NTSB Identification: ERA12FA120 Accident occurred December 22, 2011 in Nashville, PA Aircraft: Cessna 441 Conquest II, Registration: N48BS

Date of Report: February 17, 2012

Introduction:

The following analyses were performed by Honeywell based on information provided during the preliminary and on-scene investigations into this accident. Honeywell was requested by the NTSB to perform a fuel burn estimate of two model TPE331-10N-535S installed on the subject aircraft along the provided flight path.

Two separate, independent analyses were performed. One was a purely analytical analysis while the second was a fuel usage estimate from a pilot's planning perspective.

Summary:

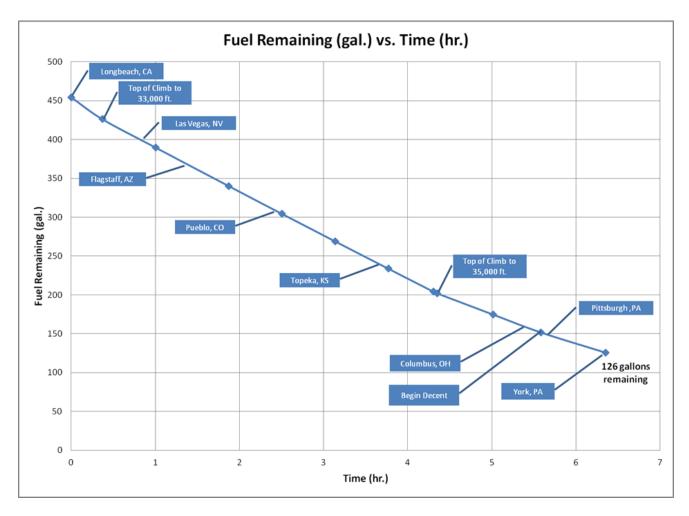
Both, independent, analyses concurred that, given specific assumptions (as detailed below), there should have been sufficient fuel remaining to complete the flight into York, PA with IFR reserve fuel remaining.

Analytical Analysis:

The first, independent, analysis performed was a purely analytical analysis of fuel burn based on information provided to the engineering team along with assumptions which included:

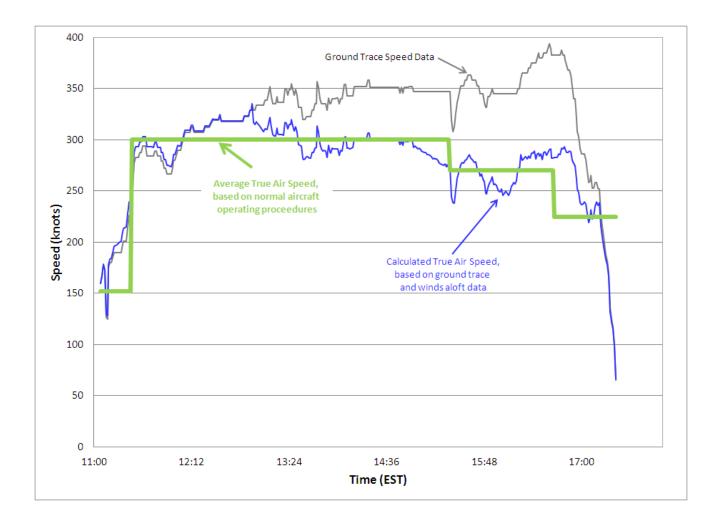
- Flight path as provided by Flight Aware
- Winds aloft as provided by the NTSB
- Propeller performance characteristics as provided by Hartzell
- Fuel burn characteristics as given in the West Star Aviation, Inc. Pilots Operating Handbook and FAA Approved Airplane Flight Manual Supplement for Cessna Model 441 Airplanes Serial No. -0173 and On Equipped with Garrett TPE331-10N engines.
- Take Off Weight: 9200 lb
- Fuel: Full fuel / 475 gal. (3230 lb)
- Empty Weight: 5700 lb.
- Pilot Weight: 170 lb.
- Baggage: 100 lb
- Cruise Speeds: Averaged from winds aloft and ground track data

The assessment indicates that the aircraft likely had 126 gallons of fuel left at the time of the accident.



	Track Data					Aircraft Mission Analysis Results				
Segment	Туре	Altitude (ft)	Air Speed (KTAS)	Head Wind (knots)	Seg. Time (hr)	Seg. Ground Distance (n-mile)	Air Speed (KTAS)	Head Wind (knots)	Seg. Time (hr)	Seg. Ground Distance (n-mile)
1	Taxi	0	0	0	0.00	0	0	0	0	0
2	Takeoff	0	0	0	0.00	0	0	0	0.00	0
3	Climb	33000	152	7	0.37	53	152	7	0.37	53
4	Cruise	33000	294	9	0.63	181	300	14	0.63	181
5	Cruise	33000	310	2	0.87	267	300	-8	0.87	267
6	Cruise	33000	317	-20	0.63	213	300	-37	0.63	213
7	Cruise	33000	295	-45	0.63	215	300	-40	0.63	215
8	Cruise	33000	301	-52	0.63	224	300	-53	0.63	224
9	Cruise	33000	282	-63	0.53	184	300	-45	0.53	184
10	Climb	35000	272	-72	0.05	10	270	-72	0.04	10
11	Cruise	35000	272	-83	0.67	237	270	-86	0.67	237
12	Cruise	35000	267	-99	0.57	207	270	-96	0.57	207
13	Descent	0	225	-50	0.77	211	225	-50	0.77	211
				Total	6.35	2004		Total	6.35	2003

Due to the scatter in the winds aloft data and the resolution of the ground track data, this analysis used average cruise speeds for the assessment. The last chart below illustrates the level of scatter in cruise speeds calculated from the winds aloft and ground track data.



Pilot's Fuel Usage Estimates:

The second, independent, analysis performed was from a pilot's perspective using typical fuel burn estimates as would be performed prior to flight departure.

Proviso:

- All aircraft performance data is based the West Star Aviation, Inc. STC SA5682NM, dated September 30, 1993 for Cessna Model 441 Airplanes Serial No.-0173 and on (note: the FAA registry identifies the aircraft serial number for N48BS as -0125).
- The take off gross weight (TOGW) is assumed to be 9,850 Lbs
- The zero flight weight (ZFW) is assumed to be 6,667 Lbs
- The take off fuel load is assumed to be 3183 Lbs
- Aircraft is flown using AFM recommended power settings

From a flight planning point of view, the intended flight on Dec 22, 2011 from KLGB to KTHV [KLGB direct DAG, DAG to KTHV along a great circle path], at a total distance of 2,008 NM can be made with sufficient IFR reserve fuel remaining at the destination.

This assessment is based on the following 3 different sources of information:

Data from the STC AFM Supplement (Standard Atmosphere no wind).

1. PERFORMANCE AND SPECIFICATION (Page i)

1. PERFORMANCE AND SPECIFICATION (Pag Maximum Cruise Power	je I)								
At 35,000 Feet	Range 2,248 NM								
	8.81 Hrs								
	259 KTAS								
2. RANGE PROFILE (Page 5-24)									
Maximum Range Power Curve									
At 35,000 Feet	Approximate Range 2,160 NM								
	257 KTAS								
Data from the STC AFM Supplement (Non-Standard Atmosphere and Wind Component) 3. PLANNING NAV LOG (Table A)									
Total Distance KLGB – KTHV	2,008 NM								
	5.8 HRS								
	Fuel Remaining 764 LBS								
Note: PLANNING NAV LOG (Table A) is based on STC AFM Supplement data as follows: (Page 5-14) TIME, FUEL, AND DISTANCE TO CLIMB – MAXIMUM CLIMB (Page 5-17) MAXIMUM RECOMMENDED CRUISE POWER									

Note: Data from NWS Forecast Winds and Temperature Aloft (FD) Valid Dec 22, 1800Z

- (Table B) NWS FORECAST WINDS AND TEMPERATURE ALOFT (FD) DATA BASED ON DEC 22, 1200 Z
 - (Table C) FL330 INTERPOLATION WIND AND ΔT FROM SA
 - (Table D) FL330 EFFECTIVE TAILWIND/HEADWIND COMPONENT (+T/-H).

	NAV PLAN KLGB - KTHV FL 33 N48BS									30 at ISA*	
3,183	lbs Fuel	6,667	lbs ZFW					Fuel		GW	
KLGB	NM	TC	KTAS	+T/-H	GS	MINUTES	FF	Burn	Remain	9,850	
	72		196	10	206	22.0	600	220	2963	9,630	
L/O	31.9	48	305	10	315	6.1	401	41	2922	9,589	
DAG	255.4	69	307	10	317	48.3	401	323	2599	9,266	
BCE	191.3	72	308	20	328	35.0	401	234	2365	9,032	
GJT	92.9	73	309	53	362	15.4	410	105	2260	8,927	
ALS	76.4	76	309	53	362	12.7	410	87	2174	8,841	
PUB	14.7	74	309	39	348	2.5	410	17	2156	8,823	
DEN	130.3	77	310	53	363	21.5	410	147	2009	8,676	
GLD	23.2	80	310	60	370	3.8	410	26	1983	8,650	
GCK	151.8	78	311	52	363	25.1	410	171	1812	8,479	
SLN											
MKC	142.2	80	312	54	366	23.3	410	159	1653	8,320	
STL	194.1	83	313	72	385	30.2	410	207	1446	8,113	
SPI	29.3	86	313	70	383	4.6	410	31	1415	8,082	
IND	164.8	86	314	96	410	24.1	410	165	1250	7,917	
	159.8	88	314	77	391	24.5	410	168	1082	7,749	
СМН	133.7	89	315	102	417	19.2	410	131	951	7,618	
AGC	144.3	91	316		316	27.4	410	187	764	7,431	
KTHV											

Based on NWS Forescats Winds and Temperature Aloft (FD) FL 300 [Interpolated]

* BCE= ISA +5 GJT= ISA +3

Ref: AFM Supplement S/N -0173 and on, page 5-17 and page 5-24

(Table A)

<u>NWS Forecast Winds and Temperature Aloft (FD)</u> Bulletin current prior to the accident was as follows, issued at 1400Z and valid for 1800Z and for use between 1400-2100Z for the first half of the planning:

(Table B)

Valid 221800Z Flight Level Flight Level Flight Level 300 340 330 SA °c °c °c W dir W dir ΔT °c WV W dir WV wv Station -45 -45 27 -45 5 BCE 320 19 290 29 298 3 240 -46 260 22 255 -47 GJT 17 -47 21 1 ALS 240 62 -47 250 51 -49 248 54 -49 -1 PUB 240 56 -49 250 52 -51 248 53 -51 DEN 230 37 -50 250 39 -50 245 39 -50 0 GLD 230 240 55 238 55 -2 53 -50 -53 -52 GCK 240 -49 -54 61 -3 56 240 63 240 -53 49 -48 61 -53 58 -2 SLN 240 230 233 -52 MKC 230 -46 230 0 51 230 65 -51 62 -50 STL 210 109 -43 210 114 -53 210 113 -51 -1 -1 210 -43 220 116 -54 218 114 SPI 108 -51 -42 0 IND 230 111 240 115 -53 238 114 -50 CMH 240 100 -43 240 100 -52 240 100 -50 0 0 AGC 250 250 250 103 -42 111 -52 109 -50

Winds and Temperature Aloft

(Table C)

Winds and Temperature Aloft Valid 221800Z

	Fl	ight Level		Flight Level			Flight Level			Effective
		300			340		330			Wind
Station	W dir	WV	°c	W dir	WV	°c	W dir	WV	°c	+T/-H
BCE	320	19	-45	290	29	-45	298	27	-45	10
GJT	240	17	-46	260	22	-47	255	21	-47	20
ALS	240	62	-47	250	51	-49	248	54	-49	53
PUB	240	56	-49	250	52	-51	248	53	-51	53
DEN	230	37	-50	250	39	-50	245	39	-50	39
GLD	230	53	-50	240	55	-53	238	55	-52	53
GCK	240	56	-49	240	63	-54	240	61	-53	60
SLN	240	49	-48	230	61	-53	233	58	-52	52
MKC	230	51	-46	230	65	-51	230	62	-50	54
STL	210	109	-43	210	114	-53	210	113	-51	72
SPI	210	108	-43	220	116	-54	218	114	-51	70
IND	230	111	-42	240	115	-53	238	114	-50	96
CMH	240	100	-43	240	100	-52	240	100	-50	77
AGC	250	103	-42	250	111	-52	250	109	-50	102