Da     | ta)             |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
| Proje        | ct:             | USA          | CE, ATMOS              | Pipeline                               |             |              |                 | TEA           | M Job No.:             | 192031                                 |             |
| Borin        | g No.:          |              | B-2                    | Sample No                              | .: ST       | Г-2 De       | epth:           | 4-6'          | Consol.No.:            | 2                                      | _           |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/22         | 8               | 9:30         | 0                      | 2241.5                                 | 20          | 3/25         | 16              | 8:40          | 0                      | 2437.5                                 | 21          |
| 3/22         | 8               | 9:30         | 0.05                   | 2298                                   |             | 3/25         | 16              | 8:40          | 0.05                   | 2480.5                                 |             |
| 3/22         | 8               | 9:30         | 0.1                    | 2302.5                                 |             | 3/25         | 16              | 8:40          | 0.1                    | 2484.5                                 |             |
| 3/22         | 8               | 9:30         | 0.2                    | 2306.8                                 |             | 3/25         | 16              | 8:40          | 0.2                    | 2488                                   |             |
| 3/22         | 8               | 9:30         | 0.33                   | 2311                                   |             | 3/25         | 16              | 8:40          | 0.33                   | 2491.5                                 |             |
| 3/22<br>3/22 | 8<br>8          | 9:30<br>9:30 | 0.5                    | 2314.5                                 |             | 3/25<br>3/25 | 16<br>16        | 8:40<br>8:40  | 0.5                    | 2494.2<br>2497.5                       |             |
| 3/22         | о<br>8          | 9.30<br>9:31 | 0.75<br>1              | 2318<br>2320.8                         |             | 3/25         | 16              | 8:41          | 0.75<br>1              | 2497.5                                 |             |
| 3/22         | 8               | 9:32         | 2                      | 2320.8                                 |             | 3/25         | 16              | 8:42          | 2                      | 2499.8                                 |             |
| 3/22         | 8               | 9:34         | 4                      | 2326.5                                 |             | 3/25         | 16              | 8:44          | 4                      | 2516.8                                 |             |
| 3/22         | 8               | 9:38         | 8                      | 2330.0                                 |             | 3/25         | 16              | 8:48          | 8                      | 2529.2                                 |             |
| 3/22         | 8               | 9:45         | 15                     | 2357                                   |             | 3/25         | 16              | 8:55          | 15                     | 2542.2                                 |             |
| 3/22         | 8               | 10:00        | 30                     | 2371.8                                 |             | 3/25         | 16              | 9:10          | 30                     | 2564                                   |             |
| 3/22         | 8               | 10:30        | 60                     | 2388                                   |             | 3/25         | 16              | 9:40          | 60                     | 2586.8                                 |             |
| 3/22         | 8               | 11:10        | 100                    | 2400.2                                 |             | 3/25         | 16              | 10:25         | 105                    | 2604.2                                 |             |
| 3/22         | 8               | 12:50        | 200                    | 2413                                   |             | 3/25         | 16              | 12:00         | 200                    | 2619.5                                 |             |
| 3/22         | 8               | 14:55        | 325                    | 2421                                   |             | 3/25         | 16              | 13:40         | 300                    | 2625.2                                 |             |
| 3/22         | 8               | 19:00        | 570                    | 2426                                   |             | 3/25         | 16              | 17:30         | 530                    | 2631.5                                 |             |
| 3/25         | 8               | 8:40         | 4270                   | 2435.8                                 | 21          | 3/26         | 16              | 8:30          | 1430                   | 2638.2                                 | 20          |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             | <u> </u>     |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             | <u> </u>     |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             |              |                 |               |                        |  |             |
|              |                 |              |                        |  |             | Τe           | echnicia        | n <u>Jaso</u> | n Young                | _                                      |             |

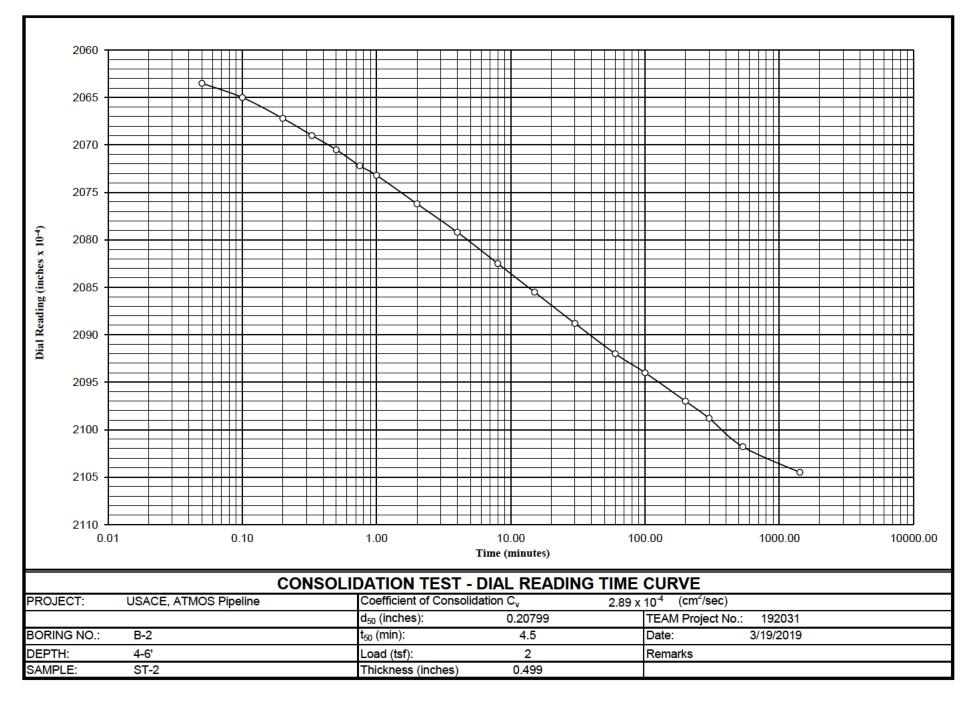
|       |                 |      | TE                     | AM C                                   | Cons                    | sulta    | ints            | , In     | с.                     |  |                         |  |
|-------|-----------------|------|------------------------|--|-------------------------|----------|-----------------|----------|------------------------|--|-------------------------|--|
|       |                 | G    | eotechnica             | l, Environn                            | nental,                 | Constr   | uction 1        | Materia  | ls Testing             |  |                         |  |
|       |                 |      |                        | CONSO                                  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        | (Time - C                              | onsolid                 | ation Da | ta)             |          |                        |  |                         |  |
|       |                 |      |                        | (                                      |                         |          | )               |          |                        |  |                         |  |
| Proie | ect:            | USA  | CE, ATMOS              | Pipeline                               |                         |          |                 | TEA      | M Job No.:             | 192031                                 |                         |  |
| -     |                 |      |                        |  |                         |          |                 |          |                        | 2                                      |                         |  |
|       | .g              |      |                        |  |                         |          |                 |          |                        |  |                         |  |
| Date  | Press.<br>(tsf) | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C | Date     | Press.<br>(tsf) | Time     | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C |  |
|       | ()              |      |                        | (10 11.)                               | Ŭ                       |          | ()              |          |                        |  | •                       |  |
|       |                 |      |                        |  |                         |          |                 | REBO     |                        | DS                                     |                         |  |
|       |                 |      |                        |  |                         | 3/26     | 4               | 8:30     | Rebound                | 2638.2                                 | 20                      |  |
|       |                 |      |                        |  |                         | 3/27     | 4               | 7:30     | 1380                   | 2522.2                                 | 20                      |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         | 3/27     | 1               | 7:30     | Rebound                | 2522.2                                 | 20                      |  |
|       |                 |      |                        |  |                         | 3/28     | 1               | 8:45     | 1515                   | 2382                                   | 20                      |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         | 3/28     | 0.25            | 8:45     | Rebound                | 2382                                   | 20                      |  |
|       |                 |      |                        |  |                         | 3/29     | 0.25            | 12:30    | 1665                   | 2278.5                                 | 20                      |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          | Ma              | achine D | eflection Re           | adings                                 |                         |  |
|       |                 |      |                        |  |                         |          | 0.125           |          |                        | 2003                                   |                         |  |
|       |                 |      |                        |  |                         |          | 1               |          |                        | 2031                                   |                         |  |
|       |                 |      |                        |  |                         |          | 2               |          |                        | 2047                                   |                         |  |
|       |                 |      |                        |  |                         |          | 4               |          |                        | 2065                                   |                         |  |
|       |                 |      |                        |  |                         |          | 8<br>16         |          |                        | 2083                                   |                         |  |
|       |                 |      |                        |  |                         |          | 4               |          | ļ                      | 2108<br>2074                           |                         |  |
|       |                 |      |                        |  |                         |          | 1               |          | L                      | 2074                                   |                         |  |
|       |                 |      |                        |  |                         |          | 0.25            |          |                        | 2020                                   |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |
|       |                 |      |                        |  |                         | Te       | chniciar        | n Jaso   | n Young                |  |                         |  |
|       |                 |      |                        |  |                         |          |                 |          |                        |  |                         |  |

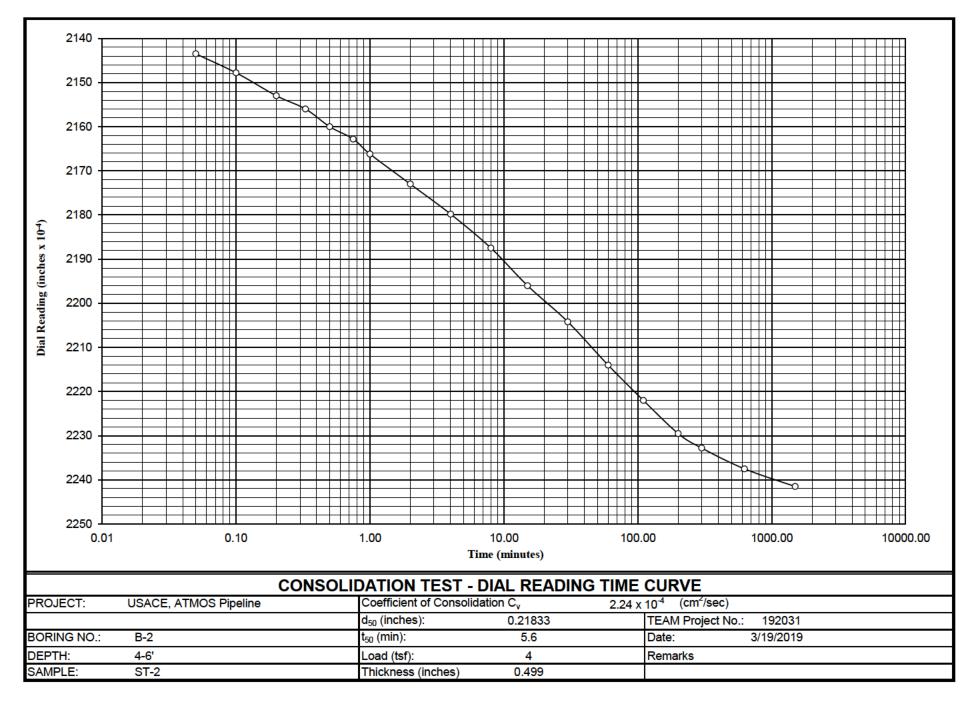
Geotechnical, Environmental, Construction Materials Testing

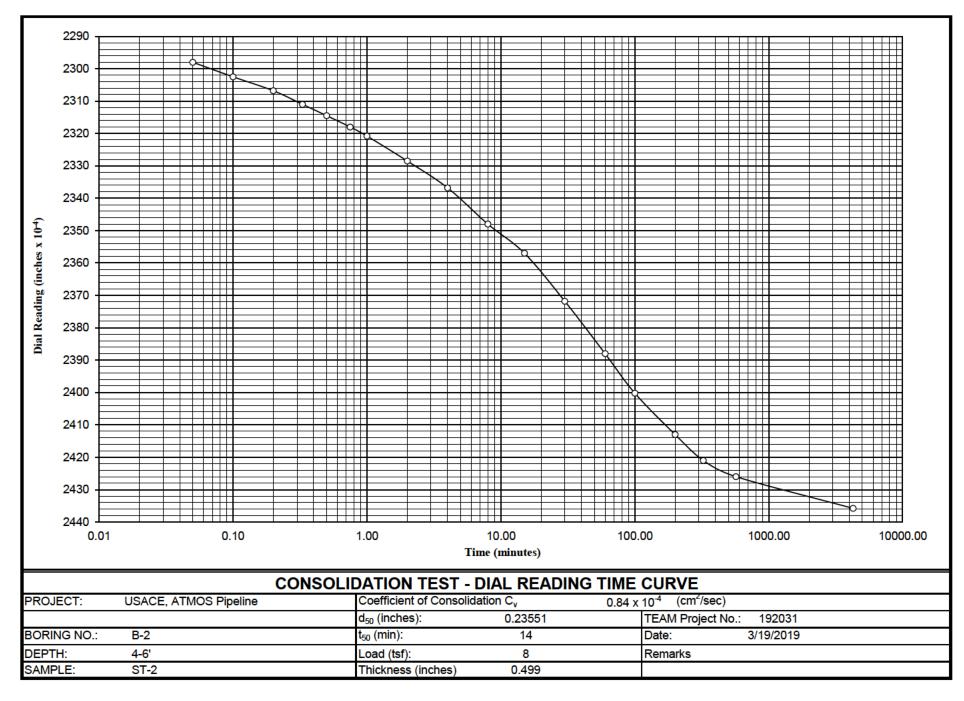
#### CONSOLIDATION TEST

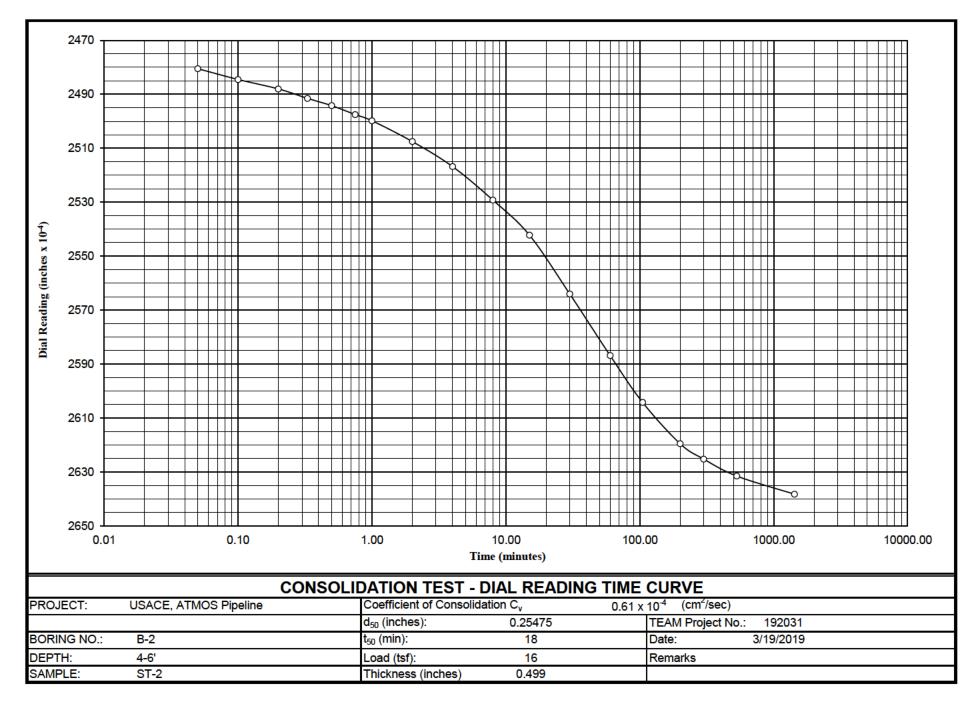
(Computation of Void Ratio)

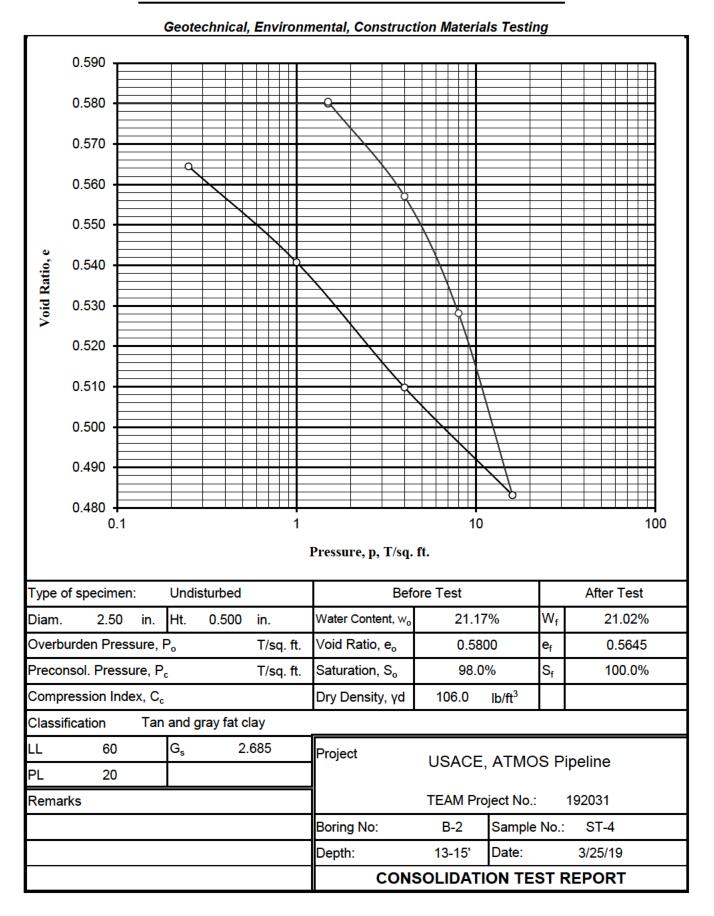
|                          |                              |  |                                      | M Job No.:                         | 192031   | DATE:                    | 3/19/19       |
|--------------------------|------------------------------|--|--------------------------------------|------------------------------------|--|--------------------------|---------------|
|                          | B-2                          | SAMP                                   | LE NO. ST-2                          | DEPTH                              | 4-6'   | CONSOLIDOMETER NO.       | 2             |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied | Time in Min.<br>Increment<br>Effective | Dial Reading<br>10 <sup>-4</sup> in. | Correction<br>10 <sup>-4</sup> in. | Change<br>Height, <i>I</i><br>10 <sup>-4</sup> in. | LH Voids, H <sub>V</sub> | Void Ratio, e |
| 0.1                      | 3/19                         | Zero Point                             | 2000                                 | 2000                               | 0  | 1926                     | 0.6285        |
| 1                        | 3/19                         | Initial Load                           | 2031                                 | 2031                               | 0  | 1926                     | 0.6285        |
| 1                        | 3/19                         | 1360                                   | 2039                                 | 2031                               | -8   | 1918                     | 0.6259        |
| 2                        | 3/20                         | 1425                                   | 2104.5                               | 2047                               | -57.5  | 1868                     | 0.6098        |
| 4                        | 3/21                         | 1495                                   | 2241.5                               | 2065                               | -176.5   | 1749                     | 0.5709        |
| 8                        | 3/22                         | 4270                                   | 2435.8                               | 2083                               | -352.8   | 1573                     | 0.5134        |
| 16                       | 3/25                         | 1430                                   | 2638.2                               | 2108                               | -530.2   | 1396                     | 0.4555        |
| 4                        | 3/26                         | 1380                                   | 2522.2                               | 2074                               | -448.2   | . 1478                   | 0.4823        |
| 1                        | 3/27                         | 1515                                   | 2382                                 | 2045                               | -337   | 1589                     | 0.5186        |
| 0.25                     | 3/28                         | 1665                                   | 2278.5                               | 2020                               | -258.5   | 1667                     | 0.5442        |
| Note:                    |                              |  |                                      |                                    |  |                          |               |











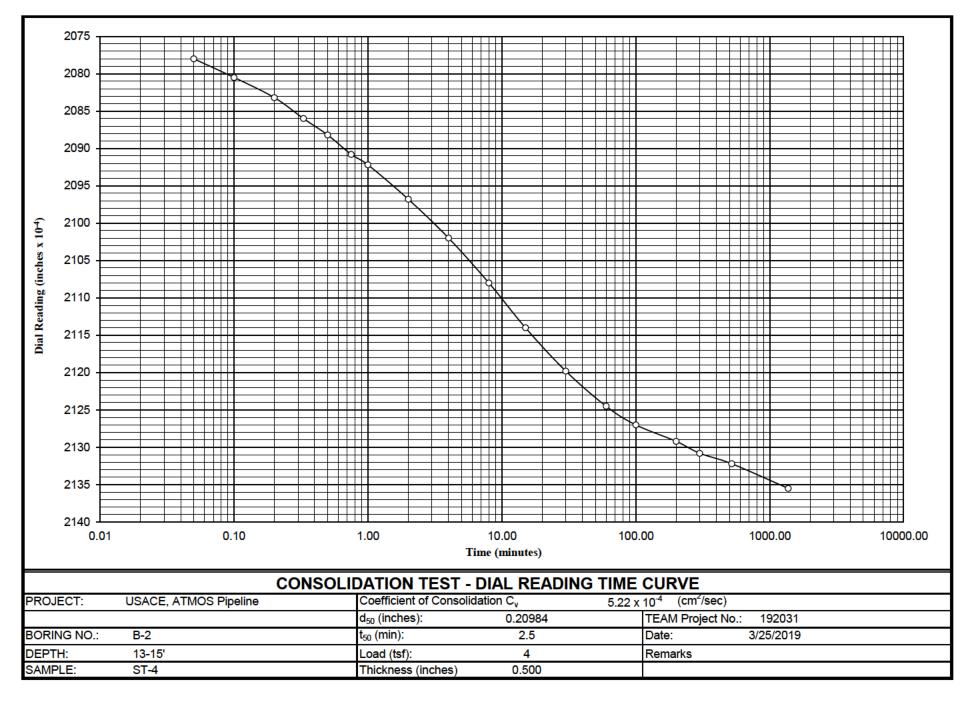
Geotechnical, Environmental, Construction Materials Testing

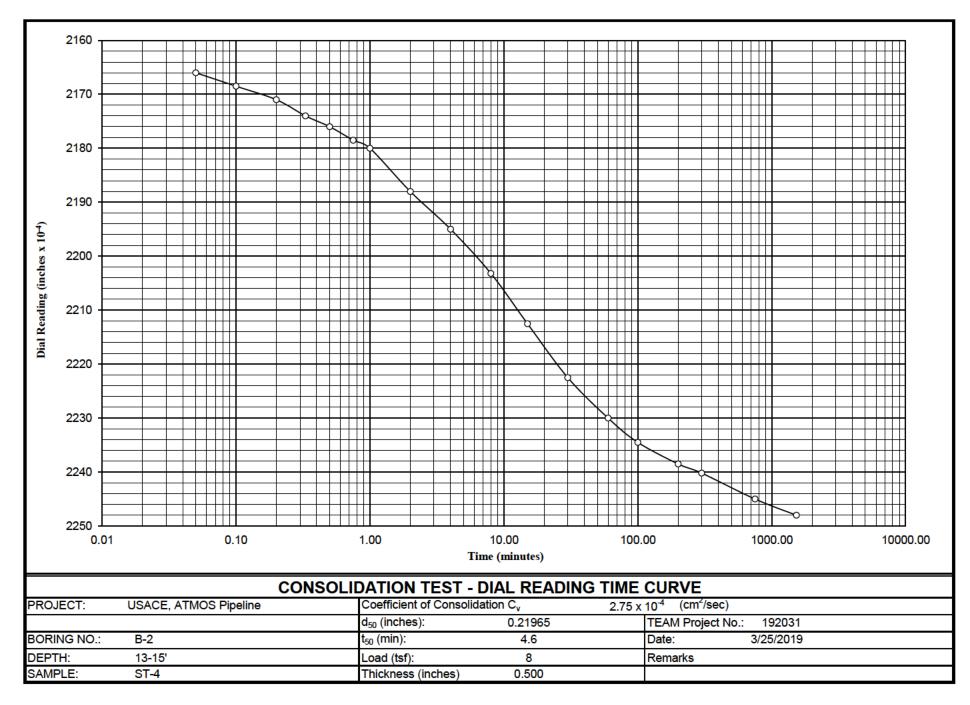
|                 |  |               |  | NSOLIDATION T<br>(Specimen Data |  |                |              |
|-----------------|--|---------------|--|---------------------------------|--|----------------|--------------|
|                 |  | се, атм<br>-2 | OS Pipeline<br>Sample No.: <u>ST</u> -   | 4 Depth:                        | TEAM Job No.:<br>13-15' Date:          | 192            | 031<br>25/19 |
| Class           | ification Tan  | and drav      | / fat clay   |                                 |  |                |              |
| 01000           |  | and gray      | lationary  | Before Test                     |  |                | After Test   |
|                 |  |               | Specimen   |                                 | Trimmings                              |                | Specimen     |
|                 | Tare No.   |               | Ring and Plates  | ;                               | 662                                    |                | 404          |
| su              | Tare plus wet  | soil          | 192.81   |                                 | 504.45                                 |                | 116.39       |
| graı            | Tare plus dry  | soil          | 178.34   |                                 | 453.49                                 |                | 102.02       |
| Weight in grams | Water  | Ww            | W <sub>WO</sub> 14.47  |                                 | 50.96                                  | Wwf            | 14.37        |
| Veigl           | Tare   |               | 109.99   |                                 | 212.80                                 |                | 33.67        |
| -               | Dry soil   | Ws            | 68.35  |                                 | 240.69                                 |                | 68.35        |
| W               | ater Content   | W             | W <sub>O</sub> 21.17%  |                                 | 21.17%                                 | W <sub>f</sub> | 21.02%       |
| C               | Consolidometer No  | .:            | 1  | Are                             | a of specimen, A, (sq.                 | cm.)           | 31.67        |
|                 | Weight of ring, g  |               | N/A  |                                 |  | (in.)          | 0.500        |
|                 | Weight of plates, <u>c</u><br>ht of solids, H <sub>s</sub> = |               | N/A  | Spe                             | cific Gravity of solids, (             | Gs)            | 2.685        |
| Net c<br>Heigl  | change in height of<br>ht of specimen at e                   | specime       | $\frac{W_{Wf}}{A \times \gamma_W} = -\frac{1}{2}$<br>en at end of test, $\Delta H =$<br>st, $H_f = H - \Delta H =$<br>$\frac{H - H_s}{H_s} = -\frac{0.5}{0.5}$ | -0.00490<br>0.4951              | 2.54 = 0.178<br>in.<br>in.<br>= 0.5800 | 6 in.          |              |
| Void            | ratio after test, e <sub>f</sub>                             | = H           | $\frac{H_{s}}{H_{s}} = \frac{0.4951}{0.0000}$  | - 0.3165<br>3165                |  |                |              |
|                 |  |               | $H_{WO} = \frac{H_{WO}}{H - H_S} =$  |                                 | 0.3165 = 98.<br>0.3165 = 100.09        | .0%            |              |
|                 |  |               |  |                                 | 0.3165 = 100.0<br>62.4 = 106.0<br>2.54 |                | .ft.         |
| Rema            | arks   |               |  |                                 |  |                |              |
| Tech            | nician Jas   | on Your       | g Computed by  | y Jaso                          | n Young Cheo                           | cked by        | James Hutt   |

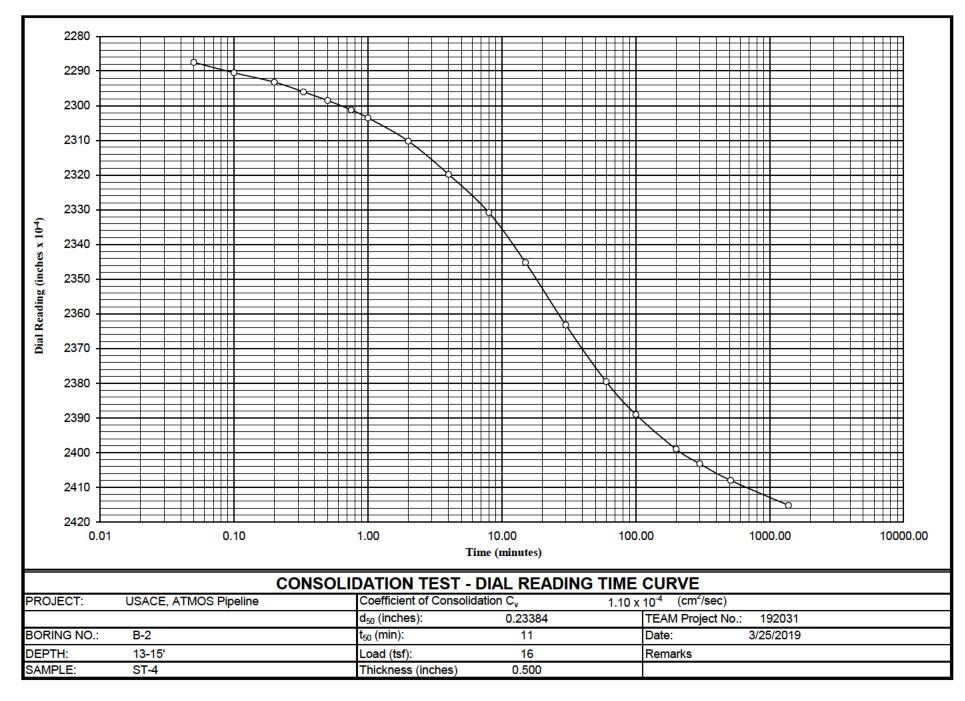
|              |                 |              | TE                     | AM C                                   | Cons        | sulte        | ants            | , In    | с.                     |                                     |             |
|--------------|-----------------|--------------|------------------------|--|-------------|--------------|-----------------|---------|------------------------|-------------------------------------|-------------|
|              |                 | Ge           | eotechnica             | l, Environn                            | -           |              |                 | Materia | ls Testing             |                                     |             |
|              |                 |              |                        | CONSO                                  | LIDATI      | ON TES       | Т               |         |                        |                                     |             |
|              |                 |              |                        | (Time - C                              | onsolida    | ation Da     | ta)             |         |                        |                                     |             |
| Proje        | t.              |              |                        | Dinalina                               |             |              |                 | ТЕЛ     | M. Joh No.             | 102021                              |             |
| -            |                 |              | CE, ATMOS              | -                                      |             |              |                 |         | M Job No.:             |                                     | •           |
| Borin        | ig No.:         |              | B-2                    | Sample No                              | .: <u>S</u> | <u>-4</u> De | epth: 1         | 3-15    | Consol.No.:            | 1                                   | •           |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time    | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/25         | 0.25            | 11:30        | 0                      | 2009                                   | 21          | 3/27         | 8               | 7:15    | 0                      | 2135.5                              | 20          |
| 3/25         | 0.5             | 11:35        | 5                      | 2003                                   |             | 3/27         | 8               | 7:15    | 0.05                   | 2166                                |             |
| 3/25         | 1               | 11:38        | 8                      | 2018                                   |             | 3/27         | 8               | 7:15    | 0.1                    | 2168.5                              |             |
| 3/25         | 1.5             | 12:00        | 30                     | 2029                                   |             | 3/27         | 8               | 7:15    | 0.2                    | 2171                                |             |
| 3/26         | 1.5             | 8:20         | 1250                   | 2038.5                                 | 20          | 3/27         | 8               | 7:15    | 0.33                   | 2174                                |             |
|              |                 |              |                        |  |             | 3/27         | 8               | 7:15    | 0.5                    | 2176                                |             |
|              |                 |              |                        |  |             | 3/27         | 8               | 7:15    | 0.75                   | 2178.5                              |             |
|              |                 |              |                        |  |             | 3/27         | 8               | 7:16    | 1                      | 2180                                |             |
| 3/26         | 4               | 8:20         | 0                      | 2038.5                                 | 20          | 3/27         | 8               | 7:17    | 2                      | 2188                                |             |
| 3/26         | 4               | 8:20         | 0.05                   | 2078                                   |             | 3/27         | 8               | 7:19    | 4                      | 2195                                |             |
| 3/26         | 4               | 8:20         | 0.1                    | 2080.5                                 |             | 3/27         | 8               | 7:23    | 8                      | 2203.2                              |             |
| 3/26         | 4               | 8:20         | 0.2                    | 2083.2                                 |             | 3/27         | 8               | 7:30    | 15                     | 2212.5                              |             |
| 3/26         | 4               | 8:20         | 0.33                   | 2086                                   |             | 3/27         | 8               | 7:45    | 30                     | 2222.5                              |             |
| 3/26         | 4               | 8:20         | 0.5                    | 2088.2                                 |             | 3/27         | 8               | 8:15    | 60                     | 2230                                |             |
| 3/26         | 4               | 8:20         | 0.75                   | 2090.8                                 |             | 3/27         | 8               | 8:55    | 100                    | 2234.5                              |             |
| 3/26         | 4               | 8:21         | 1                      | 2092.2                                 |             | 3/27         | 8               | 10:35   | 200                    | 2238.5                              |             |
| 3/26         | 4               | 8:22         | 2                      | 2096.8                                 |             | 3/27         | 8               | 12:15   | 300                    | 2240.2                              |             |
| 3/26         | 4               | 8:24         | 4                      | 2102                                   |             | 3/27         | 8               | 19:45   | 750                    | 2245                                |             |
| 3/26         | 4               | 8:28         | 8                      | 2108                                   |             | 3/28         | 8               | 8:45    | 1530                   | 2248                                | 20          |
| 3/26<br>3/26 | 4               | 8:35<br>8:50 | 15                     | 2114                                   |             |              |                 |         |                        |                                     |             |
| 3/26         | 4               | 9:20         | 30                     | 2119.8                                 |             |              |                 |         |                        |                                     |             |
| 3/26         | 4               | 9.20         | 60<br>100              | 2124.5                                 |             |              |                 |         |                        |                                     |             |
| 3/26         | 4               | 11:40        | 200                    | 2127<br>2129.2                         |             |              |                 |         |                        |                                     |             |
| 3/26         | 4               | 13:20        | 300                    | 2129.2                                 |             |              |                 |         |                        |                                     |             |
| 3/26         | 4               | 17:00        | 300<br>520             | 2130.8                                 |             |              |                 |         |                        |                                     |             |
| 3/27         | 4               | 7:15         | 1375                   | 2132.2                                 | 20          |              |                 |         |                        |                                     |             |
| JIZI         | 4               | 7.15         | 1375                   | 2155.5                                 | 20          |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |
|              |                 |              |                        |  |             | T4           | chnicia         |         | n Young                |                                     |             |
|              |                 |              |                        |  |             | 16           | conicial        | Jaso    | n roung                |                                     | •           |
|              |                 |              |                        |  |             |              |                 |         |                        |                                     |             |

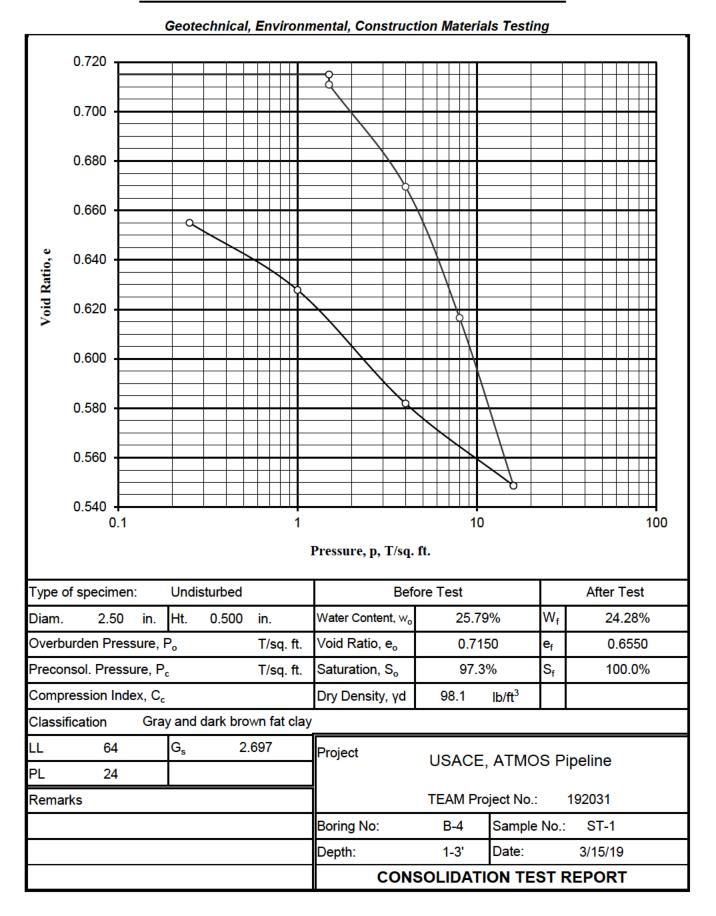
|              |                 |              |                        | AM C                                   |                         |          |                 |               |                        |                                     | -           |
|--------------|-----------------|--------------|------------------------|--|-------------------------|----------|-----------------|---------------|------------------------|-------------------------------------|-------------|
|              |                 | Ge           | eotechnica             | l, Environn                            | -                       |          |                 | Materia       | ls Testing             |                                     |             |
|              |                 |              |                        | CONSO                                  |                         | ON TES   |                 |               |                        |                                     |             |
|              |                 |              |                        | (Time - C                              | onsolida                | ation Da | ta)             |               |                        |                                     |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
| Proje        | ct:             | USA          | CE, ATMOS              | Pipeline                               |                         |          |                 | TEA           | M Job No.:             | 192031                              |             |
| -            |                 |              |                        | Sample No                              | · s                     | [-4 De   | onth: 1         |               |                        |                                     | 1           |
| Dona         | g 110           |              | 02                     | - campie ne                            |                         | <u> </u> |                 |               | 0011001.110            |                                     | •           |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C | Date     | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/28         | 16              | 8:45         | 0                      | 2248                                   | 20                      |          |                 | REBO          |                        | 20                                  |             |
| 3/28         | 16              | 8:45         | 0.05                   | 2287.5                                 |                         |          |                 |               |                        | -                                   |             |
| 3/28         | 16              | 8:45         | 0.1                    | 2290.5                                 |                         | 3/29     | 4               | 7:45          | Rebound                | 2415.2                              | 20          |
| 3/28         | 16              | 8:45         | 0.2                    | 2293.2                                 |                         | 3/30     | 4               | 21:30         | 2265                   | 2295                                | 20          |
| 3/28         | 16              | 8:45         | 0.33                   | 2296                                   |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 8:45         | 0.5                    | 2298.5                                 |                         | 0.10.0   |                 | 01.00         |                        | 0005                                |             |
| 3/28         | 16              | 8:45         | 0.75                   | 2301.2                                 |                         | 3/30     | 1               | 21:30         | Rebound                | 2295                                | 20          |
| 3/28<br>3/28 | 16<br>16        | 8:46<br>8:47 | 1                      | 2303.5                                 |                         | 4/1      | 1               | 8:15          | 2085                   | 2170                                | 19          |
| 3/28         | 16              | 8:49         | 4                      | 2310.2<br>2319.8                       |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 8:53         | 8                      | 2319.8                                 |                         | 4/1      | 0.25            | 8:15          | Rebound                | 2170                                | 19          |
| 3/28         | 16              | 9:00         | 15                     | 2345.2                                 |                         | 4/2      | 0.25            | 8:00          | 1425                   | 2075                                | 20          |
| 3/28         | 16              | 9:15         | 30                     | 2363.2                                 |                         | -112     | 0.20            | 0.00          | 1420                   | 2015                                | 20          |
| 3/28         | 16              | 9:45         | 60                     | 2379.5                                 |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 10:25        | 100                    | 2389                                   |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 12:05        | 200                    | 2399                                   |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 13:45        | 300                    | 2403.2                                 |                         |          |                 |               |                        |                                     |             |
| 3/28         | 16              | 17:15        | 510                    | 2408                                   |                         |          |                 |               |                        |                                     |             |
| 3/29         | 16              | 7:45         | 1380                   | 2415.2                                 | 20                      |          | М               | achine [      | Deflection Re          | adinas                              |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
|              |                 |              |                        |  |                         |          | 0.25            |               |                        | 2009                                |             |
|              |                 |              |                        |  |                         |          | 1.5             |               |                        | 2040                                |             |
|              |                 |              |                        |  |                         |          | 4               |               |                        | 2063                                |             |
|              |                 |              |                        |  |                         |          | 8               |               |                        | 2084                                |             |
|              |                 |              |                        |  |                         |          | 16<br>4         |               |                        | 2109                                |             |
|              |                 |              |                        |  |                         |          | 4               |               |                        | 2073<br>2046                        |             |
|              |                 |              |                        |  |                         |          | 0.25            |               |                        | 2046                                |             |
|              |                 |              |                        |  |                         |          | 0.20            |               |                        | 2020                                |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
|              |                 |              |                        |  |                         |          |                 |               |                        |                                     |             |
|              |                 |              |                        |  |                         | Te       | echnicia        | n <u>Jaso</u> | n Young                |                                     |             |

|                          |                                      | Geotechni                              | cal, Environmen                      | tal, Constructio                | on Materials Tes                                | sting  |               |  |
|--------------------------|--------------------------------------|--|--------------------------------------|---------------------------------|---|--|---------------|--|
|                          |                                      |  | CONSOLI                              | DATION TEST                     |   |  |               |  |
|                          |                                      |  | (Computatio                          | on of Void Ratio)               |   |  |               |  |
| PROJECT                  | USACE, A                             | TMOS Pipeline                          | TEA                                  | M Job No.:                      | 192031  | DATE:  | 3/25/19       |  |
|                          | B-2                                  | SAMP                                   | LE NO. ST-4                          | DEPTH 1                         | 3-15' CONS                                      | OLIDOMETER NO.                                 | 1             |  |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied         | Time in Min.<br>Increment<br>Effective | Dial Reading<br>10 <sup>-4</sup> in. | Correction 10 <sup>-4</sup> in. | Change in<br>Height, ΔH<br>10 <sup>-4</sup> in. | Height of Voids, $H_V$<br>10 <sup>-4</sup> in. | Void Ratio, e |  |
| 0.1                      | 3/25                                 | Zero Point                             | 2000                                 | 2000                            | 0   | 1835   | 0.5800        |  |
| 1.5                      | 3/25                                 | Initial Load                           | 2040                                 | 2040                            | 0   | 1835   | 0.5800        |  |
| 1.5                      | 3/25                                 | 1250                                   | 2038.5                               | 2040                            | 1.5   | 1837   | 0.5804        |  |
| 4                        | 3/26                                 | 1375                                   | 2135.5                               | 2063                            | -72.5   | 1763   | 0.5571        |  |
| 8                        | 3/27                                 | 1530                                   | 2248                                 | 2084                            | -164  | 1671   | 0.5281        |  |
| 16                       | 3/28                                 | 1380                                   | 2415.2                               | 2109                            | -306.2  | 1529   | 0.4832        |  |
| 4                        | 3/29                                 | 2265                                   | 2295                                 | 2073                            | -222  | 1613   | 0.5098        |  |
| 1                        | 3/30                                 | 2085                                   | 2170                                 | 2046                            | -124  | 1711   | 0.5408        |  |
| 0.25                     | 4/1                                  | 1425                                   | 2075                                 | 2026                            | -49   | 1786   | 0.5645        |  |
|                          |                                      |  |                                      |                                 |   |  |               |  |
| Note:<br>Height of vo    | pids, $H_V$ = ( H - H <sub>S</sub> ) | - ΔH                                   | H <sub>s</sub> = 0.3165              |                                 | 1 1   |  |               |  |







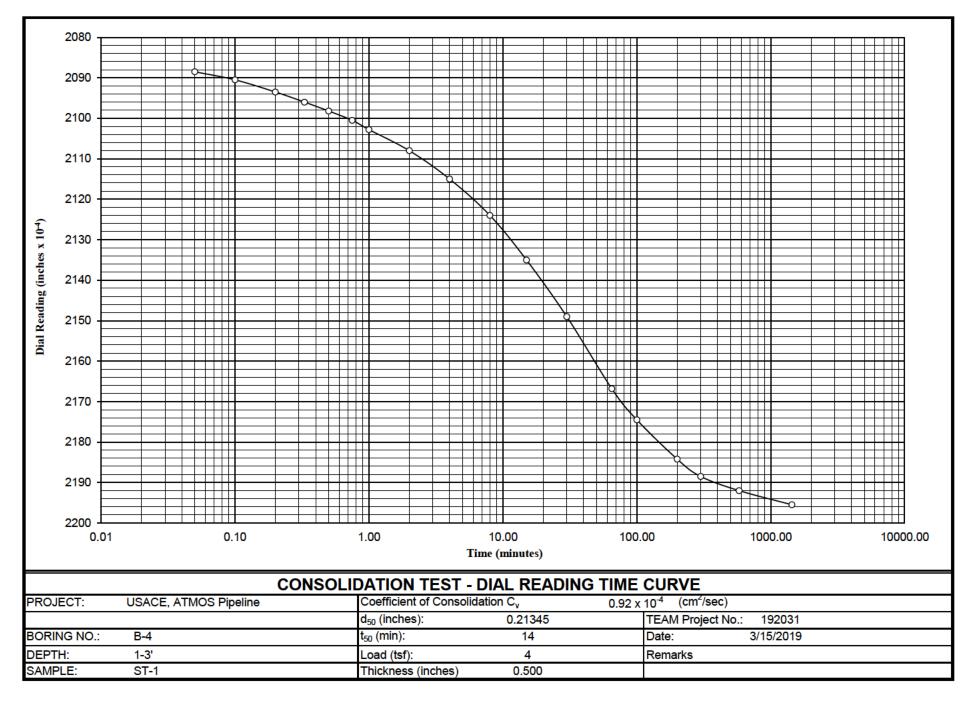


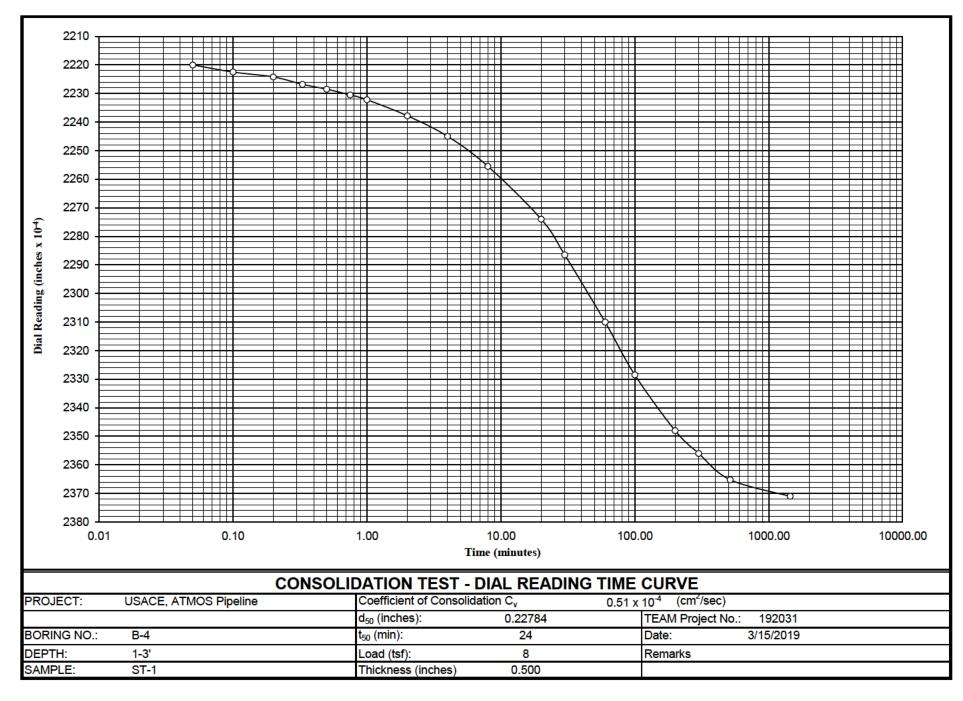
|                                 |  |   |  | DATION TEST<br>imen Data)   |       |              |
|---------------------------------|--|---|--|---|-------|--------------|
|                                 |  | E, ATMO<br>-4                                 | S Pipeline<br>Sample No.: <u>ST-1</u>  | TEAM Job No.:<br>Depth:1-3' Date:   |       | 031<br>15/19 |
| Class                           | ification Gray   | and dark                                      | brown fat clay   |   |       |              |
| 01400                           | inclution oray   |   |  | ore Test  |       | After Test   |
|                                 |  |   | Specimen   | Trimmings   |       | Specimen     |
|                                 | Tare No.   |   | Ring and Plates  | 630   |       | 440          |
| ns                              | Tare plus wet  | soil  | 189.56   | 522.45  |       | 114.13       |
| grar                            | Tare plus dry  | soil  | 173.25   | 457.91  |       | 98.77        |
| Weight in grams                 | Water  | Ww  | W <sub>WO</sub> 16.31  | 64.54   | Wwf   | 15.36        |
| leigh                           | Tare   |   | 110.00   | 207.61  |       | 35.52        |
| 3                               | Dry soil   | Ws  | 63.25  | 250.30  |       | 63.25        |
| W                               | ater Content   | w   | W <sub>0</sub> 25.79%  | 25.79%  | Wf    | 24.28%       |
| (                               | Consolidometer No  | .:  | 1  | Area of specimen, A, (sq.   | cm.)  | 31.67        |
|                                 | Weight of ring, g  |   | N/A  | Height of specimen, H,  | (in.) | 0.500        |
|                                 | Weight of plates, g  |   | N/A  | Specific Gravity of solids, (   | Gs)   | 2.697        |
| Final<br>Net c<br>Heigl<br>Void | height of water, H <sub>t</sub><br>change in height of<br>ht of specimen at e<br>ratio before test, e <sub>t</sub> | $w_f = \frac{V}{F}$<br>specimen<br>nd of test | , H <sub>f</sub> = H - ΔH = 0.48   | $\frac{15.36}{37 \times 1 \times 2.54} = 0.190$ $0.01750  \text{in.}$ $325  \text{in.}$ $0.2915 = 0.7150$ | 9 in. |              |
| Degr<br>Degr                    | ee of saturation be<br>ee of saturation aft  | fore test, s<br>er test, S <sub>f</sub>       | $S_{0} = \frac{H_{WO}}{H - H_{S}} = \frac{-1}{0}$ $= \frac{H_{wf}}{H_{f} - H_{S}} = \frac{-1}{0.48}$ |   |       | ı.ft.        |
| Rem                             | arks   |   |  |   |       |              |
|                                 | nician Jas   |   |  |   |       |              |

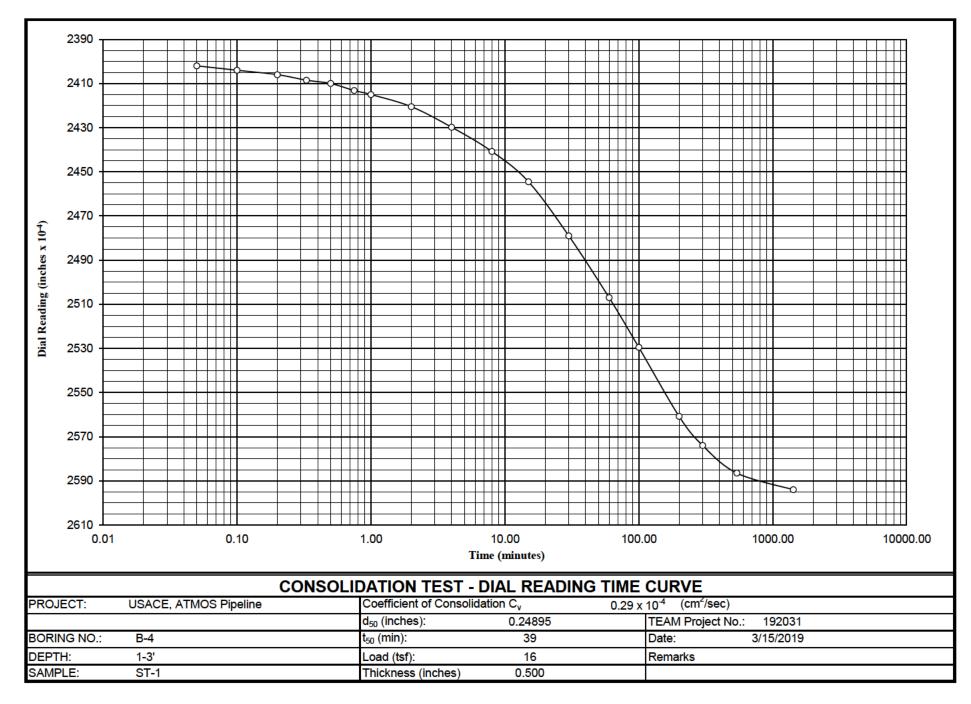
| Date (tsf) Time Time, (min) ( $10^4$ in.) °C Date (tsf) Time Time, (min) ( $10^4$ in.) °C   |       |       |       | TE.        | AM C      | Cons     | sulte    | ants     | s, In         | с.          |        |             |
|---|-------|-------|-------|------------|-----------|----------|----------|----------|---------------|-------------|--------|-------------|
| Time - Consolidation Data)           Project:         USACE, ATMOS Pipeline         TEAM Job No.:         192031           Boring No.:         B-4         Sample No.:         ST-1         Depth:         1-3'         Consol.No.:         1           Date         Press.<br>(tst)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>Press.         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>Press.           3/15         0.125         9:55         0         2004         20         3/19         8         8:40         0.2220         2201           3/15         0.15         9:57         2         2003         3/19         8         8:40         0.22         2224.2         1           3/15         1.5         11:40         105         2035         3/19         8         8:40         0.2         2224.2         1           3/18         1.5         8:00         4205         2052         19         3/19         8         8:40         0.75         2230.5         1           3/18         4         8:35         0.2         2093.5         3/19         8         8:41         1         2232.2         1  |       |       | Ge    | eotechnica | -         | -        |          |          | Materia       | ls Testing  |        | -           |
| Project:         USACE, ATMOS Pipeline         TEAM Job No.:         192031           Boring No.:         B-4         Sample No.:         ST-1         Deth:         1-3'         Consol.No.:         1           Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>0°C         Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>0°C           3/15         0.25         9:55         0         2004         20         3/19         8         8:40         0.21         22205         2           3/15         0.25         9:56         1         1992         3/19         8         8:40         0.21         2224.2         3/19         1         8:8:40         0.22         2224.2         3/19         1         1:5         1:0         1:0         105         2035         3/19         8         8:40         0.25         2220.5         1         3/19         8         8:40         0.75         2230.5         1         3/19         8         8:41         1         2232.2         1         3/18         4         8:35         0.2         2095.5         3/19         8         8:44   |       |       |       |            | CONSO     | LIDATI   | ON TES   | Т        |               |             |        |             |
| Boring No.:         B-4         Sample No.:         ST-1         Depth:         1-3'         Consol.No.:         1           Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> n.)         Temp.<br>OC         Date         Press.(tsf)         Time         ElapsedTime, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Date         Date <tdd< td=""><td></td><td></td><td></td><td></td><td>(Time - C</td><td>onsolida</td><td>ation Da</td><td>ta)</td><td></td><td></td><td></td><td></td></tdd<>  |       |       |       |            | (Time - C | onsolida | ation Da | ta)      |               |             |        |             |
| Boring No.:         B-4         Sample No.:         ST-1         Depth:         1-3'         Consol.No.:         1           Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> n.)         Temp.<br>OC         Date         Press.(tsf)         Time         ElapsedTime, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Date         Date <tdd< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tdd<>  |       |       |       |            |           |          |          |          |               |             |        |             |
| Boring No.:         B-4         Sample No.:         ST-1         Depth:         1-3'         Consol.No.:         1           Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> n.)         Temp.<br>OC         Date         Press.(tsf)         Time         ElapsedTime, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Time, (min)         Temp.(104 n.)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Time, (min)         Date         Press.(tsf)         Date         Date <tdd< td=""><td>Proie</td><td>ct:</td><td>USA</td><td>CE. ATMOS</td><td>Pipeline</td><td></td><td></td><td></td><td>TEA</td><td>M Job No.:</td><td>192031</td><td></td></tdd<>   | Proie | ct:   | USA   | CE. ATMOS  | Pipeline  |          |          |          | TEA           | M Job No.:  | 192031 |             |
| Date         Press,<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>oC         Date         Press.<br>(tsf)         Time         Elapsed<br>Time, (min)         Dial Reading<br>(10 <sup>4</sup> in.)         Temp.<br>oC           3/15         0.125         9:55         0         2004         20         3/19         8         8:40         0         2195.5         20           3/15         0.25         9:56         1         1992         3/19         8         8:40         0.01         2222.5         20           3/15         1         9:59         4         2021         3/19         8         8:40         0.2         2224.2         2           3/15         1.5         11:40         105         2035         3/19         8         8:40         0.33         2226.8           3/18         1.5         8:00         4205         2052         19         3/19         8         8:40         0.75         2230.5           -         -         -         3/19         8         8:44         4         2245           3/18         4         8:35         0.1         2090.5         3/19         8         9:40         60         23   | -     |       |       |            |           |          | [_1 D4   | anth:    |               |             |        | •           |
|   | Donin | y No  |       | 0-4        |           |          |          |          | 1-0           | 0011301.140 | I      | •           |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | Date  |       | Time  |            |           |          | Date     |          | Time          |             |        | Temp.<br>°C |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 3/15  | 0.125 | 9:55  | 0          | 2004      | 20       | 3/19     | 8        | 8:40          | 0           | 2195.5 | 20          |
| 3/15       1       9:59       4       2021       3/19       8       8:40       0.2       2224.2         3/15       1.5       11:40       105       2035       3/19       8       8:40       0.33       2226.8         3/18       1.5       8:00       4205       2052       19       3/19       8       8:40       0.5       2228.5         3/18       4       8:35       0       2052       19       3/19       8       8:40       0.75       2230.5         3/18       4       8:35       0       2052       19       3/19       8       8:41       1       2232.2         3/18       4       8:35       0.1       2090.5       3/19       8       8:44       4       2245         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.5       2098.2       3/19       8       9:10       30       2286.5         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:37<   | 3/15  | 0.25  | 9:56  | 1          | 1992      |          | 3/19     | 8        | 8:40          | 0.05        | 2220   |             |
| 3/15       1.5       11:40       105       2035       3/19       8       8:40       0.33       2226.8         3/18       1.5       8:00       4205       2052       19       3/19       8       8:40       0.5       2228.5         3/18       4       8:35       0       2052       19       3/19       8       8:40       0.75       2230.5         3/18       4       8:35       0       2052       19       3/19       8       8:41       1       2232.2         3/18       4       8:35       0.05       2088.5       3/19       8       8:42       2       2237.8         3/18       4       8:35       0.1       2090.5       3/19       8       8:48       8       2255.5         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.5       2098.2       3/19       8       9:10       30       2286.5         3/18       4       8:36       1       2102.8       3/19       8       10:20       100       2328.5         3/18       4       8:3   |       | 0.5   | 9:57  | 2          | 2003      |          | 3/19     | 8        | 8:40          | 0.1         | 2222.5 |             |
| 3/18 $1.5$ $8:00$ $4205$ $2052$ $19$ $3/19$ $8$ $8:40$ $0.5$ $2228.5$ $1.5$ $8:00$ $4205$ $2052$ $19$ $3/19$ $8$ $8:40$ $0.75$ $2223.5$ $3/18$ $4$ $8:35$ $0$ $2052$ $19$ $3/19$ $8$ $8:41$ $1$ $2232.2$ $3/18$ $4$ $8:35$ $0.05$ $2088.5$ $3/19$ $8$ $8:44$ $4$ $22455$ $3/18$ $4$ $8:35$ $0.1$ $2090.5$ $3/19$ $8$ $8:48$ $8$ $2255.5$ $3/18$ $4$ $8:35$ $0.2$ $2093.5$ $3/19$ $8$ $9:00$ $20$ $2274$ $3/18$ $4$ $8:35$ $0.5$ $2098.2$ $3/19$ $8$ $9:00$ $20$ $2274$ $3/18$ $4$ $8:35$ $0.5$ $2098.2$ $3/19$ $8$ $10:20$ $100$ $2328.5$ $3/19$ $8$ $10:20$ $100$ $2328.5$ $3/18$  | 3/15  | 1     | 9:59  | 4          | 2021      |          | 3/19     | 8        | 8:40          | 0.2         | 2224.2 |             |
| Image: state of the s | 3/15  | 1.5   | 11:40 | 105        | 2035      |          | 3/19     | 8        | 8:40          | 0.33        | 2226.8 |             |
| 3/19         8         8:41         1         2232.2           3/18         4         8:35         0         2052         19         3/19         8         8:42         2         2237.8           3/18         4         8:35         0.05         2088.5         3/19         8         8:44         4         2245           3/18         4         8:35         0.1         2090.5         3/19         8         8:44         4         2245           3/18         4         8:35         0.2         2093.5         3/19         8         9:00         20         2274           3/18         4         8:35         0.33         2096         3/19         8         9:00         20         2286.5           3/18         4         8:35         0.5         2098.2         3/19         8         9:40         60         2310           3/18         4         8:35         0.75         2100.5         3/19         8         10:20         100         2328.5           3/18         4         8:37         2         2108         3/19         8         13:40         300         2365.2           3/18 <t< td=""><td>3/18</td><td>1.5</td><td>8:00</td><td>4205</td><td>2052</td><td>19</td><td></td><td>8</td><td></td><td>0.5</td><td>2228.5</td><td></td></t<>   | 3/18  | 1.5   | 8:00  | 4205       | 2052      | 19       |          | 8        |               | 0.5         | 2228.5 |             |
| 3/18       4       8:35       0       2052       19       3/19       8       8:42       2       2237.8         3/18       4       8:35       0.05       2088.5       3/19       8       8:44       4       2245         3/18       4       8:35       0.1       2090.5       3/19       8       8:48       8       2255.5         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.3       2096       3/19       8       9:00       20       2274         3/18       4       8:35       0.5       2098.2       3/19       8       9:10       30       2286.5         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:37       2       2108       3/19       8       13:40       300       2365.2         3/18       4       8:33       4       2115   |       |       |       |            |           |          | 3/19     | 8        | 8:40          | 0.75        | 2230.5 |             |
| 3/18       4       8:35       0.05       2088.5       3/19       8       8:44       4       2245         3/18       4       8:35       0.1       2090.5       3/19       8       8:48       8       2255.5         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.33       2096       3/19       8       9:00       20       2274         3/18       4       8:35       0.5       2098.2       3/19       8       9:40       60       2310         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       1445       2371       20         3/18       4       8:43       8       2124       3/20   |       |       |       |            |           |          |          |          | 8:41          |             | 2232.2 |             |
| 3/18       4       8:35       0.1       2090.5       3/19       8       8:48       8       2255.5         3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.33       2096       3/19       8       9:10       30       2286.5         3/18       4       8:35       0.5       2098.2       3/19       8       9:40       60       2310         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       9:05       30       2149  |       | 4     |       | 0          | 2052      | 19       |          | -        | 8:42          | 2           | 2237.8 |             |
| 3/18       4       8:35       0.2       2093.5       3/19       8       9:00       20       2274         3/18       4       8:35       0.33       2096       3/19       8       9:10       30       2286.5         3/18       4       8:35       0.5       2098.2       3/19       8       9:40       60       2310         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       9:05       30       2149               3/18       4       10:15       100       2174.5  |       | 4     |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:35       0.33       2096       3/19       8       9:10       30       2286.5         3/18       4       8:35       0.5       2098.2       3/19       8       9:40       60       2310         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135       -       -       -       -       -         3/18       4       9:05       30       2149       -       -       -       -       -       -         3/18       4       10:15       100       2174.5       <   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:35       0.5       2098.2       3/19       8       9:40       60       2310         3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135               3/18       4       9:05       30       2149 <td></td>   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:35       0.75       2100.5       3/19       8       10:20       100       2328.5         3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135       -       -       -       -       -         3/18       4       9:05       30       2149       -       -       -       -       -       -         3/18       4       9:40       65       2166.8       - <td< td=""><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>   |       | -     |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:36       1       2102.8       3/19       8       12:00       200       2348         3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       9:05       30       2149                   3/18       4       9:05       30       2174.5                3/18       4       10:15       100       2174.5               3/18       4       13:35       300       2188.5   |       | -     |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:37       2       2108       3/19       8       13:40       300       2356         3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:39       4       2115       3/19       8       17:15       515       2365.2         3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135       -  |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:43       8       2124       3/20       8       8:45       1445       2371       20         3/18       4       8:50       15       2135       -   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       8:50       15       2135       15       2135         3/18       4       9:05       30       2149       10       10         3/18       4       9:40       65       2166.8       10       10         3/18       4       10:15       100       2174.5       10       10       2174.5         3/18       4       11:55       200       2184.2       10       10       2184.2         3/18       4       13:35       300       2188.5       10       10       10         3/18       4       18:15       580       2192       10       10       10   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       9:05       30       2149       Image: constraint of the stress of the stres  |       |       |       |            |           |          | 3/20     | 8        | 8:45          | 1445        | 2371   | 20          |
| 3/18       4       9:40       65       2166.8 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       10:15       100       2174.5   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       11:55       200       2184.2   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18       4       13:35       300       2188.5  <  |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/18 4 18:15 580 2192   |       |       |       |            |           |          |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
| 3/19     4     6.33     1440     2193.5     20     - <td></td> <td></td> <td></td> <td></td> <td></td> <td>20</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>  |       |       |       |            |           | 20       |          |          |               |             |        |             |
|   | 5/19  | 4     | 0.55  | 1440       | 2195.5    | 20       |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
|   |       |       |       |            |           |          |          |          |               |             |        |             |
| Technician Jason Young  |       |       |       |            |           |          | Τe       | echnicia | n <u>Jaso</u> | n Young     |        |             |

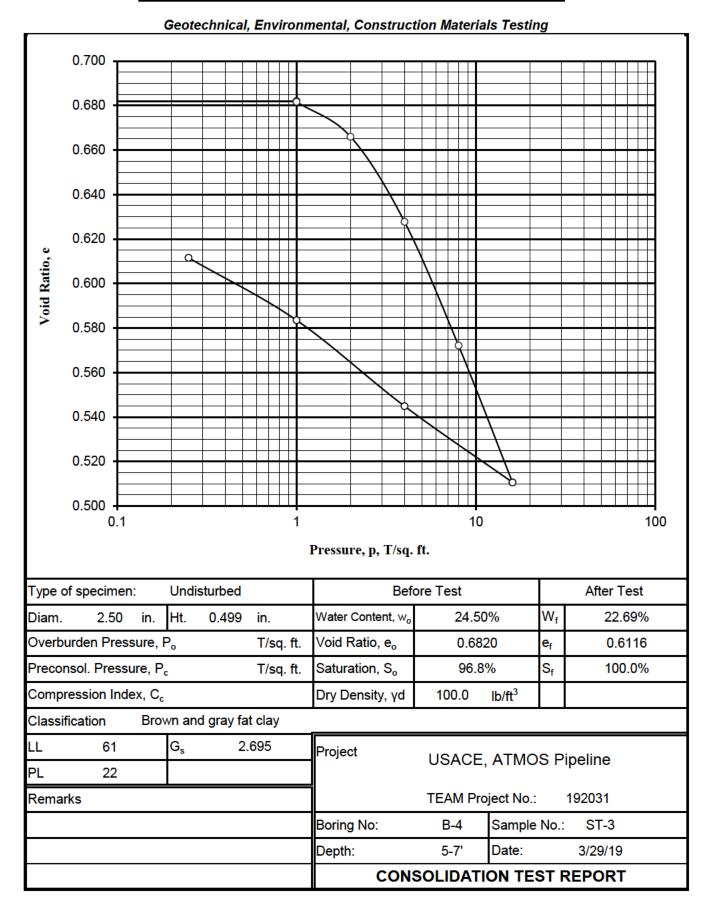
|              |                 | Ge           |                        | AM C                                   |             |              |                 |          |                        |  |             |
|--------------|-----------------|--------------|------------------------|--|-------------|--------------|-----------------|----------|------------------------|--|-------------|
|              |                 |              |                        | CONSO                                  |             |              |                 |          |                        |  |             |
|              |                 |              |                        | /Time C                                |             | tion Do      | <b>t</b> a)     |          |                        |  |             |
|              |                 |              |                        | (Time - C                              | onsolida    | ation Da     | ta)             |          |                        |  |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
| Proje        | ect:            | USA          | CE, ATMOS              | Pipeline                               |             |              |                 | TEA      | M Job No.:             | 192031                                 |             |
| Borin        | g No.:          |              | B-4                    | Sample No                              | .: S        | [-1De        | epth:           | 1-3'     | Consol.No.:            | 1                                      |             |
|              |                 |              |                        |  |             |              |                 |          |                        | 1                                      |             |
| Date         | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time     | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/20         | 16              | 8:45         | 0                      | 2371                                   | 20          |              |                 | RFB      |                        | )S                                     |             |
| 3/20         | 16              | 8:45         | 0.05                   | 2402                                   |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 8:45         | 0.1                    | 2404                                   |             | 3/21         | 4               | 8:30     | Rebound                | 2594                                   | 20          |
| 3/20         | 16              | 8:45         | 0.2                    | 2406                                   |             | 3/22         | 4               | 9:20     | 1490                   | 2461                                   | 20          |
| 3/20         | 16              | 8:45         | 0.33                   | 2408.5                                 |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 8:45         | 0.5                    | 2410                                   |             | 2/22         | 4               | 0.00     |                        | 0.404                                  | 20          |
| 3/20<br>3/20 | 16              | 8:45         | 0.75                   | 2413.2                                 |             | 3/22<br>3/24 | 1               | 9:20     | Rebound                | 2461                                   | 20          |
| 3/20         | 16<br>16        | 8:46<br>8:47 | 1                      | 2415<br>2420.5                         |             | 3/24         | 1               | 14:15    | 3175                   | 2300.2                                 | 20          |
| 3/20         | 16              | 8:49         | 4                      | 2420.3                                 |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 8:53         | 8                      | 2440.8                                 |             | 3/24         | 0.25            | 14:15    | Rebound                | 2300.2                                 | 20          |
| 3/20         | 16              | 9:00         | 15                     | 2454.5                                 |             | 3/25         | 0.25            | 17:30    | 1635                   | 2200                                   | 21          |
| 3/20         | 16              | 9:15         | 30                     | 2479                                   |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 9:45         | 60                     | 2507                                   |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 10:25        | 100                    | 2529.5                                 |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 12:05        | 200                    | 2560.8                                 |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 13:45        | 300                    | 2574                                   |             |              |                 |          |                        |  |             |
| 3/20         | 16              | 17:45        | 540                    | 2586.5                                 |             |              |                 |          |                        |  |             |
| 3/21         | 16              | 8:30         | 1425                   | 2594                                   | 20          |              | M               | achine D | eflection Re           | adinas                                 |             |
|              |                 |              |                        |  |             |              |                 |          |                        | -                                      |             |
|              |                 |              |                        |  |             |              | 0.125           |          |                        | 2004                                   |             |
|              |                 |              |                        |  |             |              | 1.5<br>4        |          |                        | 2040<br>2063                           |             |
|              |                 |              |                        |  |             |              | 4<br>8          |          |                        | 2083                                   |             |
|              |                 |              |                        |  |             |              | 16              |          |                        | 2109                                   |             |
|              |                 |              |                        |  |             |              | 4               |          |                        | 2073                                   |             |
|              |                 |              |                        |  |             |              | 1               |          |                        | 2046                                   |             |
|              |                 |              |                        |  |             |              | 0.25            |          |                        | 2026                                   |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
|              |                 |              |                        |  |             |              |                 |          |                        |  |             |
|              |                 |              |                        |  |             | Te           | echniciar       | n Jaso   | n Young                |  |             |

|                          |                              | Geotechni                              | cal, Environmen                      | ntal, Constructio                  | on Materials Te                                 | sting  |               |
|--------------------------|------------------------------|--|--------------------------------------|------------------------------------|---|--|---------------|
|                          |                              |  | CONSOLI                              | DATION TEST                        |   |  |               |
|                          |                              |  | (Computatio                          | on of Void Ratio)                  |   |  |               |
| ROJECT                   | USACE, A                     | TMOS Pipeline                          | TEA                                  | M Job No.:                         | 192031  | DATE:  | 3/15/19       |
| BORING NO.               | B-4                          | SAMP                                   | LE NO. ST-1                          | DEPTH                              | 1-3' CONS                                       |  | 1             |
| Pressure, P<br>T./sq.ft. | Date<br>Increment<br>Applied | Time in Min.<br>Increment<br>Effective | Dial Reading<br>10 <sup>-4</sup> in. | Correction<br>10 <sup>-4</sup> in. | Change in<br>Height, ΔH<br>10 <sup>-4</sup> in. | Height of<br>Voids, H <sub>V</sub><br>10 <sup>-4</sup> in, | Void Ratio, e |
| 0.1                      | 3/15                         | Zero Point                             | 2000                                 | 2000                               | 0   | 2085   | 0.7150        |
| 1.5                      | 3/15                         | Initial Load                           | 2040                                 | 2040                               | 0   | 2085   | 0.7150        |
| 1.5                      | 3/15                         | 4205                                   | 2052                                 | 2040                               | -12   | 2073   | 0.7109        |
| 4                        | 3/18                         | 1440                                   | 2195.5                               | 2063                               | -132.5  | 1952   | 0.6696        |
| 8                        | 3/19                         | 1445                                   | 2371                                 | 2084                               | -287  | 1798   | 0.6166        |
| 16                       | 3/20                         | 1425                                   | 2594                                 | 2109                               | -485  | 1600   | 0.5487        |
| 4                        | 3/21                         | 1490                                   | 2461                                 | 2073                               | -388  | 1697   | 0.5819        |
| 1                        | 3/22                         | 3175                                   | 2300.2                               | 2046                               | -254.2  | 1830   | 0.6278        |
| 0.25                     | 3/24                         | 1635                                   | 2201                                 | 2026                               | -175  | 1910   | 0.6550        |
|                          |                              |  |                                      |                                    |   |  |               |
|                          |                              |  |                                      |                                    |   |  |               |
| Note:<br>Height of v     | roids, $H_V = (H - H_S)$     | - ΔH                                   | H <sub>s</sub> = 0.2915              |                                    |   |  |               |









|                                |  |                                       |   |  | IDATION TE<br>cimen Data)                             | ST                    |           |                 |               |
|--------------------------------|--|---------------------------------------|---|--|---|-----------------------|-----------|-----------------|---------------|
| Р                              | roject: USAC   | E. ATM                                | OS Pipeline   |  |   | TEAM Job              | No.:      | 192             | 031           |
|                                |  | -4                                    | Sample No.:   | ST-3   | Depth:  | 5-7'                  | Date:     |                 |               |
| Class                          | sification Brow  | /n and o                              | ray fat clay  |  |   |                       |           |                 |               |
| Chaot                          | Bron   | in and g                              | aj lat olaj   | Be   | fore Test   |                       |           |                 | After Test    |
|                                |  |                                       | Spec  | imen   |   | Trimmings             |           |                 | Specimen      |
|                                | Tare No.   |                                       |   | d Plates   |   | 662                   |           |                 | 440           |
| ns                             | Tare plus wet  | soil                                  | 190   | ).06   |   | 602.15                |           |                 | 114.42        |
| gran                           | Tare plus dry  | soil                                  | 174   | 4.30   |   | 524.51                |           |                 | 99.83         |
| Weight in grams                | Water  | Ww                                    | W <sub>WO</sub> 15.                                   | 76   |   | 77.64                 |           | W <sub>wf</sub> | <b>14</b> .59 |
| eigh                           | Tare   |                                       | 110   | 0.00   |   | 207.64                |           |                 | 35.53         |
| 3                              | Dry soil   | Ws                                    | 64  | .30  |   | 316.87                |           |                 | 64.30         |
| N                              | Vater Content  | w                                     | W <sub>0</sub> 24.5                                   | 50%  |   | 24.50%                |           | W <sub>f</sub>  | 22.69%        |
| (                              | Consolidometer No  |                                       | 2   | 2  | Area  | of specimen,          | A, (sq. c | cm.)            | 31.67         |
|                                | Weight of ring, g  |                                       | N   | /A   | Heig  | ht of specimer        | i, H, (   | in.)            | 0.499         |
|                                | Weight of plates, g  | ļ                                     | N   | /A   | Speci   | fic Gravity of s      | olids, (  | Gs)             | 2.695         |
| Final<br>Net o<br>Heig<br>Void | inal height of water<br>I height of water, H<br>change in height of<br>ht of specimen at e<br>I ratio before test, e<br>I ratio after test, e <sub>f</sub> | wr =<br>specime<br>end of te<br>o = = | st, H <sub>f</sub> = H - ΔH =<br>H - H <sub>S</sub> = | 31.<br>31.<br>, ΔH =<br>0.4<br>0.499 -<br>0.2967 | 14.59<br>67 x 1 x 2<br>-0.02090<br>781 ir<br>0.2967 = | in.<br>n.<br>= 0.6820 | = 0.19    |                 | in.           |
|                                | ree of saturation be<br>ree of saturation aff  | ter test,                             |   | - = - 0.4  | 0.1814<br>781 - 0.1                                   | 2967 =                | 100.0%    | 6               |               |
|                                |  | Yd -                                  |   |  |   |                       |           |                 | .tt.          |
| Dry (                          | aarks  |                                       |   |  |   |                       |           |                 | .tt.          |

| -          |                 |               | IE                     | AM C                                   | ons           | sult        | ants            | 5, In         | С.                     |                                     |             |
|------------|-----------------|---------------|------------------------|--|---------------|-------------|-----------------|---------------|------------------------|-------------------------------------|-------------|
|            |                 | Ge            | eotechnica             | l, Environn                            | -             |             |                 | Materia       | ls Testing             |                                     |             |
|            |                 |               |                        | CONSO                                  |               | ON TES      | Т               |               |                        |                                     |             |
|            |                 |               |                        | (Time - C                              | onsolida      | ation Da    | ita)            |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 |               |                        |                                     |             |
| Proje      | ct:             | USA           | CE, ATMOS              | Pipeline                               |               |             |                 | TEA           | M Job No.:             | 192031                              |             |
| Borin      | g No.:          |               | B-4                    | Sample No                              | .: <u>S</u> T | <u>-3</u> D | epth:           | 5-7'          | Consol.No.:            | 2                                   |             |
| Date       | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C   | Date        | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/29       | 0.25            | 13:10         | 0                      | 2008                                   | 20            | 4/2         | 4               | 9:05          | 0                      | 2094.5                              | 20          |
| 3/29       | 0.5             | 13:15         | 5                      | 2005                                   |               | 4/2         | 4               | 9:05          | 0.05                   | 2128                                |             |
| 3/29       | 0.75            | 14:00         | 50                     | 2010                                   |               | 4/2         | 4               | 9:05          | 0.1                    | 2131                                |             |
| 3/29       | 1               | 16:00         | 170                    | 2023                                   |               | 4/2         | 4               | 9:05          | 0.2                    | 2134                                |             |
| 4/1        | 1               | 8:20          | 4030                   | 2032                                   | 19            | 4/2         | 4               | 9:05          | 0.33                   | 2137.8                              |             |
|            |                 |               |                        |  |               | 4/2         | 4               | 9:05          | 0.5                    | 2140                                |             |
|            |                 |               |                        |  |               | 4/2         | 4               | 9:05          | 0.75                   | 2143                                |             |
|            |                 |               |                        |  |               | 4/2         | 4               | 9:06          | 1                      | 2145.2                              |             |
| 4/1        | 2               | 8:20          | 0                      | 2032                                   | 19            | 4/2         | 4               | 9:07          | 2                      | 2151.2                              |             |
| 4/1        | 2               | 8:20          | 0.05                   | 2051                                   |               | 4/2         | 4               | 9:09          | 4                      | 2158                                |             |
| 4/1        | 2               | 8:20          | 0.1                    | 2052.5                                 |               | 4/2         | 4               | 9:13          | 8                      | 2166.8                              |             |
| 4/1        | 2               | 8:20          | 0.2                    | 2054                                   |               | 4/2         | 4               | 9:20          | 15                     | 2175.5                              |             |
| 4/1        | 2               | 8:20          | 0.33                   | 2055.5                                 |               | 4/2         | 4               | 9:35          | 30                     | 2186                                |             |
| 4/1        | 2               | 8:20          | 0.5                    | 2056.8                                 |               | 4/2         | 4               | 10:05         | 60                     | 2198.8                              |             |
| 4/1        | 2               | 8:20          | 0.75                   | 2058                                   |               | 4/2         | 4               | 10:45         | 100                    | 2207                                |             |
| 4/1        | 2               | 8:21          | 1                      | 2059                                   |               | 4/2         | 4               | 12:25         | 200                    | 2215                                |             |
| 4/1        | 2               | 8:22          | 2                      | 2061.8                                 |               | 4/2         | 4               | 14:05         | 300                    | 2219.5                              |             |
| 4/1        | 2               | 8:24          | 4                      | 2064.8                                 |               | 4/2         | 4               | 17:00         | 475                    | 2222.2                              |             |
| 4/1        | 2               | 8:28          | 8                      | 2068.2                                 |               | 4/3         | 4               | 7:55          | 1370                   | 2226                                | 20          |
| 4/1<br>4/1 | 2               | 8:35<br>8:50  | 15                     | 2072                                   |               |             |                 |               |                        |                                     |             |
| 4/1        | 2               | 9:20          | 30<br>60               | 2076.2<br>2080.8                       |               |             |                 |               |                        |                                     |             |
| 4/1        | 2               | 9.20<br>10:00 | 100                    | 2080.8                                 |               |             |                 |               |                        |                                     |             |
| 4/1        | 2               | 11:40         | 200                    | 2084                                   |               |             |                 |               |                        |                                     |             |
| 4/1        | 2               | 13:20         | 300                    | 2000                                   |               |             |                 |               |                        |                                     |             |
| 4/1        | 2               | 17:00         | 520                    | 2090.2                                 |               |             |                 |               |                        |                                     |             |
| 4/2        | 2               | 9:05          | 1485                   | 2092.5                                 | 20            |             |                 |               |                        |                                     |             |
|            | -               | 0.00          | 100                    | 2007.0                                 |               |             |                 |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 |               |                        |                                     |             |
|            |                 |               |                        |  |               |             |                 | 1             |                        |                                     |             |
|            |                 |               |                        |  |               | Te          | echnicia        | n <u>Jaso</u> | n Young                |                                     |             |

|            |                 |              |                        | AM C                                |             |              |                 |               |                        |                                     |             |
|------------|-----------------|--------------|------------------------|-------------------------------------|-------------|--------------|-----------------|---------------|------------------------|-------------------------------------|-------------|
|            |                 | Ge           | eolechnica             | <i>l, Environn</i><br>CONSO         | -           |              |                 | Materia       | ls Testing             |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        | (Time - C                           | onsolida    | ation Da     | ita)            |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
| Proje      |                 |              | CE, ATMOS              |                                     |             |              |                 |               | M Job No.:             |                                     | •           |
| Borir      | ng No.:         |              | B-4                    | Sample No                           | .: <u>S</u> | <u>-3</u> De | epth:           | 5-7'          | Consol.No.:            | 2                                   |             |
| Date       | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C | Date         | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 4/3        | 8               | 7:55         | 0                      | 2226                                | 20          | 4/4          | 16              | 8:25          | 0                      | 2409                                | 21          |
| 4/3        | 8               | 7:55         | 0.05                   | 2272                                |             | 4/4          | 16              | 8:25          | 0.05                   | 2449                                |             |
| 4/3        | 8               | 7:55         | 0.1                    | 2276                                |             | 4/4          | 16              | 8:25          | 0.1                    | 2452                                |             |
| 4/3        | 8               | 7:55         | 0.2                    | 2280                                |             | 4/4          | 16              | 8:25          | 0.2                    | 2454.8                              |             |
| 4/3        | 8               | 7:55         | 0.33                   | 2283.2                              |             | 4/4          | 16              | 8:25          | 0.33                   | 2457.8                              |             |
| 4/3        | 8               | 7:55         | 0.5                    | 2286                                |             | 4/4          | 16              | 8:25          | 0.5                    | 2460.2                              |             |
| 4/3        | 8               | 7:55         | 0.75                   | 2288.8                              |             | 4/4          | 16              | 8:25          | 0.75                   | 2463.2                              |             |
| 4/3<br>4/3 | 8<br>8          | 7:56<br>7:57 | 1                      | 2291<br>2297.2                      |             | 4/4<br>4/4   | 16<br>16        | 8:26<br>8:27  | 1<br>2                 | 2465.5<br>2472.2                    |             |
| 4/3        | 8               | 7:59         | 4                      | 2305.2                              |             | 4/4          | 16              | 8:29          | 4                      | 2472.2                              |             |
| 4/3        | 8               | 8:03         | 8                      | 2303.2                              |             | 4/4          | 16              | 8:33          | 8                      | 2492.5                              |             |
| 4/3        | 8               | 8:10         | 15                     | 2327                                |             | 4/4          | 16              | 8:40          | 15                     | 2507                                |             |
| 4/3        | 8               | 8:25         | 30                     | 2342.2                              |             | 4/4          | 16              | 8:55          | 30                     | 2526.8                              |             |
| 4/3        | 8               | 8:55         | 60                     | 2361.5                              |             | 4/4          | 16              | 9:25          | 60                     | 2552                                |             |
| 4/3        | 8               | 9:35         | 100                    | 2375.5                              |             | 4/4          | 16              | 10:05         | 100                    | 2572.8                              |             |
| 4/3        | 8               | 11:15        | 200                    | 2391.8                              |             | 4/4          | 16              | 11:45         | 200                    | 2595.5                              |             |
| 4/3        | 8               | 12:55        | 300                    | 2397                                |             | 4/4          | 16              | 13:25         | 300                    | 2603.2                              |             |
| 4/3        | 8               | 17:00        | 545                    | 2403.5                              |             | 4/4          | 16              | 17:00         | 515                    | 2609.5                              |             |
| 4/4        | 8               | 8:25         | 1470                   | 2409                                | 21          | 4/5          | 16              | 8:00          | 1415                   | 2616.5                              | 21          |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             | <u> </u>     |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             | <u> </u>     |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             |              |                 |               |                        |                                     |             |
|            |                 |              |                        |                                     |             | Te           | echnicia        | n <u>Jaso</u> | n Young                |                                     |             |

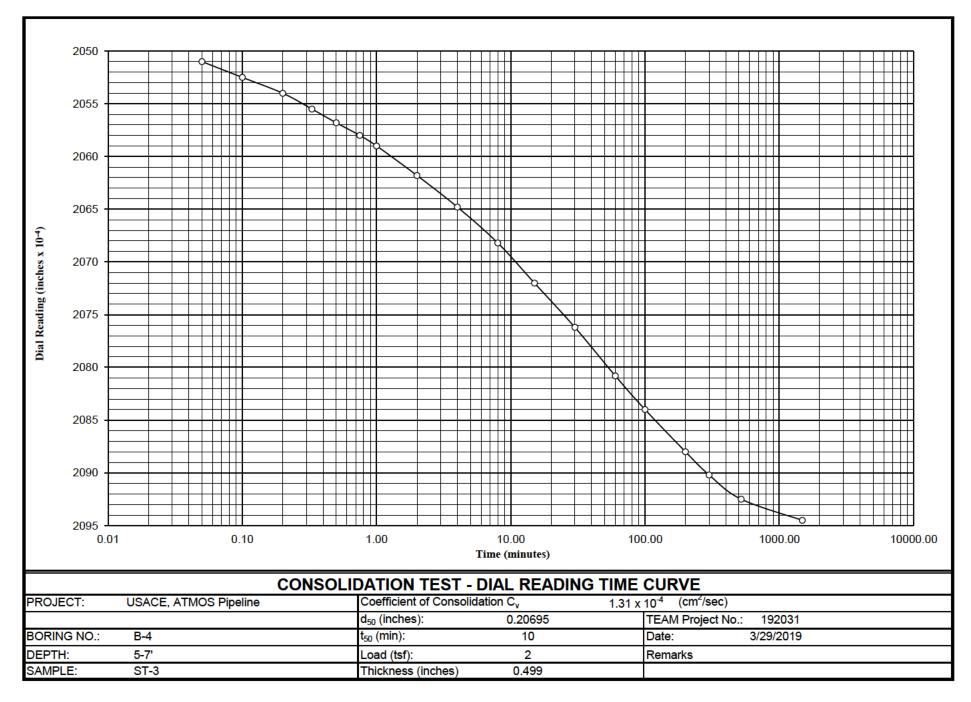
|       |        |      | TE          | AM C                   | ons      | sulta        | ants      | , In          | С.           |                        |       |
|-------|--------|------|-------------|------------------------|----------|--------------|-----------|---------------|--------------|------------------------|-------|
|       |        | G    | eotechnica  | l, Environn            | nental,  | Constru      | uction    | Materia       | ls Testing   |                        |       |
|       |        |      |             | CONSO                  |          |              |           |               |              |                        |       |
|       |        |      |             | (Time - C              | onsolida | ation Da     | ta)       |               |              |                        |       |
|       |        |      |             | (                      |          |              |           |               |              |                        |       |
| Proie | et.    | USA  | CE, ATMOS   | Pineline               |          |              |           | TFΔ           | M Job No.:   | 192031                 |       |
| -     |        |      |             |                        |          |              | anth:     |               |              | 2                      |       |
| BOH   | ig No  |      | D-4         | Sample No              |          | <u>-5</u> D6 | -pui      | 5-7           | CONSOI.110   | 2                      |       |
| Date  | Press. | Time | Elapsed     | Dial Reading           | Temp.    | Date         | Press.    | Time          | Elapsed      | Dial Reading           | Temp. |
| Dute  | (tsf)  | Time | Time, (min) | (10 <sup>-4</sup> in.) | °C       | Date         | (tsf)     | Time          | Time, (min)  | (10 <sup>-4</sup> in.) | °C    |
|       |        |      |             |                        |          |              |           | REBO          |              | DS                     |       |
|       |        |      |             |                        |          | 4/5          | 4         | 8:00          | Rebound      | 2616.5                 | 21    |
|       |        |      |             |                        |          | 4/6          | 4         | 11:10         | 1630         | 2480.8                 | 21    |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          | 4/6          | 1         | 11:10         | Rebound      | 2480.8                 | 21    |
|       |        |      |             |                        |          | 4/7          | 1         | 13:30         | 1580         | 2337.2                 | 21    |
|       |        |      |             |                        |          |              | -         |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          | 4/7          | 0.25      | 13:30         | Rebound      | 2337.2                 | 21    |
|       |        |      |             |                        |          | 4/8          | 0.25      | 13:30         | 1440         | 2229                   | 21    |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              | М         | achine D      | eflection Re | eadings                |       |
|       |        |      |             |                        |          |              | 0.25      |               |              | 2008                   |       |
|       |        |      |             |                        |          |              | 1         |               |              | 2031                   |       |
|       |        |      |             |                        |          |              | 2         |               |              | 2047                   |       |
|       |        |      |             |                        |          |              | 4         |               |              | 2065                   |       |
|       |        |      |             |                        |          |              | 8<br>16   |               |              | 2083                   |       |
|       |        |      |             |                        |          |              | 4         |               | ļ            | 2108<br>2074           |       |
|       |        |      |             |                        |          |              | 1         |               | L            | 2074                   |       |
|       |        |      |             |                        |          |              | 0.25      |               |              | 2020                   |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          |              |           |               |              |                        |       |
|       |        |      |             |                        |          | Τe           | echniciar | n <u>Jaso</u> | n Young      |                        |       |

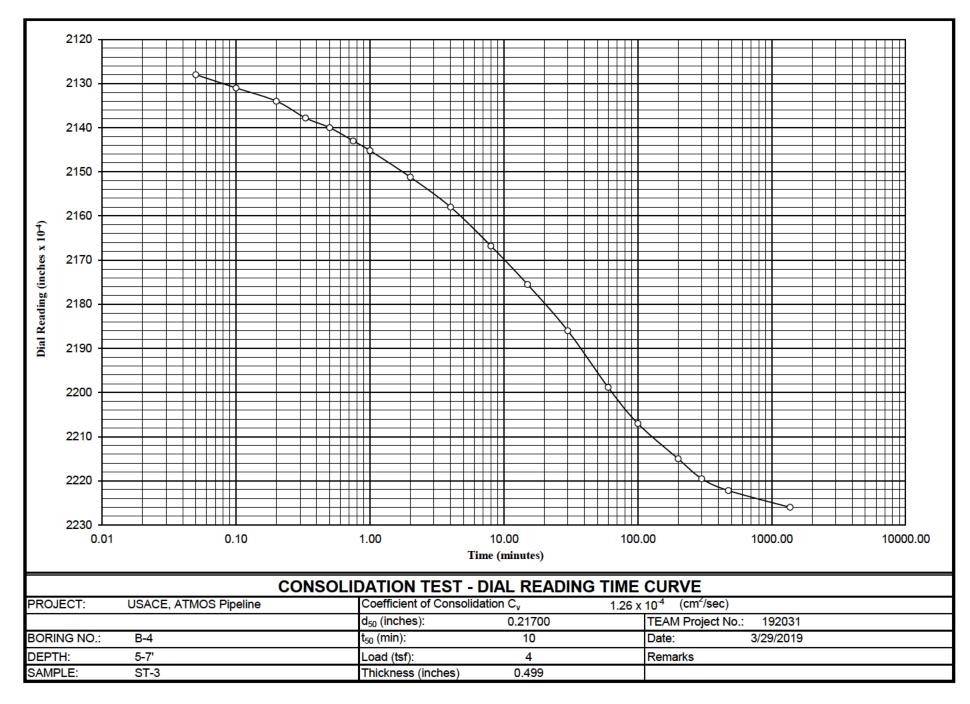
Geotechnical, Environmental, Construction Materials Testing

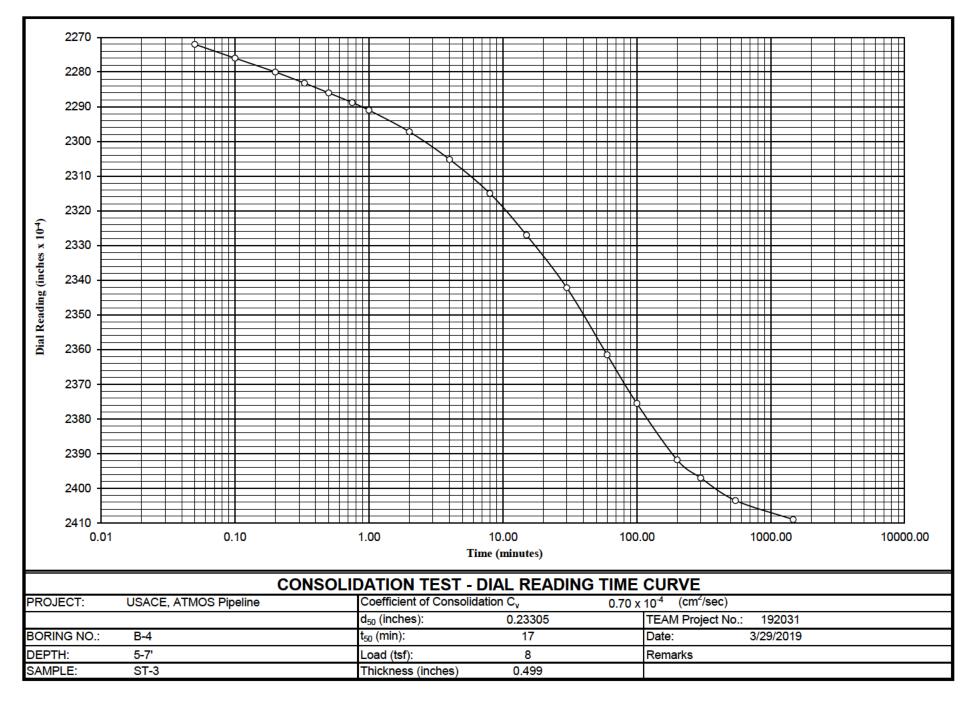
#### CONSOLIDATION TEST

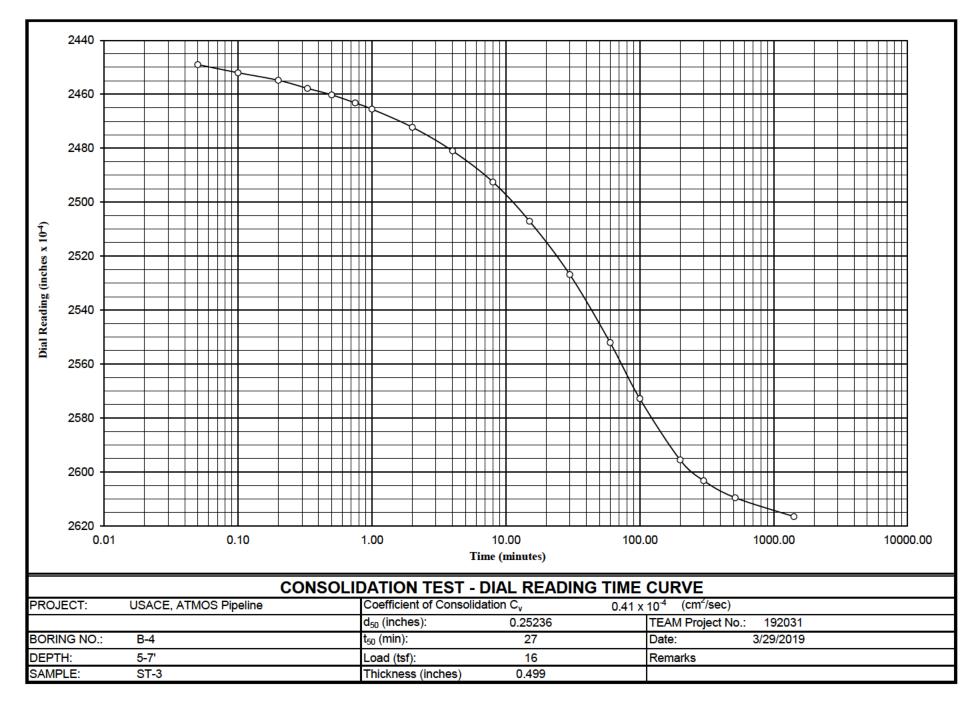
(Computation of Void Ratio)

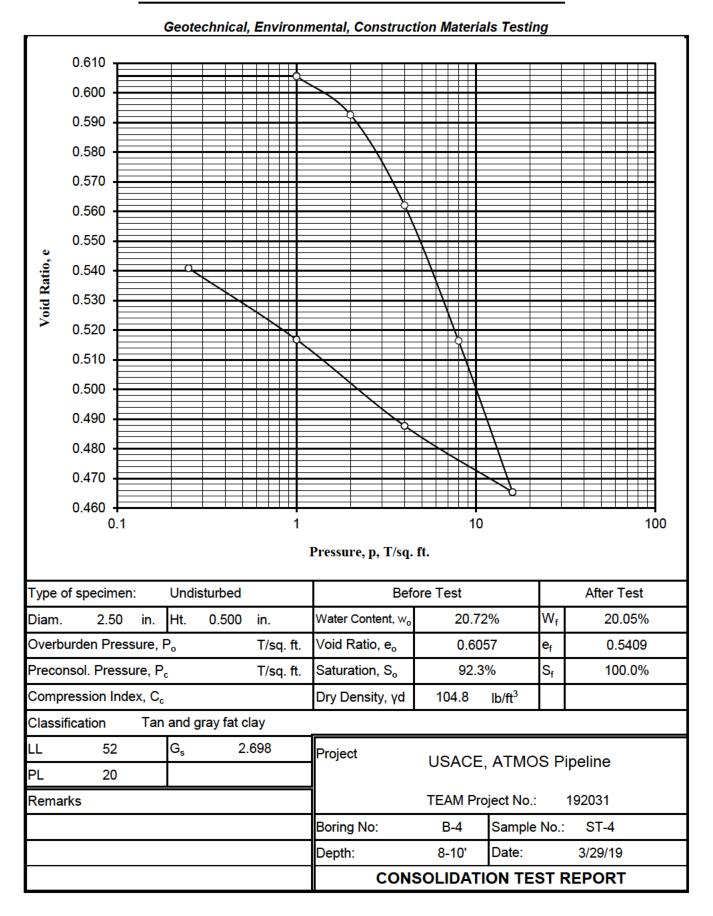
| PROJECT                              | USACE, AT  | TMOS Pipeline                          | TEA                               | M Job No.:                      | 192031 | DATE:  | 3/29/19       |
|--------------------------------------|--|--|-----------------------------------|---------------------------------|--------|--|---------------|
|                                      | B-4  | SAMF                                   | PLE NO. ST-3                      | DEPTH                           | 5-7'   | CONSOLIDOMETER NO  | . 2           |
| Pressure, P<br>T./sq.ft.             | Date<br>Increment<br>Applied                     | Time in Min.<br>Increment<br>Effective | Dial Reading 10 <sup>-4</sup> in. | Correction 10 <sup>-4</sup> in. | Heigh  | the second sec | Void Ratio, e |
| 0.1                                  | 3/29   | Zero Point                             | 2000                              | 2000                            |        | 2023   | 0.6820        |
| 1                                    | 3/29   | Initial Load                           | 2031                              | 2031                            | (      | 2023   | 0.6820        |
| 1                                    | 3/29   | 4030                                   | 2032                              | 2031                            | -      | 1 2022   | 0.6817        |
| 2                                    | 4/1  | 1485                                   | 2094.5                            | 2047                            | -47    | 7.5 1976   | 0.6660        |
| 4                                    | 4/2  | 1370                                   | 2226                              | 2065                            | -1     | 61 1862  | 0.6278        |
| 8                                    | 4/3  | 1470                                   | 2409                              | 2083                            | -3     | 26 1697  | 0.5722        |
| 16                                   | 4/4  | 1415                                   | 2616.5                            | 2108                            | -50    | 8.5 1515   | 0.5106        |
| 4                                    | 4/5  | 1630                                   | 2480.8                            | 2074                            | -40    | 6.8 1617   | 0.5449        |
| 1                                    | 4/6  | 1580                                   | 2337.2                            | 2045                            | -29    | 2.2 1731   | 0.5836        |
| 0.25                                 | 4/7  | 1440                                   | 2229                              | 2020                            | -2     | 09 1814  | 0.6116        |
|                                      |  |  |                                   |                                 |        |  |               |
| Note:<br>Height of vi<br>Void Ratio, | oids, $H_V = (H - H_S)$<br>e = $\underline{H_V}$ |  | H <sub>S</sub> = 0.2967           |                                 |        | oung Checked by Jam  |               |











|                 |   |          |                             |         | IDATION TE<br>cimen Data) | ST                               |                |            |
|-----------------|---|----------|-----------------------------|---------|---------------------------|----------------------------------|----------------|------------|
|                 |   | E, ATM-4 | OS Pipeline<br>Sample No.:  | ST-4    | Depth:                    | TEAM Job No.:<br>8-10' Date      | 192<br>: 3/29  |            |
|                 |   | and gray | fat clay                    |         |                           |                                  |                |            |
| Class           |   | anu yray | Tat Clay                    | Be      | fore Test                 |                                  | 1              | After Test |
|                 |   |          | Specir                      |         |                           | Trimmings                        |                | Specimen   |
|                 | Tare No.  |          | Ring and                    |         |                           | 623                              |                | 411        |
| ns              | Tare plus wet   | soil     | 191.                        | 58      |                           | 620.28                           |                | 116.55     |
| grar            | Tare plus dry   | soil     | 177.                        | 58      |                           | 551.10                           |                | 103.00     |
| Weight in grams | Water   | Ww       | W <sub>wo</sub> 14.0        | 0       |                           | 69.18                            | Wwf            | 13.55      |
| /eigł           | Tare  |          | 110.                        | 00      |                           | 217.16                           |                | 35.42      |
| -               | Dry soil  | Ws       | 67.5                        |         |                           | 333.94                           | <u> </u>       | 67.58      |
| W               | ater Content  | W        | W <sub>0</sub> 20.72        | 2%      |                           | 20.72%                           | W <sub>f</sub> | 20.05%     |
| C               | Consolidometer No.  | .:       | 3                           |         | Area                      | of specimen, A, (sq.             | cm.)           | 31.67      |
|                 | Weight of ring, g   |          | N//                         |         |                           | ht of specimen, H,               | (in.)          | 0.500      |
|                 | Weight of plates, g   |          | N/A                         | 4       | Spec                      | ific Gravity of solids,          | ( Gs)          | 2.698      |
| Net c           | height of water, H <sub>t</sub><br>change in height of<br>ht of specimen at e | specime  | en at end of test, <i>i</i> | ∆H =    | -0.02020                  | 2.54 = 0.168<br>in.<br>n.        | 34 in.         |            |
|                 | ratio before test, e <sub>r</sub><br>ratio after test, e <sub>f</sub>         |          |                             |         |                           | = 0.6057<br>= 0.5409             |                |            |
|                 | ee of saturation be   |          |                             |         |                           |                                  | 2.3%           |            |
|                 |   |          |                             |         |                           | 3114 = 100.0<br>2.4 = 104.<br>54 |                | ı.ft.      |
| Rema            | arks  |          |                             |         |                           |                                  |                |            |
| Tech            | nician Jaso   | on Youn  | g Comp                      | uted by | Jason                     | Young Che                        | cked by        | James Hutt |

|       |                 |       |                        | AM C                                   |             |               |                 | -       |                        |                                     |             |
|-------|-----------------|-------|------------------------|--|-------------|---------------|-----------------|---------|------------------------|-------------------------------------|-------------|
|       |                 | Ge    | eotechnica             | l, Environn                            |             |               |                 | Materia | ls Testing             |                                     |             |
|       |                 |       |                        | CONSO                                  |             | ON TES        | T               |         |                        |                                     |             |
|       |                 |       |                        | (Time - C                              | onsolida    | ation Da      | ita)            |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
| Proje | ect:            | USA   | CE, ATMOS              | Pipeline                               |             |               |                 | TEA     | M Job No.:             | 192031                              |             |
| Borin | ng No.:         |       | B-4                    | Sample No                              | .: <u>S</u> | <u>Г-4</u> De | epth: 8         | 8-10'   | Consol.No.:            | 3                                   |             |
| Date  | Press.<br>(tsf) | Time  | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date          | Press.<br>(tsf) | Time    | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br>°C |
| 3/29  | 0.25            | 13:50 | 0                      | 2008                                   | 20          | 4/2           | 4               | 9:10    | 0                      | 2083                                | 20          |
| 3/29  | 0.5             | 14:00 | 10                     | 2005                                   |             | 4/2           | 4               | 9:10    | 0.05                   | 2122                                | -           |
| 3/29  | 1               | 14:05 | 15                     | 2020                                   |             | 4/2           | 4               | 9:10    | 0.00                   | 2125                                |             |
| 4/1   | 1               | 8:25  | 3995                   | 2028.5                                 | 19          | 4/2           | 4               | 9:10    | 0.2                    | 2129                                |             |
|       |                 |       |                        |  |             | 4/2           | 4               | 9:10    | 0.33                   | 2133                                |             |
|       |                 |       |                        |  |             | 4/2           | 4               | 9:10    | 0.5                    | 2136.2                              |             |
|       |                 |       |                        |  |             | 4/2           | 4               | 9:10    | 0.75                   | 2139.5                              |             |
|       |                 |       |                        |  |             | 4/2           | 4               | 9:11    | 1                      | 2141.5                              |             |
| 4/1   | 2               | 8:25  | 0                      | 2028.5                                 | 19          | 4/2           | 4               | 9:12    | 2                      | 2146.8                              |             |
| 4/1   | 2               | 8:25  | 0.05                   | 2046.2                                 |             | 4/2           | 4               | 9:14    | 4                      | 2153                                |             |
| 4/1   | 2               | 8:25  | 0.1                    | 2048                                   |             | 4/2           | 4               | 9:18    | 8                      | 2159.5                              |             |
| 4/1   | 2               | 8:25  | 0.2                    | 2050                                   |             | 4/2           | 4               | 9:25    | 15                     | 2165.5                              |             |
| 4/1   | 2               | 8:25  | 0.33                   | 2051.8                                 |             | 4/2           | 4               | 9:40    | 30                     | 2173                                |             |
| 4/1   | 2               | 8:25  | 0.5                    | 2053                                   |             | 4/2           | 4               | 10:10   | 60                     | 2178.8                              |             |
| 4/1   | 2               | 8:25  | 0.75                   | 2054.5                                 |             | 4/2           | 4               | 10:50   | 100                    | 2182.2                              |             |
| 4/1   | 2               | 8:26  | 1                      | 2055.2                                 |             | 4/2           | 4               | 12:30   | 200                    | 2186.5                              |             |
| 4/1   | 2               | 8:27  | 2                      | 2058                                   |             | 4/2           | 4               | 14:10   | 300                    | 2188.8                              |             |
| 4/1   | 2               | 8:29  | 4                      | 2060.8                                 |             | 4/2           | 4               | 17:00   | 470                    | 2191.8                              |             |
| 4/1   | 2               | 8:33  | 8                      | 2063.8                                 |             | 4/3           | 4               | 8:00    | 1370                   | 2195                                | 20          |
| 4/1   | 2               | 8:40  | 15                     | 2066.2                                 |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 8:55  | 30                     | 2069.2                                 |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 9:25  | 60                     | 2072.2                                 |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 10:05 | 100                    | 2074.5                                 |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 11:45 | 200                    | 2077                                   |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 13:25 | 300                    | 2078.5                                 |             |               |                 |         |                        |                                     |             |
| 4/1   | 2               | 17:00 | 515                    | 2080.8                                 |             |               |                 |         |                        |                                     |             |
| 4/2   | 2               | 9:10  | 1485                   | 2083                                   | 20          |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             | 1             |                 |         |                        |                                     |             |
|       |                 |       |                        |  |             | Те            | echnicia        | n Jaso  | n Young                |                                     |             |
|       |                 |       |                        |  |             |               |                 |         |                        |                                     |             |

|            |                 |              |                        | AM C                                   |             |               |                 |               |                        |  |             |
|------------|-----------------|--------------|------------------------|--|-------------|---------------|-----------------|---------------|------------------------|--|-------------|
|            |                 | G            | eotechnica             | l, Environn                            |             |               |                 | Materia       | ls Testing             |  |             |
|            |                 |              |                        | CONSO                                  |             | ON TES        |                 |               |                        |  |             |
|            |                 |              |                        | (Time - C                              | onsolid     | ation Da      | ta)             |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
| Proje      | ect:            | USA          | CE, ATMOS              | Pipeline                               |             |               |                 | TEA           | M Job No.:             | 192031                                 |             |
| Borir      | ng No.:         |              | B-4                    | Sample No                              | .: S        | <u>Г-4</u> De | epth: 8         | 3-10'         | Consol.No.:            | 3                                      |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
| Date       | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date          | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 4/3        | 8               | 8:00         | 0                      | 2195                                   | 20          | 4/4           | 16              | 8:30          | 0                      | 2358.2                                 | 21          |
| 4/3        | 8               | 8:00         | 0.05                   | 2249                                   |             | 4/4           | 16              | 8:30          | 0.05                   | 2406                                   |             |
| 4/3        | 8               | 8:00         | 0.1                    | 2253                                   |             | 4/4           | 16              | 8:30          | 0.1                    | 2409                                   |             |
| 4/3        | 8               | 8:00         | 0.2                    | 2257.5                                 |             | 4/4           | 16              | 8:30          | 0.2                    | 2412.2                                 |             |
| 4/3<br>4/3 | 8<br>8          | 8:00<br>8:00 | 0.33                   | 2262.2<br>2265.5                       |             | 4/4<br>4/4    | 16<br>16        | 8:30<br>8:30  | 0.33<br>0.5            | 2416.5<br>2419.8                       |             |
| 4/3        | 8               | 8:00         | 0.5                    | 2265.5                                 |             | 4/4           | 16              | 8:30          | 0.5                    | 2419.8                                 |             |
| 4/3        | 8               | 8:01         | 1                      | 2209                                   |             | 4/4           | 16              | 8:31          | 1                      | 2425                                   |             |
| 4/3        | 8               | 8:02         | 2                      | 2278.5                                 |             | 4/4           | 16              | 8:32          | 2                      | 2433.8                                 |             |
| 4/3        | 8               | 8:04         | 4                      | 2287                                   |             | 4/4           | 16              | 8:34          | 4                      | 2444                                   |             |
| 4/3        | 8               | 8:08         | 8                      | 2297.2                                 |             | 4/4           | 16              | 8:38          | 8                      | 2457.5                                 |             |
| 4/3        | 8               | 8:15         | 15                     | 2308.2                                 |             | 4/4           | 16              | 8:45          | 15                     | 2472.5                                 |             |
| 4/3        | 8               | 8:30         | 30                     | 2320.8                                 |             | 4/4           | 16              | 9:00          | 30                     | 2491.8                                 |             |
| 4/3        | 8               | 9:00         | 60                     | 2332.5                                 |             | 4/4           | 16              | 9:30          | 60                     | 2510.2                                 |             |
| 4/3        | 8               | 9:40         | 100                    | 2339.2                                 |             | 4/4           | 16              | 10:10         | 100                    | 2520.2                                 |             |
| 4/3        | 8               | 11:20        | 200                    | 2345.5                                 |             | 4/4           | 16              | 11:50         | 200                    | 2529.2                                 |             |
| 4/3        | 8               | 13:00        | 300                    | 2349.2                                 |             | 4/4           | 16              | 13:30         | 300                    | 2533                                   |             |
| 4/3        | 8               | 17:00        | 540                    | 2353.5                                 |             | 4/4           | 16              | 17:00         | 510                    | 2537                                   |             |
| 4/4        | 8               | 8:30         | 1470                   | 2358.2                                 | 21          | 4/5           | 16              | 8:00          | 1410                   | 2543                                   | 21          |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             |               |                 |               |                        |  |             |
|            |                 |              |                        |  |             | Te            | echnicia        | n <u>Jaso</u> | n Young                |  |             |

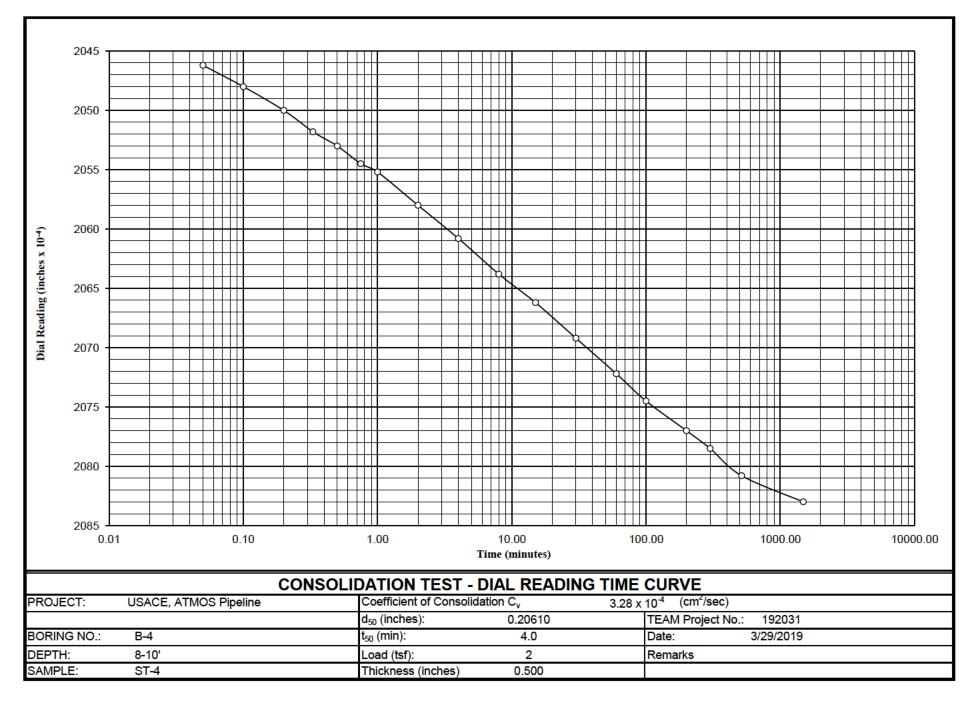
|       | TEAM Consultants, Inc. |      |                        |  |             |          |                 |               |                        |  |                         |  |
|-------|------------------------|------|------------------------|--|-------------|----------|-----------------|---------------|------------------------|--|-------------------------|--|
|       |                        | G    | eotechnica             | l, Environn                            | nental,     | Constr   | uction          | Materia       | ls Testing             |  |                         |  |
|       |                        |      |                        | CONSO                                  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        | (Time - C                              | onsolida    | ation Da | ta)             |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
| Proje | ect:                   | USA  | CE, ATMOS              | Pipeline                               |             |          |                 | TEA           | M Job No.:             | 192031                                 |                         |  |
| Borir | ng No.:                |      | B-4                    |  |             |          |                 |               |                        | 3                                      | •                       |  |
|       | -                      |      |                        |  |             |          |                 |               |                        |  |                         |  |
| Date  | Press.<br>(tsf)        | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date     | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C |  |
|       | REBOUND LOADS          |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             | 4/5      | 4               | 8:00          | Rebound                | 2543                                   | 21                      |  |
|       |                        |      |                        |  |             | 4/6      | 4               | 11:10         | 1630                   | 2438.5                                 | 21                      |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             | 4/6      | 1               | 11:10         | Rebound                | 2438.5                                 | 21                      |  |
|       |                        |      |                        |  |             | 4/7      | 1               | 13:30         | 1580                   | 2320                                   | 21                      |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             | 4/7      | 0.25            | 13:30         | Rebound                | 2320                                   | 21                      |  |
|       |                        |      |                        |  |             | 4/8      | 0.25            | 13:30         | 1440                   | 2224                                   | 21                      |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          | Μ               | achine D      | eflection Re           | eadings                                |                         |  |
|       |                        |      |                        |  |             |          | 0.25            |               |                        | 2008                                   |                         |  |
|       |                        |      |                        |  |             |          | 1               |               |                        | 2028                                   |                         |  |
|       |                        |      |                        |  |             |          | 2               |               |                        | 2042                                   |                         |  |
|       |                        |      |                        |  |             |          | 4               |               |                        | 2059                                   |                         |  |
|       |                        |      |                        |  |             |          | 8<br>16         |               |                        | 2080<br>2106                           |                         |  |
|       |                        |      |                        |  |             |          | 4               |               |                        | 2071                                   |                         |  |
|       |                        |      |                        |  |             |          | 1               |               |                        | 2043                                   |                         |  |
|       |                        |      |                        |  |             |          | 0.25            |               |                        | 2022                                   |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             |          |                 |               |                        |  |                         |  |
|       |                        |      |                        |  |             | Te       | echniciar       | n <u>Jaso</u> | n Young                |  | •                       |  |

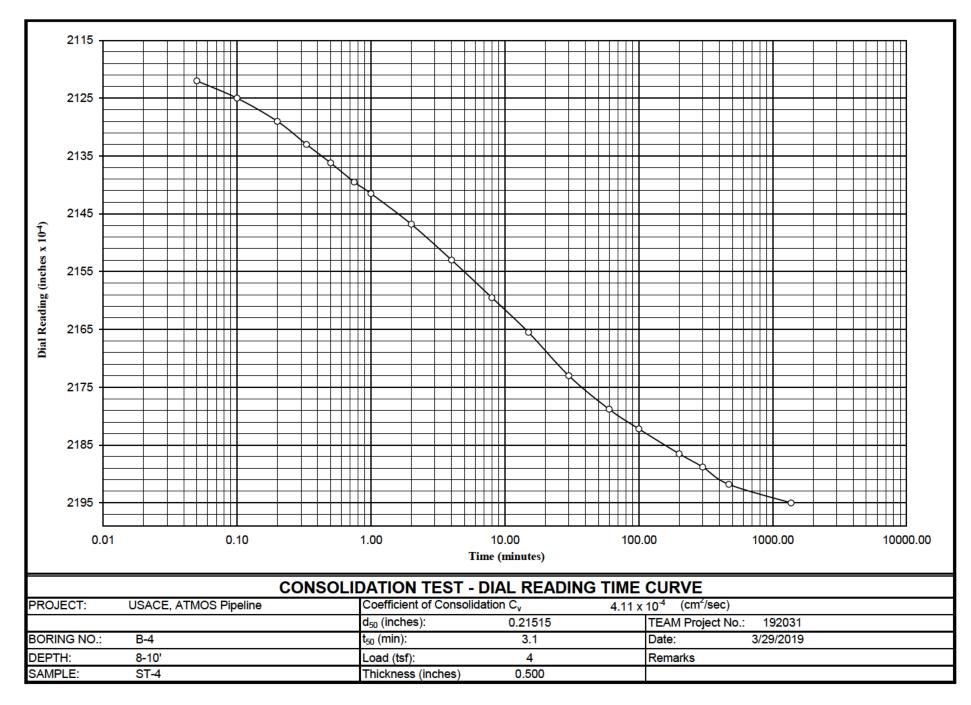
Geotechnical, Environmental, Construction Materials Testing

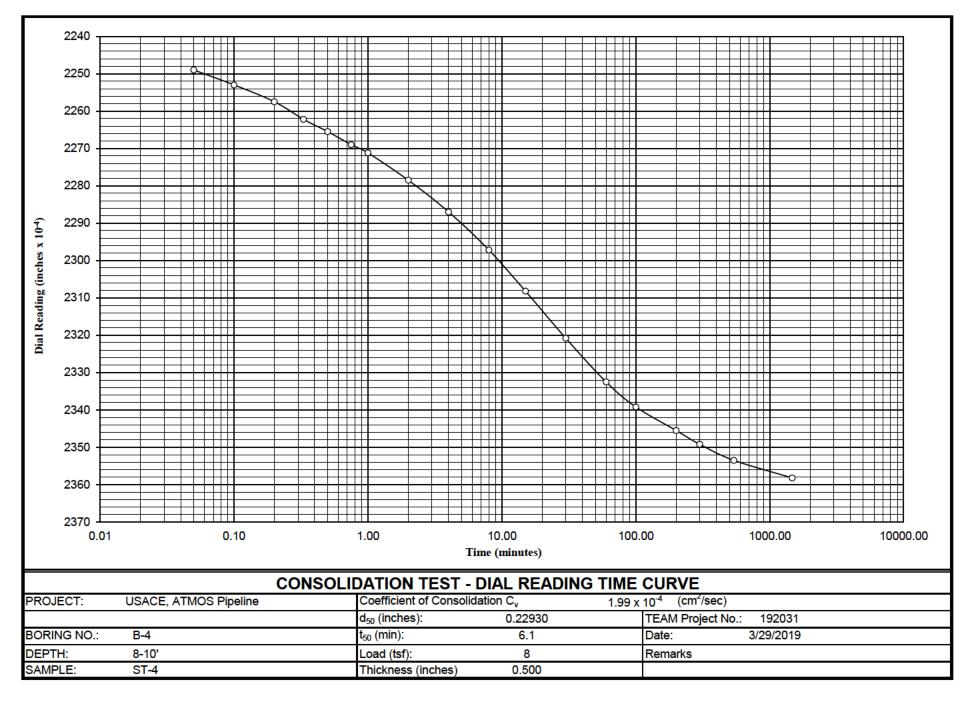
#### CONSOLIDATION TEST

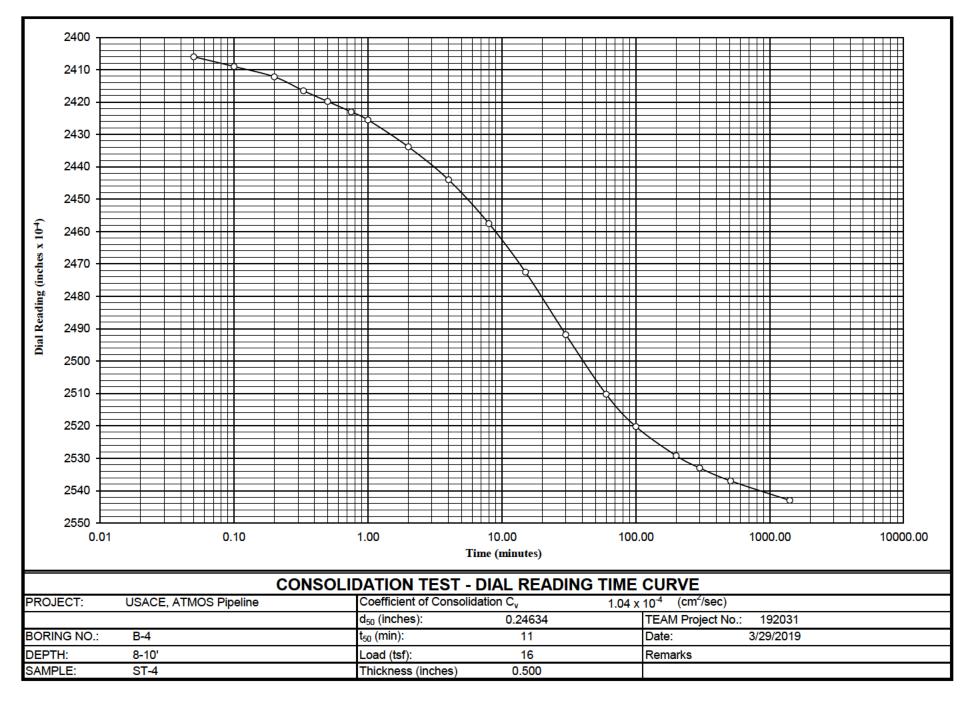
(Computation of Void Ratio)

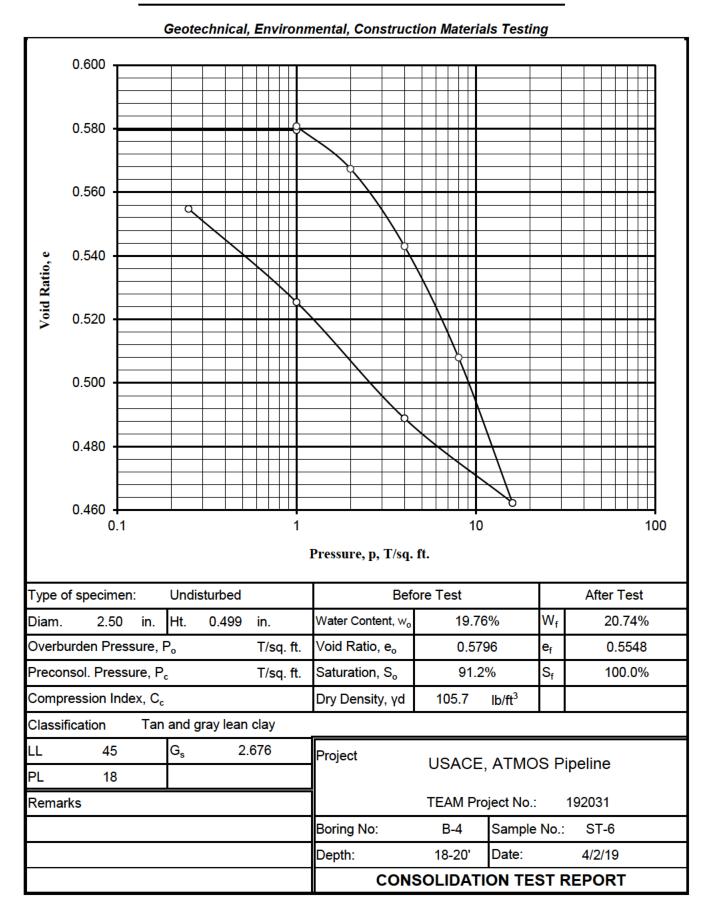
| PROJECT                                | USACE, AT   | MOS Pipeline                           | TEA                               | M Job No.:                      | 192031                              | DATE:                               | 3/29/19       |
|--|---|--|-----------------------------------|---------------------------------|-------------------------------------|-------------------------------------|---------------|
|  | B-4   | SAMP                                   | PLE NO. ST-4                      | DEPTH                           | 8-10'                               | CONSOLIDOMETER NO.                  | 3             |
| Pressure, P<br>T./sq.ft.               | Date<br>Increment<br>Applied  | Time in Min.<br>Increment<br>Effective | Dial Reading 10 <sup>-4</sup> in. | Correction 10 <sup>-4</sup> in. | Chang<br>Height<br>10 <sup>-4</sup> | t, $\Delta H$ Voids, H <sub>V</sub> | Void Ratio, e |
| 0.1                                    | 3/29  | Zero Point                             | 2000                              | 2000                            | 0                                   |                                     | 0.6057        |
| 1                                      | 3/29  | Initial Load                           | 2028                              | 2028                            | 0                                   | 1886                                | 0.6057        |
| 1                                      | 3/29  | 3995                                   | 2028.5                            | 2028                            | -0.                                 | 5 1886                              | 0.6056        |
| 2                                      | 4/1   | 1485                                   | 2083                              | 2042                            | -4                                  | 1 1845                              | 0.5926        |
| 4                                      | 4/2   | 1370                                   | 2195                              | 2059                            | -13                                 | 36 1750                             | 0.5621        |
| 8                                      | 4/3   | 1470                                   | 2358.2                            | 2080                            | -278                                | 3.2 1608                            | 0.5164        |
| 16                                     | 4/4   | 1410                                   | 2543                              | 2106                            | -43                                 | 37 1449                             | 0.4654        |
| 4                                      | 4/5   | 1630                                   | 2438.5                            | 2071                            | -367                                | 7.5 1519                            | 0.4877        |
| 1                                      | 4/6   | 1580                                   | 2320                              | 2043                            | -27                                 | 7 1609                              | 0.5168        |
| 0.25                                   | 4/7   | 1440                                   | 2224                              | 2022                            | -20                                 | 1684                                | 0.5409        |
|  |   |  |                                   |                                 |                                     |                                     |               |
| Note:<br>Height of vo<br>Void Ratio, o | pids, H <sub>V</sub> = (H - H <sub>S</sub> )<br>e = $\frac{H_V}{H_C}$ |  | H <sub>S</sub> = 0.3114           | Computed                        | hy Jason Vo                         | ung Checked by Jame                 | s Hutt        |











|                         |   |                              |   | DATION TEST<br>men Data)   |                 |            |
|-------------------------|---|------------------------------|---|--|-----------------|------------|
|                         | oject: USAC<br>pring No.: B   |                              | OS Pipeline<br>Sample No.: ST-6   | TEAM Job No.:<br>Depth: 18-20' Date:   | 192             |            |
|                         |   | and drav                     | / lean clay   |  |                 |            |
| 01035                   |   | and gray                     |   | ore Test   |                 | After Test |
|                         |   |                              | Specimen  | Trimmings  |                 | Specimen   |
|                         | Tare No.  |                              | Ring and Plates   | 625  |                 | 412        |
| su                      | Tare plus wet   | soil                         | 191.44  | 634.10   |                 | 117.52     |
| grar                    | Tare plus dry   | soil                         | 178.00  | 562.60   |                 | 103.42     |
| Weight in grams         | Water   | Ww                           | W <sub>WO</sub> 13.44   | 7 <b>1</b> .50   | W <sub>wf</sub> | 14.10      |
| /eigh                   | Tare  |                              | 110.00  | 200.80   |                 | 35.42      |
| 3                       | Dry soil  | Ws                           | 68.00   | 361.8  |                 | 68.00      |
| W                       | ater Content  | w                            | W <sub>O</sub> 19.76%   | 19.76%   | W <sub>f</sub>  | 20.74%     |
| C                       | Consolidometer No.  | .:                           | 1   | Area of specimen, A, (sq. o  | cm.)            | 31.67      |
|                         | Weight of ring, g   |                              | N/A   | Height of specimen, H, (   | (in.)           | 0.499      |
|                         | Weight of plates, g   |                              | N/A   | Specific Gravity of solids, (  | Gs)             | 2.676      |
| Final<br>Net c<br>Heigl | height of water, H <sub>t</sub><br>change in height of<br>ht of specimen at e | wf =<br>specime<br>nd of tes | st, $H_f = H - \Delta H = 0.49$   | 14.10<br>7 x 1 x 2.54<br>0.00782 in.<br>12 in.                                 |                 | in.        |
|                         |   |                              | $\frac{H - H_{s}}{H_{s}} = \frac{0.499 - 0.3159}{0.3159}$ $\frac{H_{s}}{H_{s}} = \frac{0.49118 - 0.3159}{0.3159}$ | = 0.5796   |                 |            |
|                         |   |                              | $H_{\rm WO} = \frac{H_{\rm WO}}{H - H_{\rm S}} = 0.$  |  |                 |            |
|                         |   |                              |   | $\frac{0.1753}{12 - 0.3159} = 100.09$ $\frac{x  62.4}{31.67  x  2.54} = 105.7$ |                 | .ft.       |
| Rema                    | arks  |                              |   |  |                 |            |
| Tech                    | nician Jaso   | on Youn                      | g Computed by   | Jason Young Chec   | ked by          | James Hutt |

|            |                 | <u> </u>     |                        |  |             |            |                 | -             |                        |  |             |
|------------|-----------------|--------------|------------------------|--|-------------|------------|-----------------|---------------|------------------------|--|-------------|
|            |                 | Ge           | eolecnnica             | <i>l, Environn</i><br>CONSO            | -           |            |                 | Materia       | is Testing             |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        | (Time - C                              | onsolida    | ation Da   | ita)            |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
| Proje      | ect:            | USA          | CE, ATMOS              | Pipeline                               |             |            |                 | TEA           | M Job No.:             | 192031                                 |             |
| Borir      | ng No.:         |              | B-4                    | Sample No                              | .: S1       | -6 De      | epth: 1         | 8-20'         | Consol.No.:            | 1                                      | _           |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
| Date       | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date       | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |
| 4/2        | 0.25            | 10:30        | 0                      | 2009                                   | 20          | 4/4        | 4               | 8:20          | 0                      | 2084.5                                 | 21          |
| 4/2        | 0.50            | 10:35        | 5                      | 2008                                   |             | 4/4        | 4               | 8:20          | 0.05                   | 2118                                   |             |
| 4/2        | 1.00            | 11:30        | 60                     | 2017                                   |             | 4/4        | 4               | 8:20          | 0.1                    | 2121.5                                 |             |
| 4/3        | 1.00            | 7:50         | 1280                   | 2028.2                                 | 20          | 4/4        | 4               | 8:20          | 0.2                    | 2124.8                                 |             |
|            |                 |              |                        |  |             | 4/4        | 4               | 8:20          | 0.33                   | 2128.5                                 |             |
|            |                 |              |                        |  |             | 4/4        | 4               | 8:20          | 0.5                    | 2130                                   |             |
|            |                 |              |                        |  |             | 4/4        | 4               | 8:20          | 0.75                   | 2132.2                                 |             |
|            |                 |              |                        |  |             | 4/4        | 4               | 8:21          | 1                      | 2134.8                                 |             |
| 4/3        | 2               | 7:50         | 0                      | 2028.2                                 | 20          | 4/4        | 4               | 8:22          | 2                      | 2138.8                                 |             |
| 4/3        | 2               | 7:50         | 0.05                   | 2047.2                                 |             | 4/4        | 4               | 8:24          | 4                      | 2143.5                                 |             |
| 4/3        | 2               | 7:50         | 0.1                    | 2049.2                                 |             | 4/4        | 4               | 8:28          | 8                      | 2149.8                                 |             |
| 4/3        | 2               | 7:50         | 0.2                    | 2051                                   |             | 4/4        | 4               | 8:35          | 15                     | 2153.2                                 |             |
| 4/3        | 2               | 7:50         | 0.33                   | 2053.2                                 |             | 4/4        | 4               | 8:50          | 30                     | 2159                                   |             |
| 4/3        | 2               | 7:50         | 0.5                    | 2054.8                                 |             | 4/4        | 4               | 9:20          | 60                     | 2163.2                                 |             |
| 4/3        | 2               | 7:50         | 0.75                   | 2056.5                                 |             | 4/4        | 4               | 10:00         | 100                    | 2165                                   |             |
| 4/3        | 2               | 7:51         | 1                      | 2057.8                                 |             | 4/4        | 4               | 11:40         | 200                    | 2168.5                                 |             |
| 4/3        | 2               | 7:52         | 2                      | 2060.8                                 |             | 4/4        | 4               | 13:20         | 300                    | 2170                                   |             |
| 4/3<br>4/3 | 2               | 7:54<br>7:58 | 4                      | 2063.8                                 |             | 4/4<br>4/5 | 4               | 17:00<br>8:00 | 520                    | 2176.5                                 | 21          |
| 4/3        | 2               | 8:05         | 8<br>15                | 2066.8                                 |             | 4/5        | 4               | 0.00          | 1420                   | 2178.5                                 | 21          |
| 4/3        | 2               | 8:20         | 30                     | 2069.2<br>2071.8                       |             |            |                 |               |                        |  |             |
| 4/3        | 2               | 8:50         | 60                     | 2071.8                                 |             |            |                 |               |                        |  |             |
| 4/3        | 2               | 9:30         | 100                    | 2074                                   |             |            |                 |               |                        |  |             |
| 4/3        | 2               | 11:10        | 200                    | 2073.3                                 |             |            |                 |               |                        |  |             |
| 4/3        | 2               | 12:50        | 300                    | 2077.8                                 |             |            |                 |               |                        |  |             |
| 4/3        | 2               | 17:00        | 550                    | 2078.8                                 |             |            |                 |               |                        |  |             |
| 4/4        | 2               | 8:20         | 1470                   | 2084.5                                 | 21          |            |                 |               |                        |  |             |
|            | -               | 0.20         | VITI                   | 2007.0                                 |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |
|            |                 |              |                        |  |             | Te         | echnicia        | n Jaso        | n Young                |  |             |
|            |                 |              |                        |  |             |            |                 |               |                        |  |             |

|            |                 | Ge           |                        | AM C                                   |             |               |                 |               |                        |                                     |                         |
|------------|-----------------|--------------|------------------------|--|-------------|---------------|-----------------|---------------|------------------------|-------------------------------------|-------------------------|
|            |                 |              |                        | CONSO                                  | _           |               |                 |               |                        |                                     |                         |
|            |                 |              |                        | (Time - C                              | onsolid     | ation Da      | ta)             |               |                        |                                     |                         |
|            |                 |              |                        | (11116-0                               | onsonua     |               | ita)            |               |                        |                                     |                         |
| Proje      | vot:            |              | CE, ATMOS              | Dipolino                               |             |               |                 |               | M Job No.:             | 102021                              |                         |
| -          |                 |              |                        |  |             |               | neth: 1         |               |                        |                                     |                         |
| DOUL       | ig ino          |              | D-4                    | Sample No                              | 3           | <u>1-0</u> D6 | epin. <u>1</u>  | 0-20          | Consol.No              | I                                   |                         |
| Date       | Press.<br>(tsf) | Time         | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date          | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading (10 <sup>-4</sup> in.) | Temp.<br><sup>o</sup> C |
| 4/5        | 8               | 8:00         | 0                      | 2178.5                                 | 21          | 4/8           | 16              | 8:00          | 0                      | 2310                                | 21                      |
| 4/5        | 8               | 8:00         | 0.05                   | 2220                                   |             | 4/8           | 16              | 8:00          | 0.05                   | 2355.5                              |                         |
| 4/5        | 8               | 8:00         | 0.1                    | 2224                                   |             | 4/8           | 16              | 8:00          | 0.1                    | 2358.5                              |                         |
| 4/5        | 8               | 8:00         | 0.2                    | 2228                                   |             | 4/8           | 16              | 8:00          | 0.2                    | 2362                                |                         |
| 4/5        | 8               | 8:00         | 0.33                   | 2231.8                                 |             | 4/8           | 16              | 8:00          | 0.33                   | 2366.2                              |                         |
| 4/5<br>4/5 | 8<br>8          | 8:00<br>8:00 | 0.5                    | 2234.8                                 |             | 4/8<br>4/8    | 16<br>16        | 8:00<br>8:00  | 0.5                    | 2370.5                              |                         |
| 4/5        | 8               | 8:00         | 0.75<br>1              | 2237.8<br>2240                         |             | 4/8           | 16              | 8:00          | 0.75<br>1              | 2374.5<br>2380                      |                         |
| 4/5        | 8               | 8:02         | 2                      | 2240                                   |             | 4/8           | 16              | 8:02          | 2                      | 2389.8                              |                         |
| 4/5        | 8               | 8:04         | 4                      | 2240.0                                 |             | 4/8           | 16              | 8:04          | 4                      | 2400.5                              |                         |
| 4/5        | 8               | 8:08         | 8                      | 2262.8                                 |             | 4/8           | 16              | 8:08          | 8                      | 2413.8                              |                         |
| 4/5        | 8               | 8:15         | 15                     | 2270.2                                 |             | 4/8           | 16              | 8:15          | 15                     | 2427                                |                         |
| 4/5        | 8               | 8:30         | 30                     | 2278.2                                 |             | 4/8           | 16              | 8:30          | 30                     | 2441.2                              |                         |
| 4/5        | 8               | 9:00         | 60                     | 2284.2                                 |             | 4/8           | 16              | 9:00          | 60                     | 2451.8                              |                         |
| 4/5        | 8               | 9:40         | 100                    | 2288.2                                 |             | 4/8           | 16              | 9:40          | 100                    | 2458                                |                         |
| 4/5        | 8               | 11:20        | 200                    | 2292.8                                 |             | 4/8           | 16              | 11:20         | 200                    | 2464.5                              |                         |
| 4/5        | 8               | 13:00        | 300                    | 2295                                   |             | 4/8           | 16              | 13:00         | 300                    | 2468                                |                         |
| 4/5        | 8               | 17:15        |                        | 2298.5                                 |             | 4/8           | 16              | 18:00         | 600                    | 2473.2                              |                         |
| 4/8        | 8               | 8:00         | 4320                   | 2310                                   | 21          | 4/9           | 16              | 8:00          | 1440                   | 2479.5                              | 21                      |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     | L                       |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             |               |                 |               |                        |                                     |                         |
|            |                 |              |                        |  |             | Τe            | echnicia        | n Jaso        | n Young                |                                     |                         |
|            |                 |              |                        |  |             | Τe            | echnicia        | n <u>Jaso</u> | n Young                |                                     |                         |

|       | TEAM Consultants, Inc.   |      |                        |  |             |          |                 |               |                        |  |             |  |
|-------|--|------|------------------------|--|-------------|----------|-----------------|---------------|------------------------|--|-------------|--|
|       |  | G    | eotechnica             | l, Environn                            | nental,     | Constru  | uction ]        | Materia       | ls Testing             |  |             |  |
|       |  |      |                        | CONSO                                  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        | (Time - C                              | onsolida    | ation Da | ta)             |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
| Proje | ect:   | USA  | CE, ATMOS              | Pipeline                               |             |          |                 | TEA           | M Job No.:             | 192031                                 |             |  |
| Borin | Boring No.: <u>B-4</u> Sample No.: <u>ST-6</u> Depth: <u>18-20'</u> Consol.No.: <u>1</u> |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  | 1    |                        |  | Tama        |          |                 |               |                        |  | Tama        |  |
| Date  | Press.<br>(tsf)  | Time | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C | Date     | Press.<br>(tsf) | Time          | Elapsed<br>Time, (min) | Dial Reading<br>(10 <sup>-4</sup> in.) | Temp.<br>°C |  |
|       |  |      |                        |  |             |          |                 | REB           |                        | )S                                     |             |  |
|       |  |      |                        |  |             | 4/9      | 4               | 8:00          | Rebound                | 2479.5                                 | 21          |  |
|       |  |      |                        |  |             | 4/9      | 4               | 8:00          | 1440                   | 2359.5                                 | 21          |  |
|       |  |      |                        |  |             |          |                 | 5.50          |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             | 4/10     | 1               | 8:00          | Rebound                | 2359.5                                 | 21          |  |
|       |  |      |                        |  |             | 4/11     | 1               | 8:00          | 1440                   | 2217                                   | 21          |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             | 4/11     | 0.25            | 8:00          | Rebound                | 2217                                   | 21          |  |
|       |  |      |                        |  |             | 4/12     | 0.25            | 7:30          | 1410                   | 2104.2                                 | 21          |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          | M               | achine [      | Deflection Re          | adings                                 |             |  |
|       |  |      |                        |  |             |          | 0.25            |               |                        | 2009                                   |             |  |
|       |  |      |                        |  |             |          | 1               |               |                        | 2032                                   |             |  |
|       |  |      |                        |  |             |          | 2               |               |                        | 2046                                   |             |  |
|       |  |      |                        |  |             |          | 4               |               |                        | 2063                                   |             |  |
|       |  |      |                        |  |             |          | 8<br>16         |               |                        | 2084<br>2109                           |             |  |
|       |  |      |                        |  |             |          | 4               |               |                        | 2109                                   |             |  |
|       |  |      |                        |  |             |          | 1               |               |                        | 2046                                   |             |  |
|       |  |      |                        |  |             |          | 0.25            |               |                        | 2026                                   |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             |          |                 |               |                        |  |             |  |
|       |  |      |                        |  |             | Τe       | echniciar       | n <u>Jaso</u> | n Young                |  |             |  |

Geotechnical, Environmental, Construction Materials Testing

#### CONSOLIDATION TEST

(Computation of Void Ratio)

| PROJECT                                | USACE, AT                            | MOS Pipeline                           | TEA                                  | M Job No.:                         | 192031                                   | DATE:                    | 4/2/19        |
|--|--------------------------------------|--|--------------------------------------|------------------------------------|--|--------------------------|---------------|
|  | B-4                                  | SAMP                                   | LE NO. ST-6                          | DEPTH                              | 18-20'                                   | CONSOLIDOMETER NO.       | 1             |
| Pressure, P<br>T./sq.ft.               | Date<br>Increment<br>Applied         | Time in Min.<br>Increment<br>Effective | Dial Reading<br>10 <sup>-4</sup> in. | Correction<br>10 <sup>-4</sup> in. | Change<br>Height,<br>10 <sup>-4</sup> ir | ∆H Voids, H <sub>V</sub> | Void Ratio, e |
| 0.1                                    | 4/2                                  | Zero Point                             | 2000                                 | 2000                               | 0  | <mark>1</mark> 831       | 0.5796        |
| 1                                      | 4/2                                  | Initial Load                           | 2032                                 | 2032                               | 0  | 1831                     | 0.5796        |
| 1                                      | 4/2                                  | 1280                                   | 2028.2                               | 2032                               | 3.8                                      | 1835                     | 0.5808        |
| 2                                      | 4/3                                  | 1470                                   | 2084.5                               | 2046                               | -38.5                                    | 5 1792                   | 0.5674        |
| 4                                      | 4/4                                  | 1420                                   | 2178.5                               | 2063                               | -115.                                    | 5 <b>1</b> 715           | 0.5430        |
| 8                                      | 4/5                                  | 4320                                   | 2310                                 | 2084                               | -226                                     | 6 1605                   | 0.5080        |
| 16                                     | 4/8                                  | 1440                                   | 2479.5                               | 2109                               | -370.                                    | 5 1460                   | 0.4623        |
| 4                                      | 4/9                                  | 1440                                   | 2359.5                               | 2073                               | -286.                                    | 5 1544                   | 0.4889        |
| 1                                      | 4/10                                 | 1440                                   | 2217                                 | 2046                               | -171                                     | 1660                     | 0.5254        |
| 0.25                                   | 4/11                                 | 1410                                   | 2104.2                               | 2026                               | -78.2                                    | 2 1753                   | 0.5548        |
|  |                                      |  |                                      |                                    |  |                          |               |
| Note:<br>Height of vo<br>Void Ratio, o | bids, $H_V = (H - H_S)$<br>$e = H_V$ | - ΔH                                   | H <sub>S</sub> = 0.3159              |                                    |  |                          |               |
|  | H <sub>s</sub>                       | Tech                                   | nician Jason Young                   | Computed                           | by Jason You                             | ng Checked by Jame       | s Hutt        |

