Aerospace Operation
Cherry Division of Textron Inc.



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Lap Joint Fatigue Comparison of Cherry SST™, CherryMAX®, Solid Rivet and Huck Clinch® Blind Rivets

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<u>SUMMARY</u>

The Research and Development department of the Cherry division of Textron Inc., has conducted a series of lap joint fatigue tests per MIL-STD-1312/21. This program was undertaken to study the comparative joint fatigue strength of the Cherry SST™ and CherryMAX® blind rivet designs. It was later expanded to include the Huck Clinch® and MS20470DD solid rivets.

The fasteners tested were 3/16 diameter protruding head oversize bulbed rivets having a 3/16" grip and 3/16 diameter solid rivets having a - 6 length. The test specimen used was the standard MIL-STD-1312/21 (four fastener) lap joint coupon. Coupon material was 2024-T3 clad aluminum alloy sheet having a nominal thickness of .090".

Each type of fastener was tested at three different load levels roughly corresponding to 80%, 60% and 40% of ultimate static joint strength. The load ratio (R = min / max) was 0.1. The frequency was 30 cycles per second (30 Hz).

The test results are summarized graphically in figure 1. The method of least squares was used to derive equations of the form f(x) = AX for the "Best Fit" curves. A review of figure 1 shows the following:

- The new Cherry SST™ blind rivet provides four (4) times the life of the Huck Clinch® at the higher load levels and twice the life at lower load levels.
- Only the Cherry SST™ exhibits fatigue strength in excess of MS20470DD solid rivets under these test conditions.
- The CherryMAX® rivet provides fatigue life in excess of the Huck Clinch®.

INTRODUCTION

The Cherry SSTTM is designed to fit the installation envelope of existing bulb rivet systems and is installed with the standard MIL-R-85188 hand riveter (Cherry part number G704). The sleeve material is 5056 aluminum alloy which is mated with a non-magnetic, cadmium free A-286 stem. An A-286 expander, having a shape optimized for sheet take up, is wrapped on the stem. It is believed that the exceptional residual preload of the design is responsible for its superior lap joint fatigue properties. The Cherry SSTTM incorporates the same proven "Safe - lock" locking collar and driving anvil concept as the original CherryMax® fastening system.

The results of this fatigue study clearly show not only that CherryMAX® rivet exceeds the fatigue strength of Huck Clinch®, but also that the new Cherry SST™ rivet provides up to four times the life of the Huck product and up to twice the fatigue life of solid rivets.

TEST PLAN

Fasteners Tested:

Protruding head oversize bulbed blind rivets: CR3243 - 06 - 03 (CherryMAX®)

CR6253 - 06 - 03 (CherrySSTTM)

HC3243 - 06 - 03 (Huck Clinch®)

Solid Rivets

MS20470DD6 -06 (Aerospace rivet)

Test Coupon

MIL-STD-1312/21 coupon as shown in figure 2 below.

Material: 2024-T3 Clad sheet per QQ-A-250/5

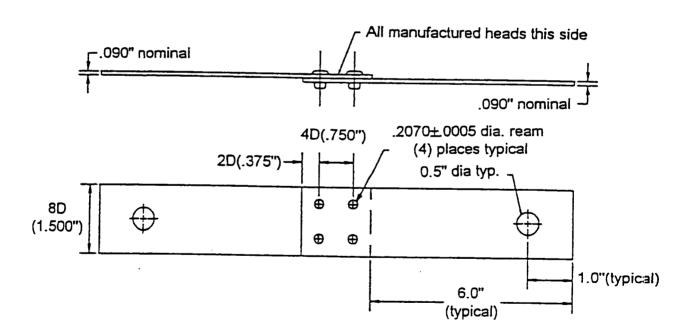


Figure 2. Shear Joint Fatigue Coupon

TEST PLAN (continued)

Test Equipment

The fatigue testing was conducted on an MTS model 810 fatigue machine using an Instron model 8500 amplitude controler.

Static testing was performed on a Satec model 20UD universal testing machine (UTM).

A Cherry model G704 riveter with model H701B456 nose assembly was used for installation of the blind rivets. The solid rivets were squeezed on the Satec UTM.

TEST PROCEDURE

To establish the static ultimate strength, one of the Cherry SST coupons was loaded to failure in accordance with MIL-STD-1312, test method 4 on the Satec UTM. Failure load was 4690 lbs from which the maximum fatigue loads corresponding to 80%, 60% and 40% were derived.

The fatigue tests were conducted in accordance with MIL-STD-1312, test method 21. Figure 3 below shows a typical coupon under test.

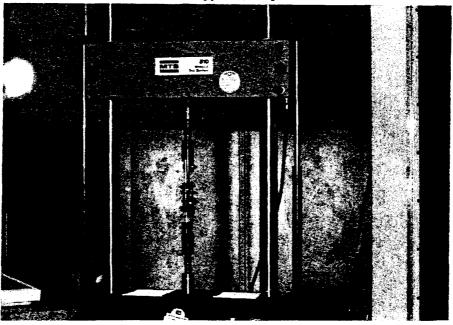


Figure 3

TEST PROCEDURE (continued)

All tests were conducted under ambient conditions at a frequency of 30 Hz.

The solid rivet installations were carried out as follows:

- The rivets were solution treated at 920°F and water quenched per MIL-H-6088G to provide rivets in the 2024-W condition. Rivets were then chilled to -109°F by packing in dry ice where they remained until used.
- The rivets were squeezed to an upset height of 0.4D with the resulting tail diameter of approximately 1.5D on the Satec UTM. These installations took place on the same day as the solution treatment and with fifteen (15) minutes of removal from the dry ice box.
- 3. The installed rivets were allowed to age at room temperature for a minimum of 96 hours before testing commenced (except for specimen #36 which was aged for 88 hours prior to test). Rivets were thus in the T3 condition at the time of test.

Dynamic testing was performed at loads roughly corresponding to 80%, 60% and 40% of the maximum static load. A load ratio 0.1 was used for all tests. Three (3) coupons of each fastener type were tested at each load level in order to examine the scatter of results (which turned out to be minimal).

RESULTS

The actual results are tabulated in tables 1 through 4 for Cherry SST™, CherryMAX®, Huck Clinch® and the solid rivets respectively. S-N curves for the results are shown in figures 4 through 7 for the four fastener types. The averages of all four fasteners are shown in figure 1.

An examination of figure 1 leads one to the following conclusions:

- CherryMAX® exceeds the fatigue strength of Huck Clinch® at all load levels.
- The CherrySST exhibits fatigue life up to 4 times that of the Huck Clinch® at high load levels and twice the life at lower load levels.

RESULTS (continued)

• The CherrySST™ exhibits fatigue strength equal to or greater than 'DD' solid rivets under these test conditions.

Examination Of Failure Modes

Figure 8 through 11 show the typical coupon failures experienced during this study. The following observations are apparent.

- CherrySST™ ___ All coupons showed faying surface fretting adjacent to the fastener holes. This is indicative of high residual tension (preload) in the installed fastener. See figure 8.
- Huck Clinch® ___ Faying surface fretting occurred away from the fastener holes, notably midway between the holes as shown in figure 10.
 This is indicative of low residual tension.
- Except for one instance, the origins of fracture started from points along the coupon faying surface.

CONCLUSIONS

The industry standard CherryMAX® rivet provides lap joint fatigue properties in excess of the Huck Clinch® rivet.

The Cherry SST™ product exhibits exceptional fatigue characteristics compared to other bulbed rivets and solid rivets. Further comparisons to solid rivet are planned in the near future.

Table 1 Cherry SST Blind Rivet Lapshear Fatigue Test Results

ATIGU	JE TEST TYPE:	LAP JOINT	SHEAR FAT	IGUE, FULL	LOAD TRA	ANSFER				FASTENER TYPE				
OAD F	RATIO:	R = 0.1												
EST S	STATION:	MTS				CI	HERRY TEXTRO	N		PART # : CR6253-6-3				
EST S	SPEED:	30 Cycles /	Sec			122	4 E. WARNER A	I <i>VE</i> .						
PECIF	ICATION:	Mil-Std-132	1/21			SAN	TA ANA, CA 92	2707						
HEET	MATERIAL:	2024-T3 CI	ad											
rest	% OF STATIC	THICK	NESS	TEST LC	AD (lbs.)	FATIGUE LIFE	DATE &	FAILURE LO	CATION 1	TYPE OF				
NO.	ULT. TENSILE	T1	T2	MAX.	MIN.	(CYCLES)	OPERATOR	PLATE	HOLE NO.	FAILURE				
4		0.0901	0.0901			94,736	11/10/93 G.F	BP	1,2	MO, Predominantly @ 2				
5	80%	0.0902	0.0904	3750	375	93,565	11/11/93 G.F	ВР	1,2	MO, Predominantly @ 1				
6		0.0903	0.0901			94,029	11/11/93 G.F	ВР	1,2	MO, Predominantly @ 2				
10		0.0903	0.0898			240,327	11/11/93 G.F	TP	3,4	Multiple Origin				
11	60%	0.0900	0.0900	2800	280	257,804	11/12/93 G.F	TP	3,4	MO, Predominantly @ 4				
12		0.0900	0.0902			390,971	11/15/93 D.P	TP	3	Multiple Origin				
28	0.0900		0.0900			689,454	11/15/93 D.P	BP	1	Multiple Origin				
29 40%		0.0903	0.0902	1870	187	698,513	11/16/93 G.F	BP	1	Multiple Origin				
30		0.0900	0.0903			760,542	11/17/93 G.F	ВР		Multiple Origin				

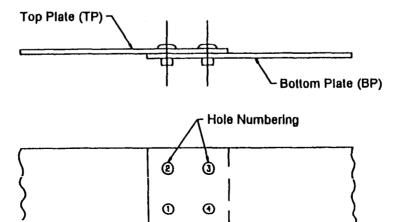
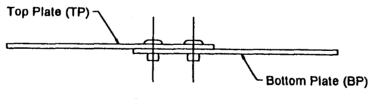


Table 2 CherryMAX Blind Rivet Lapshear Fatigue Test Results

rigu	E TEST TYPE:	LAP JOINT	SHEAR FAT	IGUE, FULI	L LOAD TR.	ANSFER				FASTENER TYPE
ND P	ATIO:	R = 0.1			· · · · · · · · · · · · · · · · · · ·					
TS	TATION:	MTS			PART # : CR3243-6-3					
TS	PEED:	30 Cycles /	Sec			122	4 E. WARNER A	I <i>VE</i> .		
CIF	CATION:	Mil-Std-132	21/21			SAN	TA ANA, CA 92	?707		
ΞT	MATERIAL:	2024-T3 C	lad							
T	% OF STATIC	THIC	(NESS	TEST LC	OAD (lbs.)	FATIGUE LIFE	DATE &	FAILURE LO	CATION 1	TYPE OF
	ULT. TENSILE	T1	T2	MAX.	MIN.	(CYCLES)	OPERATOR	PLATE	HOLE NO.	FAILURE
		0.0902	0.0902			26,562	11/12/93 G.F	TP	3,4	MO, Predominantly @ 3
	80%	0.0900	0.0902	3750	375	25,303	11/12/93 G.F	TP	3,4	Multiple Origin
_[0.0903	0.0898			28,556	11/12/93 G.F	ВР	1,2	Fatigue Failure @ 2
╝		0.0902	0.0904			102,050	11/12/93 G.F	TP	3,4	Fatigue Failure @ 3
┛	60%	0.0898	0.0902	2800	280	120,833	11/15/93 G.F	BP	1,2	Fatigue Failure @ 1
╝		0.0903	0.0902			190,637	11/16/93 G.F	ВР	1,2	Fatigue Failure @ 2
_]		0.0902	0.0901			461,891	11/18/93 G.F	TP	3,4	MO, Predominantly @ 4
┛	40%	0.0903	0.0903	1870	187	248,249	11/19/93 G.F	BP	1,2	Fatigue Failure @ 2
		0.0904	0.0901			725,193	11/19/93 G.F	BP	1,2	MO, Predominantly @ 1



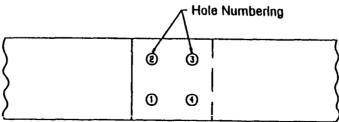
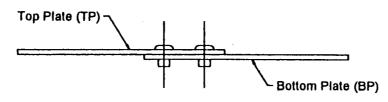


Table 3 Huck Clinch Blind Rivet Lapshear Fatigue Test Results

ATIG	UE TEST TYPE:	LAP JOINT	SHEAR FAT	IGUE, FUL	L LOAD TR	ANSFER				FASTENER TYPE
OAD I	RATIO:	R = 0.1								
EST S	STATION:	MTS			PART # : HC3243-6-3					
TEST S	SPEED:	30 Cycles /	'Sec			122	4 E. WARNER A	IVE.		
PECIF	ICATION:	Mil-Std-132	21/21			SAN	TA ANA, CA 92	2707		TYPE OF FAILURE Multiple Origin Multiple Origin
HEET	MATERIAL:	2024-T3 C	lad							
TEST	% OF STATIC	THICK	KNESS	TEST LO	DAD (lbs.)	FATIGUE LIFE	DATE &	FAILURE LO	CATION 1	TYPE OF
NO.	ULT. TENSILE	T1	T2	MAX. MIN.		(CYCLES)	OPERATOR	PLATE	HOLE NO.	FAILURE
7		0.0901	0.0901			24,651	11/10/93 G.F	BP	1,2	Multiple Origin
8	80%	0.0903	0.0899	3750	0 375	24,397	11/11/93 G.F	ВР	1,2	Multiple Origin
9		0.0900	0.0900			31,400	11/11/93 G.F	BP	1,2	Fatigue Failure @ 1
16		0.0902	0.0902			69,103	11/12/93 G.F	BP	1,2	Multiple Origin
17	60%	0.0900	0.0901	2800	280	47,594	11/12/93 G.F	ВР	1,2	Multiple Origin
18		0.0901	0.0901			123,840	11/15/93 G.F	BP	1,2	Fatigue Failure @ 1
30		0.0903	0.0900			368,176	11/18/93 G.F	BP	1,2	Fatigue Failure @ 1
31	40%	0.0897 0.0897		1870	187	316,832	11/18/93 G.F	BP	1,2	Multiple Origin
32		0.0901	0.0903			647,949	11/18/93 G.F	BP	1,2	Multiple Origin



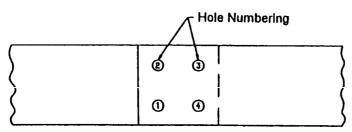
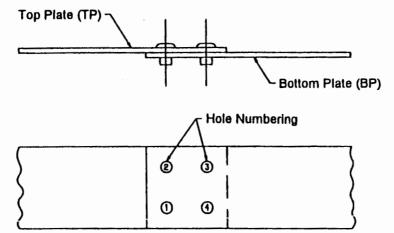


Table 4 MS20470DD Solid Rivet Lapshear Fatigue Test Results

TIGL	JE TEST TYPE:	LAP JOINT	SHEAR FAT	IGUE, FULI	LOAD TR	ANSFER				FASTENER TYPE				
)AD F	RATIO:	R = 0.1												
ST S	TATION:	MTS					PART#: MS20470dd6-6							
ST S	PEED:	30 Cycles /	Sec			1224	4 E. WARNER A	VE.		1				
ECIF	ICATION:	Mil-Std-132	1/21			SAN	TA ANA, CA 92	2707						
IEET	MATERIAL:	2024-T3 CI	ad											
EST	% OF STATIC	THICK	NESS	TEST LO	AD (lbs.)	FATIGUE LIFE	DATE &	FAILURE LO	CATION 1	TYPE OF				
10.	ULT. TENSILE	ULT. TENSILE T1 T2		MAX.	MIN.	(CYCLES)	OPERATOR	PLATE	HOLE NO.	FAILURE				
36		0.0901	0.0902			52,699	11/22/93 G.F	TP	3,4	Multiple Origin				
37	80%	0.0898	0.0895	3750	375	29,247	11/23/93 G.F	TP	3,4	Multiple Origin				
38		0.0897	0.0902			63,927	11/23/93 G.F	TP	3,4	Multiple Origin				
39		0.0897	0.0895			139,397	11/23/93 G.F	TP	3,4	Multiple Origin				
10	60%	0.0895	0.0895	2800	280	229,546	11/23/93 G.F	BP		Failed In Midway Of Plate				
11		0.0895	0.0900			144,898	11/23/93 G.F	TP	3,4	Multiple Origin				
12		0.0900	0.0895			453,542	11/24/93 G.F	TP	3,4	MO, Predominantly @ 4				
13	40%	0.0905	0.0899	1870	187	581,283	11/24/93 G.F	BP	11	Multiple Origin				
16		0.0898	0.0898			809,187	11/29/93 G.F	TP	3	MO, Predominantly @ 3				



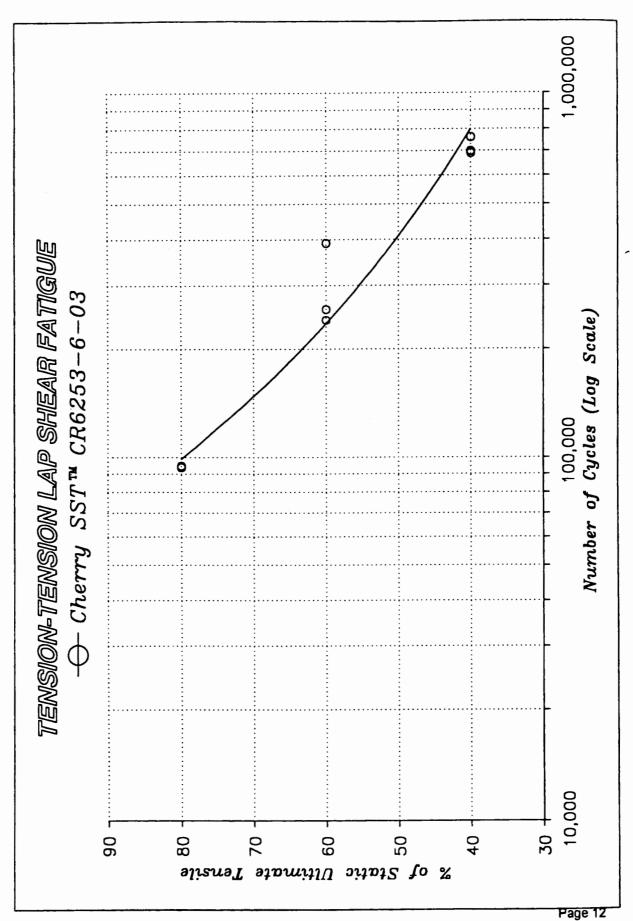


Figure 4. Cherry SSTTM Results

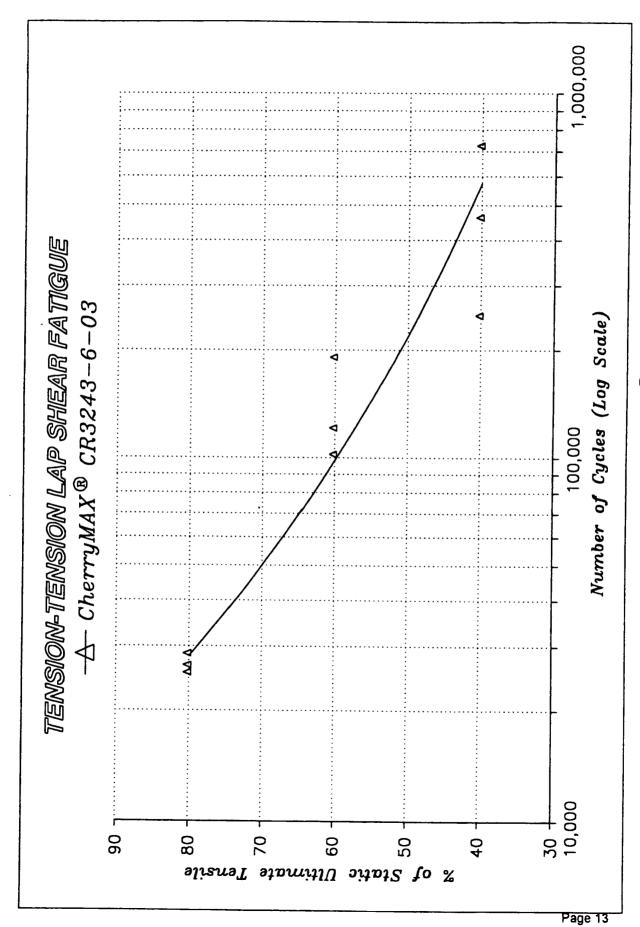


Figure 5. CherryMAX® Results

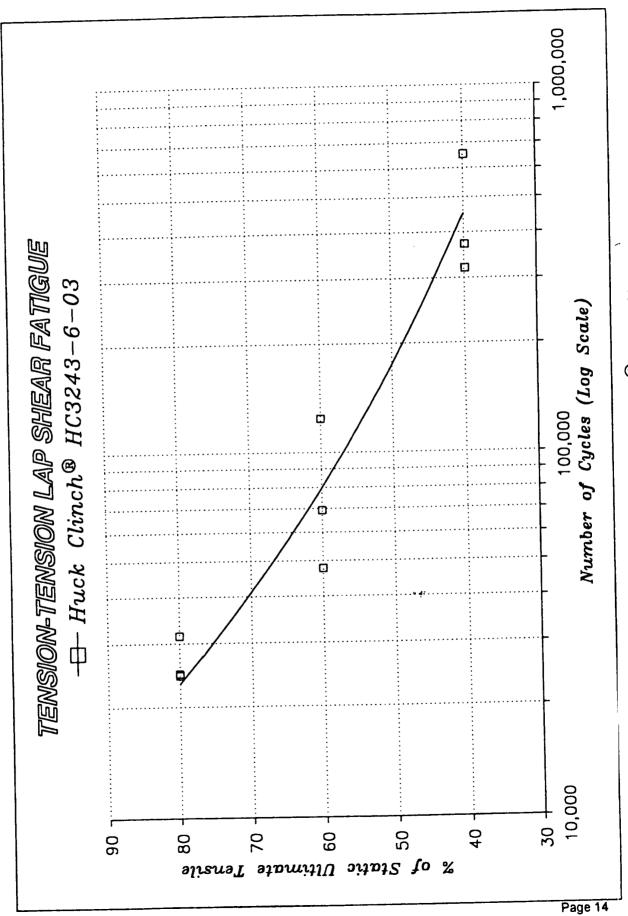


Figure 6. Huck Clinch® Results

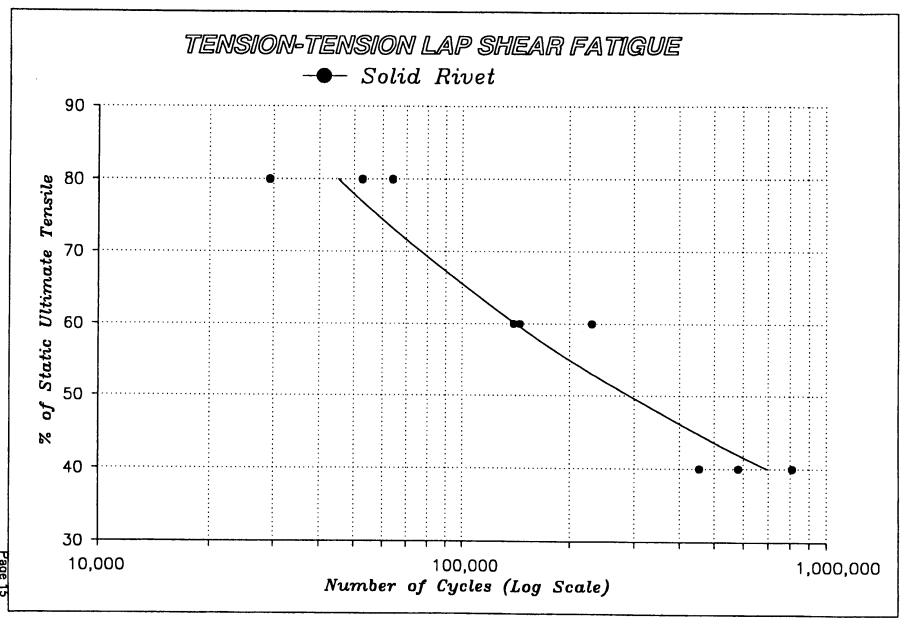


Figure 7. Solid Rivet Results

U.S. PATENT #4,012,984 #5,052,870 #5,056,973

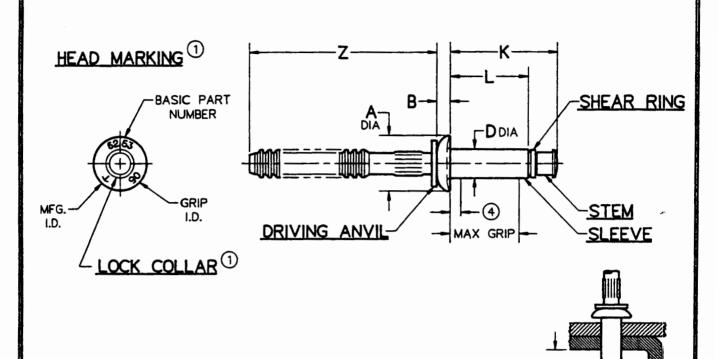
#5,131,107

CHERRY TEXTRON

AEROSPACE FASTENING SYSTEMS

FEDERAL IDENTIFICATION

CODE 11815



DIA. DASH		4	В	D	Z	BK	RECOMMENDED HOLE		
NO.	NOM. TOL.		±.005	±.002	REF	MIN ②	LIMITS		
-4	.250 ±.012		.059	.141	.87	.390	.143/.146		
-5	.312	±.016	.072	.174	.94	.395	.176/.180		
-6	.375 ±.019		.085	.202	.94	.410	.205/.209		
-8	.500	±.025	.112	.268	.97	.490	.271/.275		

	MATE	RIAL ③			FIN	ISH	
SLEEVE	STEM	LOCK COLLAR	SHEAR RING	SLEEVE	STEM	LOCK COLLAR	SHEAR RING
5056 ALUM. PER QQ-A-430	A-286 CRES PER AMS 5731	A-286 CRES PER AMS 5731 OR INCONEL 718 PER AMS 5664	A-286 CRES PER	CHEM. FILM PER MIL-C-5541 PLAIN COLOR	PASSIVATE PER QQ-P-35	NONE	NONE

NOTICE: ALL DIMENSIONS IN INCHES AND APPLY AFTER FINISH AND BEFORE LUBRICATION.

WARNING: FASTENERS MAY NOT PERFORM PROPERLY IF ALTERED FROM THE MANUFACTURER'S AS-SHIPPED CONDITION OR INSTALLED IN CONDITIONS OTHER THAN SPECIFIED HEREIN.

PROCUREMENT SPECIFICATION: PS-CMR-6000

NONE

NAS 523 CODE :

BULB RIVET-CHERRYMAX®II

1/64 OVERSIZE DIAMETER
UNIVERSAL HEAD

SHEET	r	1	OF	2	PART NUMBER
ISSUE	Q	7	-23-	92	CR6253
REV.	С	0	5-0	3-93	CROZOO

BK 2

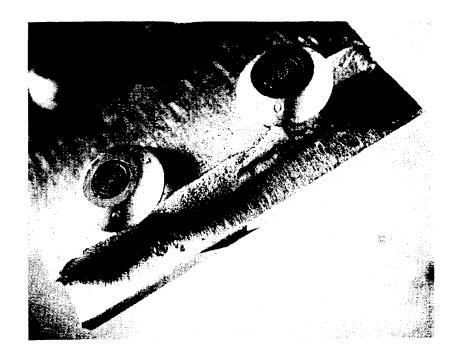


Figure 8. Typical Cherry SST™ Failure

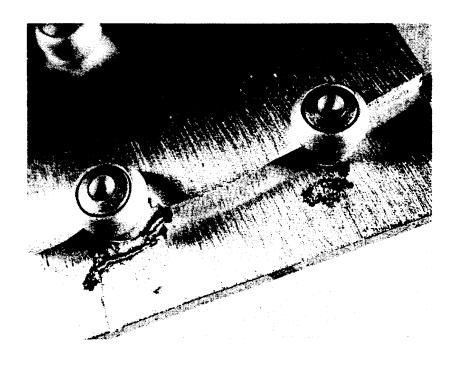


Figure 9. Typical CherryMAX® Failure

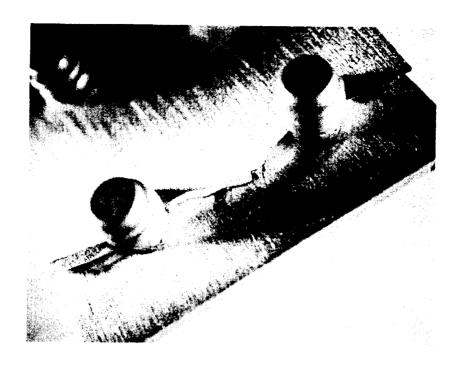


Figure 10. Typical Huck Clinch® Failure

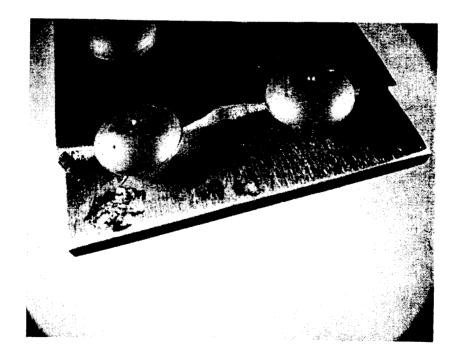


Figure 11. Typical Solid Rivet Failure

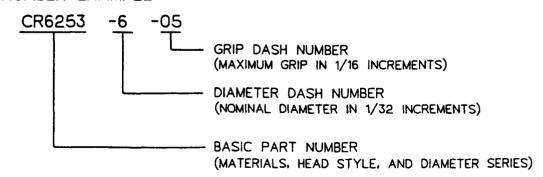
AEROSPACE FASTENING SYSTEMS

GRIP	GF	RIP	-4	DIA	- 5	DIA	-6	DIA	-8	DIA
DASH	LIM	ITS	L	K	L	K	L	K	L	K
NO.	MIN	MAX	REF	REF	REF	REF	REF	REF	REF	REF
-02	.063	.125	.238	.46	.246	.47	.265	.50		
-03	.126	.187	.301	.52	.309	.53	.328	.55	.375	.64
-04	.188	.250	.363	.58	.371	.60	.390	.62	.437	.70
-05	.251	.312	.426	.65	.434	.66	.453	.68	.500	.77
-06	.313	.375	.488	.71	.496	.72	.515	.74	.562	.83
-07	.376	.437	.551	.78	.559	.79	.578	.82	.625	.89
-08	.438	.500	.613	.84	.621	.85	.640	.89	.687	.95
-09	.501	.562	.676	.90	.684	.91	.703	.95	.750	1.02
-10	.563	.625			.746	.98	.765	1.01	.812	1.08
-11	.626	.687			.809	1.04	.828	1.07	.875	1.14
-12	.688	.750					.890	1.14	.937	1.20
-13	.751	.812							1.000	1.27
-14	.813	.875							1.062	1.33

NOTES : 1) HEAD MARKINGS AND LOCK COLLAR VISIBLE AFTER INSTALLATION.

- 2 MINIMUM BLIND SIDE CLEARANCE FOR SATISFACTORY INSTALLATION.
- 3 MATERIAL DESIGNATION REFERS TO CHEMICAL COMPOSITION ONLY.
- 4 AN INCREASE OF .001 IN "D" DIAMETER IS PERMISSIBLE FOR A DISTANCE OF .100 UNDER THE MANUFACTURED HEAD.

PART NUMBER EXAMPLE :



SHEET 2 OF 2	PART NUMBER
ISSUE 07-23-92	CDCOCZ
REV. C 05-03-93	CR6253

U.S. PATENT

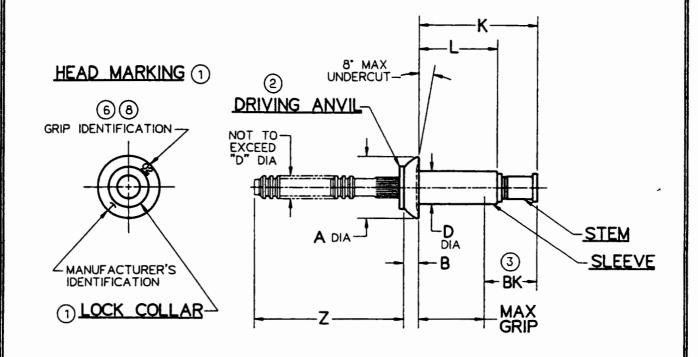
(OTHER PATENT PENDING)

CHERRY TEXTRON

AEROSPACE FASTENING SYSTEMS

FEDERAL IDENTIFICATION

CODE 11815



DIA. DASH	Α	В	D	Z	BK	HO LIM	LE ITS
NO.	±.010	+.010 000	+.003 001	MIN	MIN	MIN	MAX
-4	.250	.054	.140	.87	.390	.143	.146
-5	.312	.067	.173	.94	.395	.176	.180
-6	.375	.080	.201	.94	.410	.205	.209
-8	.500	.107	.267	.96	.490	.271	.275

SEE SHEET 2 FOR LENGTH DIMENSIONS, MATERIALS AND FINISHES
SEE SHEET 3 FOR NOTES AND PART NUMBER EXAMPLE

NOTICE: ALL DIMENSIONS IN INCHES AND APPLY AFTER FINISH AND BEFORE LUBRICATION.

WARNING: FASTENERS MAY NOT PERFORM PROPERLY IF ALTERED FROM THE MANUFACTURER'S AS-SHIPPED CONDITION OR INSTALLED IN CONDITIONS OTHER THAN SPECIFIED HEREIN.

PROCUREMENT SPECIFICATION:
PS-CMR-3000

NAS 523 CODE : SEE SHEET 2

CHERRYMAX ® RIVET
UNIVERSAL HEAD LOCKED SPINDLE
(OVERSIZE)

SHEET 1 OF 3 PART NUMBER
ISSUE 06-24-92
REV. S 06-24-92
CR3243

AEROSPACE FASTENING SYSTEMS

GRIP	GR	IP ITS	-4	DIA	-5	DIA	-6	DIA	-8	DIA
DASH NO.		RANGE	L	Κ	L	К	L	Κ	L	κ
6	MIN	MAX	+.000 030	MAX	+.000 030	MAX	+.000 030	MAX	+.000 030	MAX
-01	4	.062	.175	.39	.203	.43	.242	.45		
-02	.063	.125	.238	.46	.246	.47	.265	.50	.313	.57
-03	.126	.187	.301	.52	.309	.53	.328	.55	.375	.64
-04	.188	.250	.363	.58	.371	.60	.390	.62	.437	.70
-05	.251	.312	.426	.65	.434	.66	.453	.68	.500	.77
-06	.313	.375	.488	.71	.496	.72	.515	.74	.562	.83
-07	.376	.437	.551	.78	.559	.79	.578	.82	.625	.89
-08	.438	.500	.613	.84	.621	.85	.640	.89	.687	.95
-09	.501	.562	.676	.90	.684	.91	.703	.95	.750	1.02
-10	.563	.625			.746	.98	.765	1.01	.812	1.08
-11	.626	.687			.809	1.04	.828	1.07	.875	1.14
-12	.688	.750					.890	1.14	.937	1.20
-13	.751	.812					.953	1.20	1.000	1.27
-14	.813	.875							1.062	1.60

FINISH CODE	NAS 523 CODE		MATERIAL	9	FINISH		
		SLEEVE	STEM	LOCK COLLAR	SLEEVE	STEM	LOCK COLLAR
	ARE	5056 ALUM. PER QQ-A-430	8740 STEEL PER AMS 6322	A-286 CRES PER AMS 5731	PLAIN COLOR PER	CAD. PLATE PER QQ-P-416 TYPE IL CL.2	PASSIVATE PER QQ-P-35
A		5056 ALUM. PER QQ-A-430	8740 STEEL PER AMS 6322	A-286 CRES PER AMS 5731	CHEM. FILM GOLD COLOR PER MIL-C-5541	CAD. PLATE PER QQ-P-416 TYPE IL CL.2	PASSIVATE PER QQ-P-35
9 PR	ARE	5056 ALUM. PER QQ-A-430	8740 STEEL PER AMS 6322	A-286 CRES PER AMS 5731	PLAIN COLOR PER	CAD. PLATE PER QQ-P-416 TYPE IL CL.2	PASSIVATE PER QQ-P-35
10) T		5056 ALUM. PER QQ-A-430	8740 STEEL PER AMS 6322	A-286 CRES PER AMS 5731	PLAIN COLOR PER	CAD. PLATE PER QQ-P-416 TYPE II, CL.2	PASSIVATE PER QQ-P-35

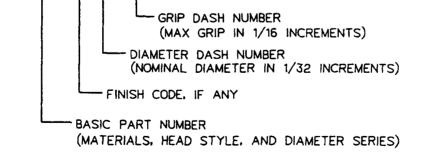
SHEET 2 OF 3	PART NUMBER	
ISSUE 06-24-92	CD7047	
DEVISION OF SE	CR3243	

AEROSPACE FASTENING SYSTEMS

- NOTES: (1) HEAD MARKINGS AND LOCK COLLAR VISIBLE AFTER INSTALLATION.
 - (2) SILVER COLORED DRIVING ANVIL IDENTIFIES OVERSIZE DIAMETER RIVETS.
 - (3) MINIMUM BLIND SIDE CLEARANCE FOR SATISFACTORY INSTALLATION.
 - (4) MINIMUM GRIP FOR -4 DIA. IS .025; FOR -5 IS .031; AND FOR -6 IS .037.
 - (5) MATERIAL DESIGNATION REFERS TO CHEMICAL COMPOSITION ONLY.
 - 6 SINGLE DIGIT HEAD MARKING IS PERMISSIBLE, AT MANUFACTURER'S OPTION, FOR GRIP DASH NUMBERS LESS THAN 10.
 - (7) SIZES BELOW HEAVY LINE ARE AVAILABLE ON SPECIAL ORDER ONLY.
 - (8) A DASH MAY BE MARKED UNDER OR TO THE RIGHT SIDE OF THE GRIP IDENTIFICATION AT MANUFACTURER'S OPTION.
 - 9 "PR" CODE PARTS ARE MANUFACTURED BARE; IF LUBE IS REQUIRED, USE PAR 90 ONLY.
 - (10) "T" CODE PARTS ARE MANUFACTURED BARE; IF LUBE IS REQUIRED. USE TRANSLUBE 20204 ONLY. TRANSLUBE ("T" CODE) WILL BE UNAVAILABLE FOR PROCUREMENT AS OF 01-01-92.

PART NUMBER EXAMPLE:

CR3243 A -5 -05



I	SHEET	•	3	OF	3	PART NUMBER		
	ISSUE 06-24-92				92	CR3243		
	REV.	S 06-24-92			-92	CR3240		