

NATIONAL TRANSPORTATION SAFETY BOARD

Office of Aviation Safety

Washington, D.C. 20594

July 17, 1996

ADDENDUM TO
SYSTEMS GROUP CHAIRMAN'S FACTUAL REPORT OF INVESTIGATION

A. ACCIDENT DCA-94-MA-076

Location: Aliquippa, Pennsylvania

Date: September 8, 1994, 1996

Time: 1904 Eastern Daylight Time

Aircraft: Boeing 737-300, N513AU

NATIONAL TRANSPORTATION SAFETY BOARD

Office of Aviation Safety

Washington, D.C. 20594

July 17, 1996

SYSTEMS GROUP CHAIRMAN'S FACTUAL REPORT OF INVESTIGATION

A. ACCIDENT DCA-94-MA-076

Location: Aliquippa, Pennsylvania

Date: September 8, 1994

Time: 1904 Eastern Daylight Time

Aircraft: Boeing 737-300, N513AU

B. SYSTEMS GROUP

Chairman: Greg Phillips
National Transportation Safety Board
Aviation Engineering Division
Washington, DC

Member: John Calvin
Boeing Commercial Airplane Group
Seattle, WA

Member: Paul Cline
Boeing Commercial Airplane Group
Seattle, WA

Member: Captain John Cox
Air Line Pilots Association/US Air
Coraopolis, PA

Member: Ken Frey
Federal Aviation Administration
Aircraft Certification Office
Seattle, WA

Member: Dale A. Hoth
Federal Aviation Administration
Flight Standards District Office
Coraopolis, PA

Member: Thomas C. Nicaastro
USAir-Engineering
Pittsburgh, PA

Member: Steve Weik
Parker Hannifin
Irvine, CA

Member: Jack A. Wurzel
USAir-IAMAW
Pittsburgh, PA

C. SUMMARY

On September 8, 1994, at 1904 Eastern Daylight time, USAir flight 427, a Boeing 737-3B7 (737-300), N513AU, crashed while maneuvering to land at Pittsburgh International Airport, Pittsburgh, Pennsylvania. The airplane was being operated on an instrument flight rules (IFR) flight plan under the provisions of Title 14, Code of Federal Regulation (CFR), Part 121, on a regularly scheduled flight from Chicago, Illinois, to Pittsburgh. The airplane was destroyed by impact forces and fire near Aliquippa, Pennsylvania. All 132 persons on board were fatally injured.

D. DETAILS OF THE INVESTIGATION

On March 7 through 9, 1995, the systems group members noted above met at the Parker Hannifin facilities in Ogden, Utah, to perform a detailed dimensional examination of the accident airplane's main rudder power control unit (PCU). The detailed dimensional analysis was conducted on parts and areas of parts determined by the group to be critical to the operation of the PCU.

A dielectric/insulation resistance check of the PCU was also conducted. The PCU passed the dielectric tests. Test results are included as Attachment 2.

The PCU bypass valves were tested and were found to operate normally. Test results are included as Attachment 3.

The group determined that there were no significant anomalies detected that would adversely affect the operation of the PCU.

The group also examined and operated a PCU mounted in a test fixture to examine the effects of binding and/or jamming on different points of the external input mechanisms. Several non-standard tests were conducted to demonstrate operation of the PCU to the group members. This examination was recorded on video tape.

1.0 Details of dimensional inspections

Prior to dimensional examination of the components, the systems group defined the critical areas for examination and identified them by marking the engineering drawings. The dimensional examination did not include every dimension on the engineering drawing, only those defined by the systems group. The data sheets used to record the dimensions are attached to this factual report as attachment 1. All noted drawing tolerances are for new parts and do not account for in-service wear.

Mr. Harby Gogna of Parker Hannifin-Ogden performed the measurements of the PCU components at the direction of the systems group. All measurements were within drawing tolerances for new parts for the following parts.

<u>Part #/Dwg Chg/# of measurements</u>	<u>Part Name</u>
69-35606/A/8	Guide-Spring, Double internal summing
69-35614/B/2	Cap-Detent, Internal Summing
69-35566/E/7	Crank Assy, Valve Input
69-35567/H/8	Lever Assy, Summing
69-35601/B,G/8	Crank, Redundant Valve Input
69-22760/A/1	Pin-Detent, Internal Summing
66-22825/B/6	Guide-Spring, Single Internal Summing
69-35602/C/14	Lever Assy, Primary
69-35563/D/1	Link Assy, Valve
60164/A/5	Roller Secondary, Slide operating
69-35611/C/4	Sleeve, Yaw Actuator
59174/K/1	Cap-End, Mod. Piston
59188/D/1	Diaphragm, LVDT Transducer

2.0 Details of simulated binding/jamming tests

2.1 Test Setup

The binding/jamming tests were conducted using a production Main Rudder PCU, P/N 65-44861-11, mounted in a production acceptance test fixture. The acceptance test fixture was modified so that a production input control rod could be installed on the PCU. The modification included the kinematic geometry of the input torque tube and the "J" section structure near the input control rod (see Figure 1). Also, the external summing lever assembly, and the H-link assembly were modified so that the degree-of-freedom could be removed from each of the positions 1 through 4 shown in Figure 1.

A yaw damper coupler was used to drive the yaw damper actuator in a closed loop configuration. The coupler could be moved to simulate the airplane yawing motion while monitoring the Main Rudder PCU output. No provisions were made to simulate the airplane rigid body loop of the yaw damper control system.

2.2 Test results

A loss of degree-of-freedom on the external summing lever did not produce any anomalous or amplified main rudder PCU output due to yaw damper commands. In two cases at positions 1 and 2, the feedback gain was increased and the output of the main rudder PCU, due to yaw damper commands, was less than 3°. Jamming position 3 to structure ("J" section) or removing the degree of freedom at position 3, had no affect on the main rudder PCU output due to yaw damper commands. Jamming the input control rod to structure, such as the "J" section, also had no affect on the main rudder PCU output due to yaw damper commands.

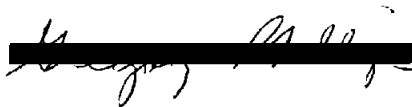
For all of the above jam conditions, the degree-of-freedom was completely removed, and the main rudder PCU motion through the input control rod was not possible.

Jamming the input crank to the manifold, or removing the degree-of-freedom at position 4, caused the main rudder PCU to go full deflection. In this case the input control rod was back-driven as the main rudder PCU deflected.

3.0 Video Documentation

Video documentation of the preceding tests was made and is attached to this report as attachment 4. The following is documented on video:

<u>Approximate Time</u>	<u>Events</u>
0-2:09	New PCU in test fixture, setup, yaw damper coupler
2:09-4:50	PCU operation with yaw damper input
4:50-7:30	Yaw damper input and PCU operation by moving yaw damper coupler
7:30-13:53	Simulated binding of center bearing on external summing link
13:53-19:30	Simulated binding of bearing nearest PCU on external summing
19:30-22:50	Simulated binding of input crank bolt
22:50-26:20	Simulated jams between input crank and PCU external manifold body stops
26:20-27:40	Examination of scrape mark on input rod at J-channel (new test unit)
27:40-30:22	Jam input rod against structure with yaw damper inputs
30:22-32:28	View of input rod clearance with structure
32:28-56:15	Secondary stroke flow test demonstration per Boeing overhaul manual



Gregory Phillips
Systems Group Chairman
National Transportation Safety Board

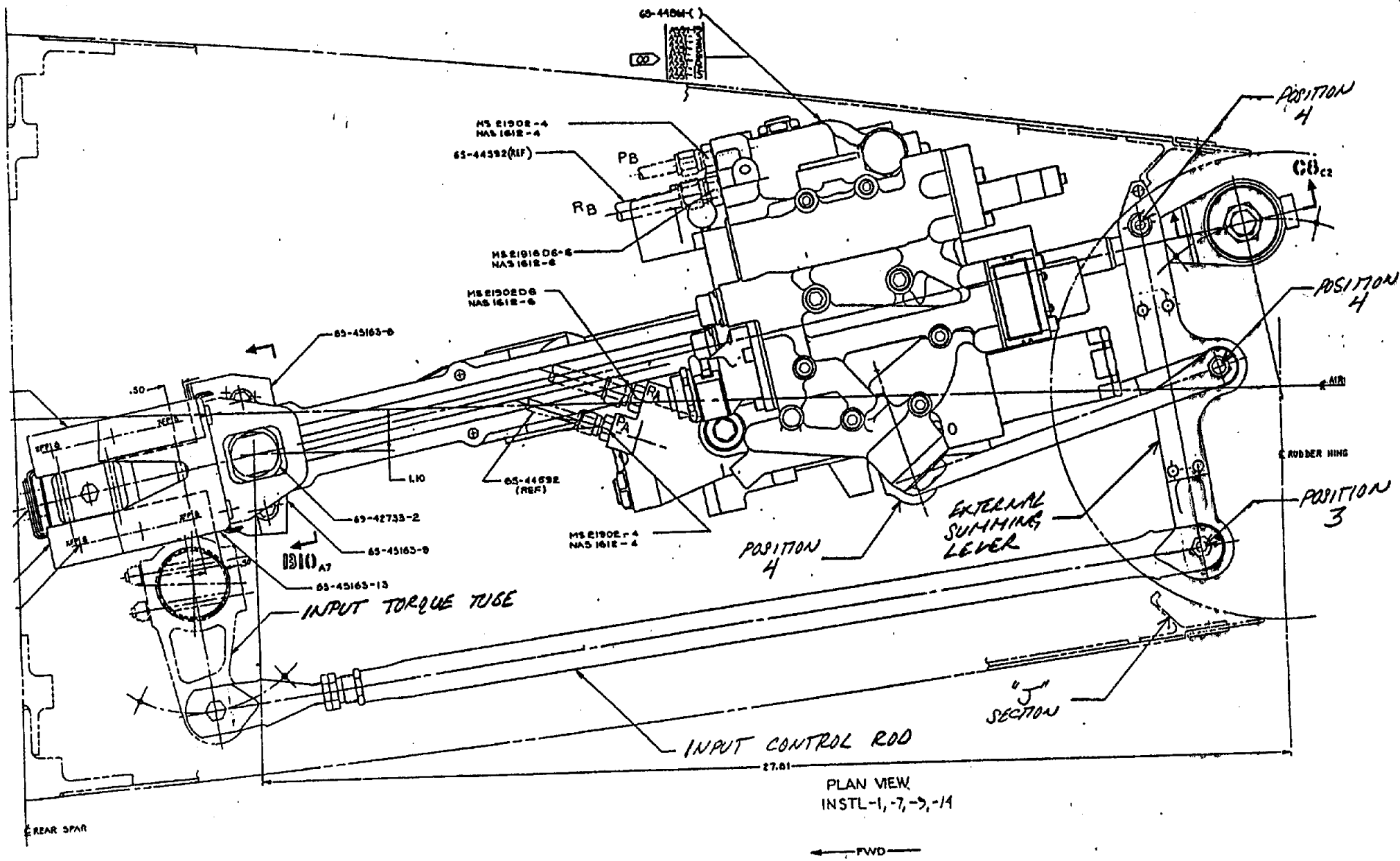


FIGURE 1

Attachment 1

[illegible]

[illegible]

[illegible]

Part No.

J946 NUMERICAL CONTROL INSPECTION

Part Number	Operation	B/P Rev.	Route
89-3555E	N/A	E	N/A
S/N	Inspector	Time	Date
1915	HARRY GOGNA	10:52 AM	8 Mar 1985

	ACTUAL	NOMINAL	+ TOL	- TOL	DEV	OUT-TOL
X	3.0000	3.0000	.0050	.0050	0.0000	
Y	0.0000	0.0000	.0050	.0050	0.0000	
Y	-.8768	-.8750	.0020	.0020	.0001	+
Y	.0000	.0000	.0020	.0020	.0017	++++
40	11.125	11.250	.250	.250	-.055	-
40	11.1111"	11.1510"	0.1510"	0.1510"	-0.319"	-
Y	-.3330	-.3330	.0030	.0030	.0001	+
40	6.5528	6.5533	0.1510"	0.1510"	0.1317"	++++
40	6.5510"	6.5533"	0.1510"	0.1510"	0.1317"	++++

[illegible]

Parker

J946 NUMERICAL CONTROL INSPECTION

Part Number	Operation	B/P Rev.	Route
68-35567	N/A	D	N/A

S/N	Inspector	Time	Date
1888	HARRY GOGNA	04:08 PM	8 Mar 1995

	ACTUAL	NOMINAL	+ TOL	- TOL	DEV	OUT-TOL
X	9.7487	9.7450	.0050	.0050	.0037	+++
Y	0.0000	0.0000	.0050	.0050	0.0000	

	ACTUAL	NOMINAL	+ TOL	- TOL	DEV	OUT-TOL
X	-4.1218	-4.1250	.0050	.0050	.0032	+
Y	1.3728	1.3820	.0050	.0050	-.0041	----

	ACTUAL	NOMINAL	+ TOL	- TOL	DEV	OUT-TOL
V	.0097	.0000	.0100	.0100	-.0013	-
W	.1154	.1250	.0100	.0100	.0004	+

[illegible]

PROGRAM 737		PART NAME GUIDE SPRING, SNGL. INTER. SWIMMING		DATE: 3-8-95		PAGE: 1 OF 1	
PARKER MADE <input type="checkbox"/> VENDOR MADE <input type="checkbox"/>		PART NO. 66-22825		DWG CHG B			
INSPECTED BY: HARRY S. GOGNA		STAMP		WORK ORDER:		ACC. 1	
VENDOR NAME		F.A.I.R. COMPLETE <input checked="" type="checkbox"/> UPDATE <input type="checkbox"/>		SERIAL NO.		NEXT ASSEMBLY	
PURCHASE ORDER NO.		UPDATE TO REV.				REL. 1	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]



J946 NUMERICAL CONTROL INSPECTION

Part Number	Operation	D/P Rev.	Route
68-35583	N/A	0	N/A

S/N	Inspector	Time	Date
0001	HARRY GOGNA	10:22 AM	8 Mar 1985

	ACTUAL	NOMINAL	+ TOL	- TOL	DEV	OUT-TOL
X	8.8327	8.8330	.0050	.0050	-.0003	-
Y	0.0000	0.0000	.0050	.0050	0.0000	

DAMAGED HOLE DIM.

X	8.8358	8.8330	.0050	.0050	.0028	+++
Y	-.0012	0.0000	.0050	.0050	-.0012	-

[illegible]



SCREEN - YAW ACTUATOR (G)

PART NUMBER: 69-35611

JOB NO:

REV: C

TOP ASSY P/N:

PROGRAM: 737

[illegible]



INSPECTION WORKSHEET

CAP-END, MOD. PISTON (6)

PART NUMBER: 59174

JOB NO:

REV: K

TOP ASSY P/N.

PROGRAM: 727,737

SERIAL NO:

LOT NO:

B/P DIM:

ACTUAL DIM:

AOC:

REJ:

[illegible]



INSPECTION WORKSHEET

PROGRAM:

[illegible]



Piston-Yaw ~~Control~~ ACTUATOR

REV. B

PROGRAM: 737

REJ:

[illegible]

PROGRAM		PART NAME		PART NO.	DWG CHG	
PARKER MADE <input type="checkbox"/> VENDOR MADE <input type="checkbox"/>		INSPECTED BY:		STAMP	WORK ORDER:	
VENDOR NAME:		P.A.I.R. COMPLETE <input type="checkbox"/> UPDATE <input type="checkbox"/>		SERIAL NO:	NEXT ASSEMBLY:	
PURCHASE ORDER NO.:		UPDATE TO REV.:		N/A	69-35603	
ITEM	B/P LOC	B/P REQ.	ACTUAL	COMMENTS	ACC.	REJ.
1		1.685 1.695 Ø	1.6898		215	
2		1.3001 1.3002 Ø	1.3001		215	
3		1.315 1.325	1.322		215	
4		.263 .267	ASSY		215	
5		1.563 ± .010	1.567		215	
6		.005 MAX MISMATCH	ASSY REG'S BEAR REMOVAL		215	
7		2.322 ± .010	2.319		215	
8		2.763 2.767	2.7668		215	
9		45° ± 1/2° X .050 ± .010 3PL	45° X .038 .020		215	
10		.462 .464	.464		215	

[illegible]

DATE: 3-8-95 PAGE: 1 OF 1

[illegible]

[illegible]

MANIFOLD, AFT (GP)

PARKER
FIRST ARTICLE TAPE INSPECTION

TAPE PROOF

Part #: 65-44863	Tape #:	Operation:	Drawing Change: REV T (62)
Job #:	Date:	S/N:	Planning Change:
Inspected By:			ACC: REJ:

LOC	DET	FT	DIM	HOLD@	TOLERANCE	ACTUAL	ACC	REJ
1 1/2		LC	.750		.755 .745	.7523	(S)	
1 B/6		LO	2.238		2.240 2.236	2.2381	(S)	
1 A/2		LO	2.750		2.755 2.745	2.7497	(S)	
1 B/3		LO	2.827		2.824 2.825	2.8260	(S)	
1 B/3		LO	1.625		1.627 1.625	1.6255	(S)	
1 1/2		FC	4.000		4.000 4.0			
1 1/2		FC	4.000		4.0010 3.999	3.9989	(S)	
1 1/4		FC	3.000		3.001 2.999	3.0005 - 3.0017	(S)	
1 B/5		LO	2.238		2.236 2.240	2.236	(S)	
1 1/3		LO	2.750		2.755 2.745	2.740	(S)	
1 B/6		LO	3.160		3.162 3.158	3.1562 (THD LOCATED IN INSERT?)	(S)	
1 B/6		LO	2.800		2.802 2.798	2.7994	(S)	
1 1/9		FC	1.450		1.448 1.452	1.4495	(S)	
1 1/9		FC	.800		.798 .802	.7995	(S)	
1 1/13		F/C	.913		.912 .914	.9125 - .9132	(S)	

MANIFOLD, AFT (GP) FIRST ARTICLE TAPE INSPECTION

[illegible]

Attachment 2

TEST
PROCEDURE

CHECK BY

DATE

PART NO: 65-44861-		SERIAL NO:	VALVE NO:	DATE:																															
IBM NO:		PART NAME RUDDER ACTUATOR P.C.U.		INSP:																															
TEST	REQUIREMENTS		RESULTS	ACC.	REJ.																														
20 LOW PRESSURE LEAKAGE	NO EXTERNAL LEAKAGE IN 2 HOURS.																																		
21 FLUSHING	FLUSH AND FILL WITH BMS 3-11 FLUID. CAP PORTS AND ELEC. RECEPTACLE.																																		
22 TEST ACCEPTANCE	INK STAMP BODY WITH DATA AND TEST ACCEPTANCE STAMP.																																		
ELECTRICAL TESTS - PERFORM IN SEQUENCE SHOWN																																			
23 DIELECTRIC STRENGTH 4.3.2	<p>SLOWLY APPLY NOTED VOLTAGE. NO ARCING OR INSULATION FAILURE IN ONE MINUTE. REDUCE VOLTAGE TO ZERO BEFORE DISCONNECTING.</p> <p>BODY TO PIN 1 AT 1500 VAC PIN 1,5,7, & BODY TO PIN 11 PIN 1,5,7, & BODY TO PIN 9 PIN 1 & BODY TO PIN 5 PIN 1 & BODY TO PIN 7 AT 1000 VAC PIN 5 TO PIN 7 PIN 9 TO PIN 11 AT 800 VAC</p>		<p>-5, THRU -9, 11, SYS. ONLY</p> <p>SYS "A" SYS "B"</p> <p>_____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u></p>																																
24 INSULATION RESISTANCE 4.3.3	<p>APPLY 500 VDC BETWEEN NOTED PINS. 100 MEGOHMS MIN RESISTANCE (REQUIREMENT)</p> <p>PINS 1,5,7,9,11 TO BODY PINS 5,7,9,11 TO 1 PINS 7,9,11 TO 5 PINS 9,11 TO 7 PINS 11 TO 9</p>		<p>-5, THRU -9, 11, SYS. ONLY</p> <p>SYS "A" SYS "B"</p> <p>_____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u> _____ <u>OK</u></p>																																
25 PIN TO PIN RESISTANCE	<p>CHECK PIN TO PIN RESISTANCE AT 70°F AND RECORD. MUST COMPLY WITH NOTED VALUE</p> <table border="1"> <thead> <tr> <th>PINS</th> <th>RESISTANCE</th> </tr> </thead> <tbody> <tr> <td>1-2</td> <td>71-87 OHMS</td> </tr> <tr> <td>5-6</td> <td>900-1100 OHMS</td> </tr> <tr> <td>7-8</td> <td>900-1100 OHMS</td> </tr> <tr> <td>9-10</td> <td>80-165 OHMS</td> </tr> <tr> <td>11-12</td> <td>60-135 OHMS</td> </tr> <tr> <td>1-4</td> <td>SHORTED</td> </tr> <tr> <td>3</td> <td>OPEN</td> </tr> </tbody> </table>		PINS	RESISTANCE	1-2	71-87 OHMS	5-6	900-1100 OHMS	7-8	900-1100 OHMS	9-10	80-165 OHMS	11-12	60-135 OHMS	1-4	SHORTED	3	OPEN	<p>SYS "A" SYS "B"</p> <table border="1"> <tbody> <tr> <td><u>77</u></td> <td><u>77</u></td> </tr> <tr> <td><u>1003</u></td> <td><u>1003</u></td> </tr> <tr> <td><u>1003</u></td> <td><u>1003</u></td> </tr> <tr> <td><u>104</u></td> <td><u>104</u></td> </tr> <tr> <td><u>83</u></td> <td><u>83</u></td> </tr> <tr> <td><u>Short</u></td> <td><u>Short</u></td> </tr> <tr> <td><u>open</u></td> <td><u>open</u></td> </tr> </tbody> </table>	<u>77</u>	<u>77</u>	<u>1003</u>	<u>1003</u>	<u>1003</u>	<u>1003</u>	<u>104</u>	<u>104</u>	<u>83</u>	<u>83</u>	<u>Short</u>	<u>Short</u>	<u>open</u>	<u>open</u>		
PINS	RESISTANCE																																		
1-2	71-87 OHMS																																		
5-6	900-1100 OHMS																																		
7-8	900-1100 OHMS																																		
9-10	80-165 OHMS																																		
11-12	60-135 OHMS																																		
1-4	SHORTED																																		
3	OPEN																																		
<u>77</u>	<u>77</u>																																		
<u>1003</u>	<u>1003</u>																																		
<u>1003</u>	<u>1003</u>																																		
<u>104</u>	<u>104</u>																																		
<u>83</u>	<u>83</u>																																		
<u>Short</u>	<u>Short</u>																																		
<u>open</u>	<u>open</u>																																		

65-44861-1

PG. 28 OF 32

1-1031-59

HA

Attachment 3

BOEING COMMERCIAL JET OVERHAUL MANUAL

(d) Apply 18 volts dc to pins A and C of receptacle (21). Valve must open without audible delay (indicated by fluid flow from cylinder port).

(6) Pressure Drop Test

- (a) Open cylinder and return ports.
- (b) Apply 28 volts dc to pins A and C of receptacle (21).
- (c) Gradually apply 140-psi fluid pressure to pressure port. Measure flow at cylinder port. Flow must be at least 0.4 gpm.

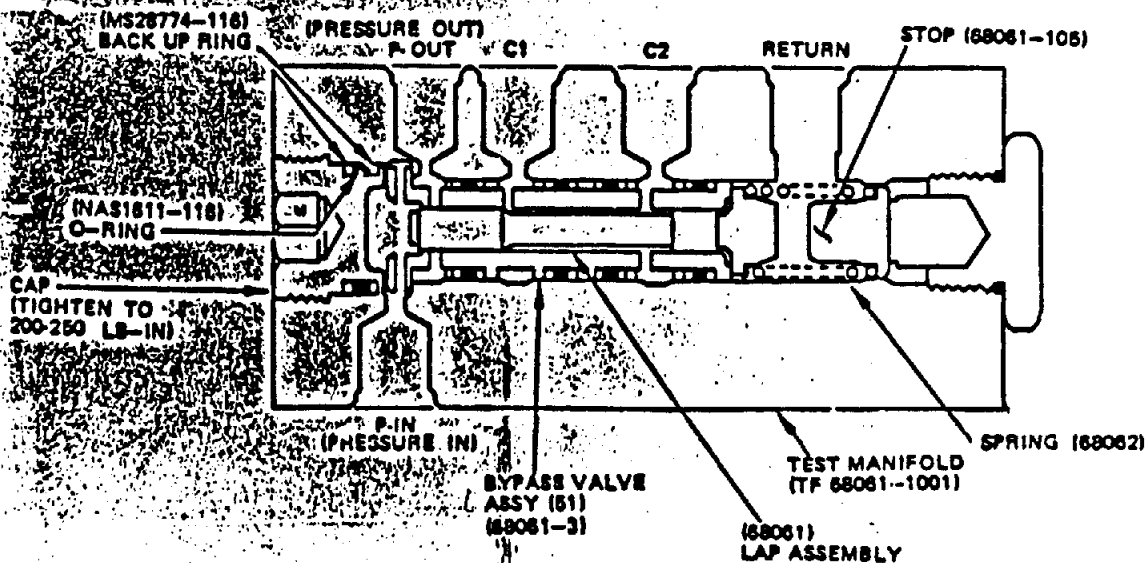
6. Bypass Valve Assembly Pretest (Fig. 1101).

A. Test Equipment

- (1) Test Fixture: TF68061-1001 (Fig. 710)
- (2) Suitable supply of fluid pressure
- (3) Suitable pressure gages, valves and flowmeters

B. Friction and Flow Tests (Fig. 1101).

- (1) Install bypass valve (51) in test fixture TF68061-1001 (Fig. 710).
- (2) Install a suitable plug in pressure outlet port.



Bypass Valve Test Setup
Figure 710

65-44861
65-45160

BOEING
COMMERCIAL JET
OVERHAUL MANUAL

- (3) Connect port C2 to flowmeter.
- (4) With R (return port) open, apply pressure simultaneously to P-IN (pressure inlet) and port C1.
- (5) Raise pressure to 250 psi and measure flow from C2. Flow from C2 shall be 1.08 gpm minimum.
- (6) Slowly increase pressure until flow from C2 reduces to approximately 166 cc per minute.
- (7) Measure maximum flow obtained prior to flow reduction to 166 cc per minute. Maximum flow shall be 1.75 gpm.
- (8) Measure pressure at which flow reduction to 166 cc per minute from C2 occurs. Pressure shall be 460 psi maximum.
- (9) Reduce pressure to 200 psi and measure flow from C2. Flow from C2 shall be 0.97 gpm minimum.
- (10) Connect port C1 to flowmeter and repeat previous tests (1) through (9) applying pressure to P-IN and port C2 simultaneously.

C. Leakage Test

- (1) Install suitable plug in P-OUT (pressure outlet) port.
- (2) Open R port and connect port C1 to flowmeter.
- (3) With 3000-psi pressure applied to P-IN port and port C2, measured flow from R port shall not exceed 19 cc per minute.
- (4) With pressure to C2 port reduced to 1500 psi, measure flow from port C1. Flow from port C1 shall be 209 to 409 cc per minute.
- (5) Open port C2 and measure flow from ports C1 and C2 combined. Flow from ports C1 and C2 shall not exceed 6 cc per minute.

D. Bypass Flow Test

- (1) With all other ports open and 50-psi fluid pressure applied to P-IN port, measured flow from P-OUT port must be 0.05 to 0.20 gallon per minute.

7. Check Valve Pretest (See figure 1101.)

A. Proof Pressure Test

Parker

PRODUCTION TEST PROCEDURE

DRAWN BYD. CHRISTENSEN DATE 12-26-








CHECK BY S. WEIK DATE 11-5-8

PART NO: -1 68061-3		SERIAL NO: 6420	VALVE NO: 68061-3	DATE: 3-8-95			
IBM NO:		PART NAME BYPASS VALVE (A-SPSTEM)		INSP:			
TEST	REQUIREMENTS		RESULTS	ACC. REV.			
1 2	FRICTION & FLOW C1 - C2 C2 - C1		PRESS	P IN, C2	P IN, C1		
			FLOW	C1	C2		
		A) 1.08 GPM MIN. AT 250 PSI		<u>1.20</u> GPM <u>250</u> PSI	<u>1.15</u> GPM <u>250</u> PSI		
		B) 1.75 GPM MAX BEFORE SHUT-OFF.		<u>1.35</u> GPM	<u>1.3</u> GPM		
		C) 460 PSI MAX AT SHUT-OFF		<u>360</u> PSI	<u>360</u> PSI		
		D) REDUCE PRES: 0.97 GPM MIN. AT 200 PSI.		<u>1.05</u> GPM <u>200</u> PSI	<u>1.00</u> GPM <u>200</u> PSI		
3	LEAKAGE ① ⑤	C1: 15 CC/MIN MAX (-1) (MIL-H-5606 10 CC/MIN)		C1	R		
	FLOW ①	300 ± 100 CC/MIN (-3) (MIL-H-5606 260 ± 50 CC/MIN)					
	LEAKAGE ① ⑤	R: 15 CC/MIN MAX (MIL-H-5606 10 CC/MIN) (-1, -3)	<u>200</u> CC/MIN	<u>No leakage</u> CC/MIN			
4	LEAKAGE ① ⑤	C1 & C2 COMBINED: 5 CC/MIN MAX. (MIL-H-5606 3.5 CC/MIN)		<u>1</u> CC/MIN			
5	BYPASS FLOW	P OUT: .20/.05 GPM (P OUT: .22/.05 GPM MIL-H-5606)		<u>0.18</u> GPM			
6	TEST ACCEPTANCE	AFTER SATISFACTORY TEST, INK STAMP WITH TEST ACCEPTANCE.					



CHECK BY S. WEIK DATE 11-5-8

PART NO: -1 68061-3	SERIAL NO: 6430	VALVE NO: 68061-3	DATE: 3-8-95
IBM NO:	PART NAME By pass Valve (B-SYSTEM)		INSP:

TEST		REQUIREMENTS	RESULTS		ACC.	REPT.	
1 2	FRICTION & FLOW C1 - C2 C2 - C1		PRESS	P IN, C2	P IN, C1		
			FLOW	C1	C2		
		A) 1.08 GPM MIN. AT 250 PSI		<u>1.15</u> GPM <u>250</u> PSI	<u>1.14</u> GPM <u>250</u> PSI		
		B) 1.75 GPM MAX BEFORE SHUT-OFF.		<u>1.4</u> GPM	<u>1.3</u> GPM		
		C) 460 PSI MAX AT SHUT-OFF		<u>370</u> PSI	<u>365</u> PSI		
	D) REDUCE PRES: 0.97 GPM MIN. AT 200 PSI.		<u>0.97</u> GPM <u>200</u> PSI	<u>1.00</u> GPM <u>200</u> PSI			
3	LEAKAGE  	C1: 15 CC/MIN MAX (-1) (MIL-H-5606 10 CC/MIN)		C1	R		
	FLOW 	300 ± 100 CC/MIN (-3) (MIL-H-5606 260 ± 50 CC/MIN)					
	LEAKAGE  	R: 15 CC/MIN MAX (MIL-H-5606 10 CC/MIN) (-1, -3)		<u>250</u> CC/MIN	<u>No leakage</u> CC/MIN		
4	LEAKAGE  	C1 & C2 COMBINED: 5 CC/MIN MAX. (MIL-H-5606 3.5 CC/MIN)		<u>1.5</u> CC/MIN			
5	BYPASS FLOW	P OUT: .20/.05 GPM (P OUT: .22/.05 GPM MIL-H-5606)		<u>0.18</u> GPM			
6	TEST ACCEPTANCE	AFTER SATISFACTORY TEST, INK STAMP WITH TEST ACCEPTANCE.					

68061-T

PG. 4 OF 4

Boeing Spec 10-60926

68061-T

25

Form 1041-19

39