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S-61 Long Body Hover Performance Test Report

October 19, 2010

Carson Helicopters Report, CHI 61-100

Prepared by:

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S-61 Long Body Hover Test Report

1. Introduction

A flight test program was conducted by Carson Helicopters to evaluate the improvement in hover performance of a long body S-61N when equipped with Carson composite main rotor blades. One objective of the tests was to provide flight data that could be used to develop new hover performance charts. Both in ground effect (IGE) and out of ground effect (OGE) tests took place at three different sites in order to obtain a range of density altitudes. The airports were Leadville, CO (LXV), Alamosa, CO (ALS) and Casa Grande, AZ (CGZ). Nominal density altitudes at these locations during the testing were 10400 ft, 7300 ft, 2400 ft, respectively. The aircraft used by Carson for these tests was a standard category S-61N, (line 25 of Sikorsky S-61 Configuration Summary), registration no. N15456 (C/N61826). The aircraft was equipped with Carson main rotor blades and optional fixed gear. The components of the aircraft are detailed in Appendix A. The aircraft is shown in Figure 1 taken at Casa Grande, AZ. In this flight program, a number of tests were conducted to evaluate the Category A and Category B performance in addition to the hover that are not discussed here. For some of the Cat A and B tests the retractable gear/sponson configuration was also flown. The hover performance was evaluated IGE at a 10 ft wheel height and OGE at a 100 ft wheel height. The IGE tests were conducted in free flight, using internal weights (400 lbs increments) that were off loaded to vary the weight of the aircraft. The OGE tests used the standard tethered hover technique. Note that because of safety concerns, the OGE hover testing is not conducted in the same manner as the IGE testing, in free flight with internal loading. Winds were monitored and test conditions used for chart development were those where the ambient wind was less than 3 kts. The nose of the aircraft was held into the wind, as is standard procedure for these tests.

All the hover performance tests were conducted with the aircraft in the fixed land gear configuration as shown in Figure 1. Primary data including torque of both engines and tether load cell reading were recorded via computer with record lengths of 6 to 8 seconds. Other variables of importance, e.g., fuel weight, were recorded on the pilot cards. Charlie Evans was the DER pilot. FAA personnel also flew a number of test points.

In the following, the following equivalents may be helpful:

1 % Torque (Q) = 24 HP at NR=100% and 1HP \approx 5 lbs lift

Rotor speeds: (NR) = 100% = 203 rpm (tip speed = 659fps)
103% = 209 rpm (679 fps), 106% = 215 rpm (699 fps)

The complete test series took place during the period from 9/27/2006 until 3/08/2007.

2. Hover Test Schedule

The hover performance test schedule was as follows:

Leadville, CO

Flight #1 100 ft tether hover 9/27/06, time: 1646 to 1719
Flight #2 10 ft IGE hover 9/28/06 time: 0736 to 0918
Flight #7 10 ft IGE hover 9/30/06 (no data terminated due to wind)
Flight #11 FAA 10 ft IGE and OGE hover 10/02/06

Alamosa, CO

Flight #2 10 ft IGE hover 10/25/06 time: not recorded
Flight #6 100 ft tether hover 11/1/06 time 0735 to 0835
Flight #7* 100 ft tether hover 11/2/06 time: 1646 to 1719 (conducted at Leadville, CO, a repeat of Leadville #1)

Casa Grande, AZ

Flight #4 10 ft IGE hover 11/10/06 time: 1200 to 1254 (data invalid, repeated in #7 and #8)
Flight #6 100 ft tether hover 11/11/06 time: 0956 to 1050
Flight #7 10 ft IGE hover 01/18/07 time: 0801 to 0844
Flight #8 10 ft IGE hover 01/18/07 time: 1022 to 1120

* For Alamosa Flight #7 the aircraft was returned to Leadville, CO to repeat the OGE flight there (#1), due to concern about a discrepancy in the load cell readings. A replacement load cell of a different manufacturer had been installed prior to the Alamosa series of tests and was used for the remainder of the test program. Very good agreement between the data from these two flights, Leadville #1 and Alamosa #7 showed that the cockpit readout was in error and that the first load cell computer output was indicating the load correctly. The agreement between these flights is shown in Figure 2. The calibration problem was determined to be associated with the cockpit indicator. Cockpit

readings were not used in the data reduction process, although the readings are listed on the pilot cards. Note that computer recorded data were used for all data reduction and analysis.

3. Hover Test Results

The OGE tests were conducted at three rotor speeds (NR = 100%, 103%, and 106%). NR=100% corresponds to 203 RPM.

The data points obtained from each location during the OGE tests were (See pilot cards in Appendix B):

Leadville, CO #1	36
Alamosa, CO #6	54
Alamosa, CO #7(at Leadville)	44
Casa Grande, AZ #6	61

The total number of points is 195. The development of the OGE charts used a total of 96 of these data points. Since the new performance charts for the Carson blades charts were to be developed for NR = 100% and 103%, the NR = 106 % data generally were not included in the 96 points for the chart development. As the non-dimensional data did not show any significant trend with rotor speed as illustrated for example in Figure 3, the 100% and 103% data were combined to determine the power coefficient-weight coefficient (CP-CW) relationship. This result is to be expected due to the use of modern airfoils on the Carson rotor blades, the swept tip and the lower tip speed of the S-61 (Mtip = 0.59 at SLS conditions at NR=100%).

Points were selected from the total above based on the strength of the ambient wind (< 3 kts) and where the recorded time history of an event indicated a well established steady hover condition. Inconsistencies in the data sets and other relevant factors were used to eliminate some points from consideration. Figure 4 shows the 96 data points and the curve fit. As a check on the sensitivity of this result to the data point selection procedure, the 96 point (CP-CW) curve fit was compared to one using 186 points (9 from Leadville were not included). The difference was found to be 0.5% torque (≈ 12 HP) or less depending upon the loading condition, well within the accuracy of the test measurements, and indicating that the selection did not introduce a significant bias in the result.

The IGE tests were also conducted at same three rotor speeds (Appendix B). Points obtained:

Leadville #2	60
Alamosa #2	39
Casa Grande #7	33

Total points 162, with 132 used to develop charts.

Figure 5 shows the non-dimensional IGE results used to develop the corresponding IGE charts. As a consequence of the small effect of rotor speed illustrated in Figure 3, all three rotor speeds were used in the development of the IGE charts. This would tend to be conservative since any small effect of tip speed would tend to be unfavorable.

Comparing the IGE and OGE results, the increase in thrust at constant power IGE is consistent with other results reported in the literature.

4. Correlation with other sources

A recent hover flight test was conducted at the Carson Helicopters facility in August 2010. Both Sikorsky Aircraft (SAC) and Carson Helicopters made independent measurements of hover performance using a short body aircraft with land gear, N3173U, (C/N 61186) at the Carson Facility. This is a restricted category ex US Navy SH-3A, civil designation S-61A (line 2 of Sikorsky S-61 Configuration Summary), modified by AFC 314 (Airframe Group-An Improved Tail Pylon and Tail Drive Shaft Group). This AFC modifies the pylon so the large tail rotor (10 ft 7.25 in diameter) can be incorporated and also replaces the small stabilizer (20 sq ft) with the large one (27 sq ft). AFC 314 was complied with via US Navy contract with Sikorsky and Carson installed the fixed landing gear via STC. Only hover OGE tests were made with this aircraft. The tests were conducted with an external load, rather than using a tether, the other alternative for hover OGE tests. Safety of flight considerations rule out the use of internal loading or other methods for OGE tests. Three different external loads were used (7260 lbs, 5198 lbs and 3160 lbs). The largest load was about 4 ft square in planform and suspended on a 105 ft cable. The aircraft was hovered such that the load was between 5 and 10 feet above the ground, so that the aircraft was at an AGL of 110 to 115 ft. With the external load in this location, no additional download would be encountered in hover.

This aircraft employed for these recent tests (N3173U) is very similar to the aircraft used by Carson for the flight tests that were used to develop the hover charts, described above (N15456). Both have fixed main gear and 10 ft 7.25 in. diameter tail rotors. The tail rotor moment arm measured from the main rotor shaft to the tail rotor shaft is 1 inch longer (FS 708.5) on N3173U than on N15456 (FS 707.5), the N model. The hub is at FS 267.5. One external difference may be noted, the vertical tail surface has a greater sweep angle on the modified A model (60°) than on the N model (45°). An aircraft similar to N3173U is shown in Figure 6. Component details for these two aircraft are provided in Appendix A. Two independent instrumentation packages were installed in the aircraft, one by SAC and the other by Carson. A tethered balloon flown at the altitude of the hovering aircraft was used to determine the ambient wind.

Three flights were made with Carson main rotor blades on the 9th, 10th and 19th of August 2010. One flight was made with metal blades, but the data was not considered satisfactory due to the wind conditions. An unconventional test technique was selected by SAC where each loading condition at evaluated at four relative wind angles (0°, 90°, 180°, and 270°. The standard technique is to conduct hover tests at one azimuth, 0° (nose into the wind).

A large number of data points were generated during the three days in which conditions were satisfactory for testing (ambient winds less than 3 knots). The use of all azimuth data tends to produce an apparent significant increase in power, even though the wind is less than 3 knots. This effect is shown in Figure 7 where the all azimuth data is shown with nose into the wind points identified. It can be seen that generally, the nose into the wind data indicates the lowest power. Restricting consideration to a comparison of nose into the wind data from this test program, using the data set recorded and reduced by SAC, excellent agreement with Carson long body data of Figure 1 is shown in Figure 8. The data of Figure 1 were of course taken by the standard method of hover testing with the aircraft nose into the wind.

4a. A Note on Fuselage Download

The long body fuselage planform area exposed to the main rotor downwash is increased by 29.5 sq ft (about a 10% increase) compared to the short body aircraft. In addition, the cockpit section is moved forward to a region of higher downwash. These changes would tend to reduce hover performance of the aircraft by increasing the fuselage download. Using an advanced rotor aerodynamics code to calculate the main rotor downwash distribution over the fuselage, and applying drag coefficients, the increase in download due to the increase in fuselage length is estimated by Carson to be 50-65 pounds (equivalent to roughly a 10 HP increase) at SLS conditions at a gross weight of 20000 lbs. This result is similar to SAC download estimates.

Another organization, QinetiQ in the UK, has extensively tested the Carson blades for their use on Westland Sea Kings by the Royal Navy. Although they did little hover performance testing, they did report that the Carson blades produced 1760 lbs of additional lift in hover, comparable to that discussed below in the comparison section.

SAC/US Navy made a brief series of hover performance tests on a short body aircraft with Carson main rotor blades. This aircraft is an NVH-3A (Bu. no. 150614), modified to the VH-3D configuration (line 16 of Sikorsky S-61 Configuration Summary). There are a number of significant differences between this aircraft and the two described above. Adjustable trim tabs were added to the Carson blades outboard of the fixed tab (0.9R). Note that Carson Helicopters does not use adjustable tabs as seven years experience with

the blades has demonstrated that they are not required for tracking. The tabs are located far outboard on the trailing edge of the blade (from 0.90R to 0.95R) where they are likely to contribute a loss in main rotor efficiency. The tail rotor is of smaller diameter (10 ft 4 in). At high altitudes, the tip of the tail rotor blade is likely to be either stalled or very close to stall. The tail moment arm is 3 in less (FS 704.5) than on the N model. In addition, one main rotor blade was instrumented with strain gages whose lead wires were taped to the upper and lower blade surfaces increasing blade drag and reducing the rotor efficiency. In addition, an unconventional method of hover testing, described above, was used where measurements were made at four relative wind azimuths. The recent tests conducted in August of 2010 at the Carson facility also used this method. The penalty incurred by this approach is indicated in Figure 7 compared to the standard approach of using nose into the wind data. All of the above factors (added trim tabs, small tail rotor, instrumentation wires on one blade, and the method of testing) would be expected to contribute to a loss in performance. The poor efficiency of the small tail rotor is discussed in detail in "A Review of Tail Rotor Design and Performance", C.V. Cook, *Vertica*, Vol. 2 .

As a result of some controversy generated by the results of this flight test with Carson main rotor blades described in the paragraph immediately above related to the validity of the Carson long body charts, Carson Helicopters contracted an independent organization, Whipple Aviation Services, LLC to make a series of hover performance measurements with an S-61N. These results of the Whipple tests are shown on the Figure 9 along with the results of Figure 1. The few points agree very well with Carson data.

5. Comparison with Metal Blade Performance

The Carson blades give a significant improvement in hover performance compared to the standard metal blades. The performance increase is particularly evident at higher altitudes. Figure 10 compares the lifted weight vs. power at 6000 ft, 15° C for both sets of main rotor blades. The metal blade curve in the figure is derived from Figure 4-8 of Sikorsky Aircraft S-61N Flight Manual, SA 4045-82. The Carson blade curve is from the Carson Rotorcraft Flight Manual Supplement No.8, Figure 6. The lift increase produced by use of the Carson blades is shown to be 1700 lbs at 2200 HP at this atmospheric condition. This improvement increases with altitude and power.

The very good agreement of the data among these various sources supports the validity of the Carson flight test data and consequently the Carson long body charts derived from these tests.

6. Aircraft Details

The Carson test aircraft was an S-61N, with registration number N15456, C/N 61826 .

a.) Power Usage:

Electrical loading: 28v DC system. Current less than 40 amps (less than 2 HP)

Bleed air: no bleed air

Air conditioning: not installed

Heating setting: off

Engine de-ice setting: off

b.) Instrumentation

OAT: aircraft instrument

Pressure altitude: aircraft instrument

Engine temperature: aircraft instrument

Main rotor tachometer: aircraft instrument and a digital readout meter

AGL height measurement:

OGE: Aircraft AGL determined by the length of tether cable, 100 feet

IGE: Calibrated radar altimeter. The altimeter was calibrated for a 10 ft wheel height above ground by a line dropped to the ground.

Wind conditions: Tethered balloon at the height of the hovering aircraft, AWOS data and hand held anemometers

7. Calibrations

a.) Tether Load Cell Calibration

Two load cells were used in the long body flight test program. Carson personnel conducted the calibrations. The first calibration took place on 9/20/06 prior to initial tether hover testing at Leadville, CO on 9/27/06. The results are shown in Figure 11. There was concern about the performance of this load cell due to a difference between the cockpit reading and computer output. As a consequence, the unit used in Leadville was replaced with a different model after the Leadville tests as noted above. The replacement was calibrated on 10/30/06, prior to the first Alamosa tether hover test on 11/1/06. This load cell was used for this and all succeeding tests. This calibration is shown in Figure 12. As a result of a possible problem associated with the operation of the load cell used in Leadville Flight #1, this OGE hover test was repeated on 11/2/06 with this new load cell. The test results from this flight (denoted above as Alamosa #7) agreed very well with Leadville #1 as shown in Figure 2.

Generally, the computer results using these calibrations showed that the cockpit readouts showed a larger load than indicated from the computer.

b.) Torque Calibration

The engine torques are determined by pressure measurements in the torque indicating system. In the flight test programs described above, pressure transducers were installed at suitable locations for each engine in the Engine Torque Indicating System. See Sikorsky Aircraft S-61N Maintenance Manual, SA 4045-80, pps. 201-206 for a description of the system. The relationship between the system oil pressure and indicated torque of the engine is given in Figure 202 on page 206. This is the standard method of engine torque measurement used by SAC. The calibration curves for engines #1 and #2 are shown in Figures 13 and 14.

8. Figures

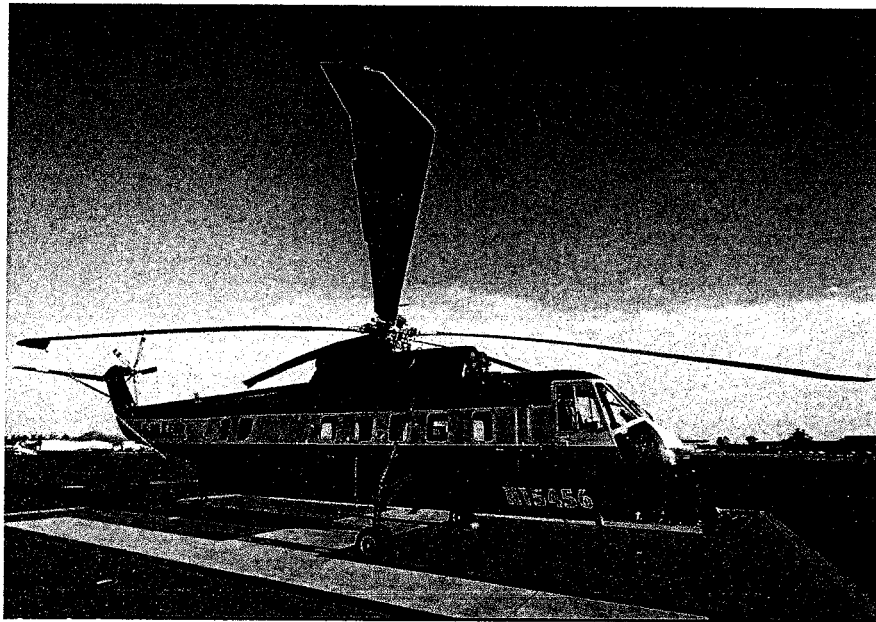


Figure 1: Carson Flight Test Aircraft, Long Body S-61N, 2006/2007

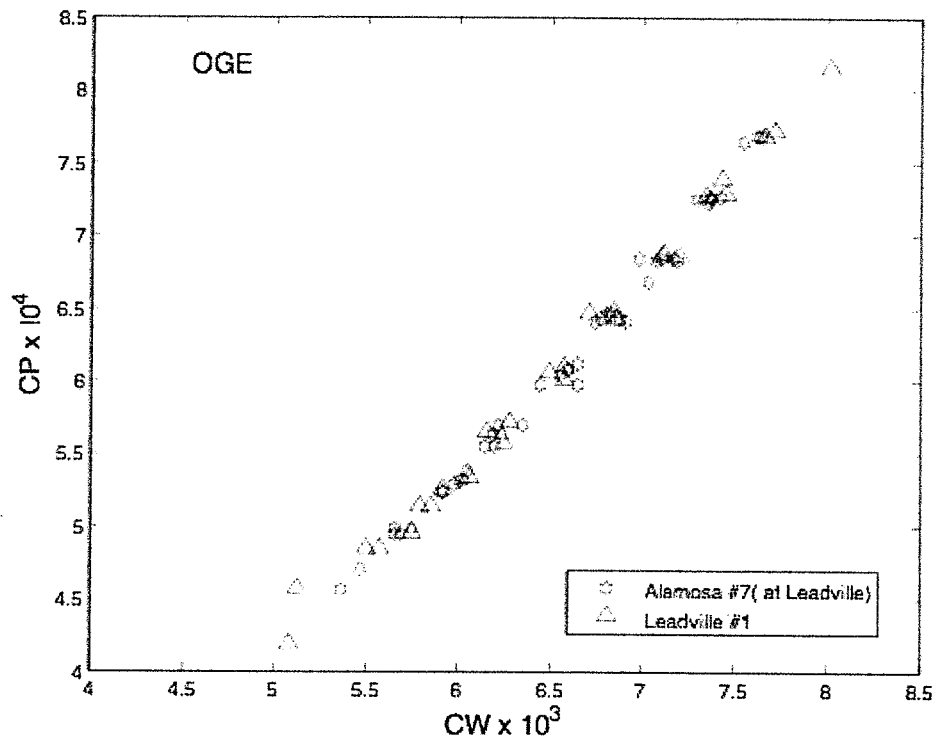


Figure 2: Comparison of Flight Test Results at Leadville Using Two Different Load Cells

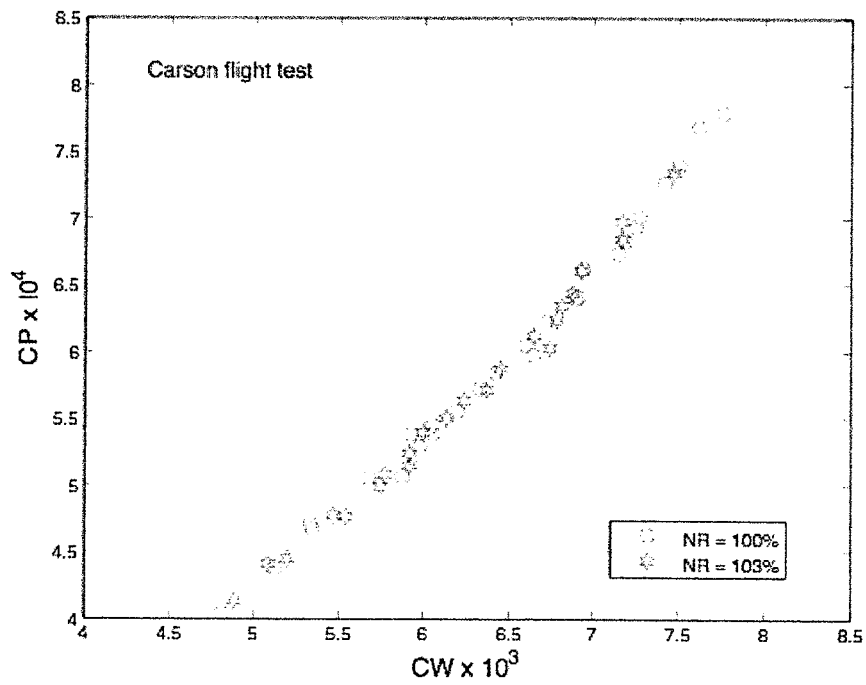


Figure 3: Effect of Rotor Rotational Speed on S-61N Hover Performance with Carson Blades

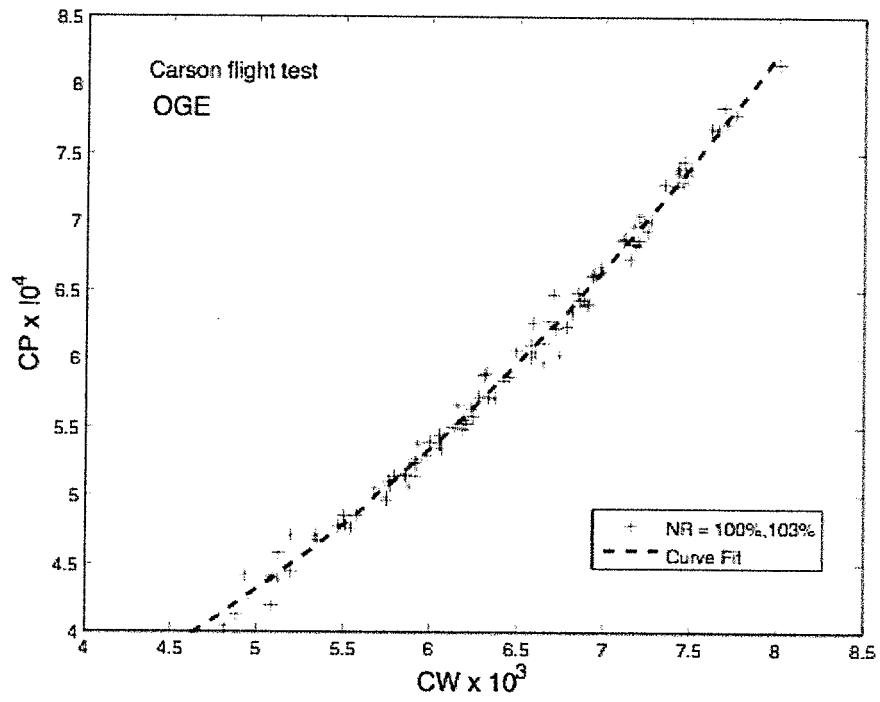


Figure 4: Hover Performance Data OGE and CP-CW Curve Fit used for Chart Development with Carson Blades

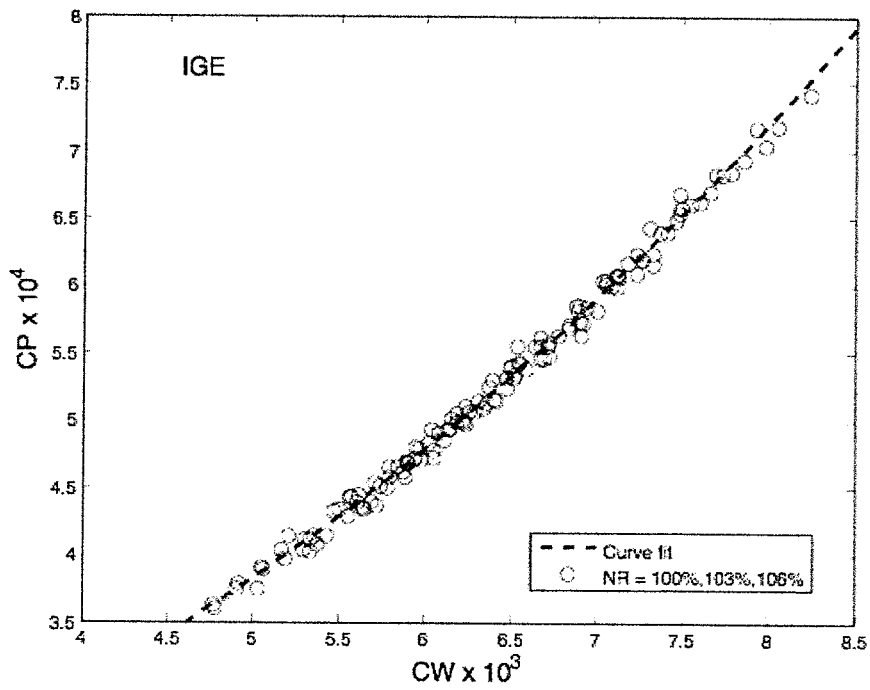


Figure 5: Hover Performance Data, IGE and CP-CW Curve Fit used for Chart Development with Carson Blades



Figure 6: Carson/SAC Flight Test Aircraft, August 2010

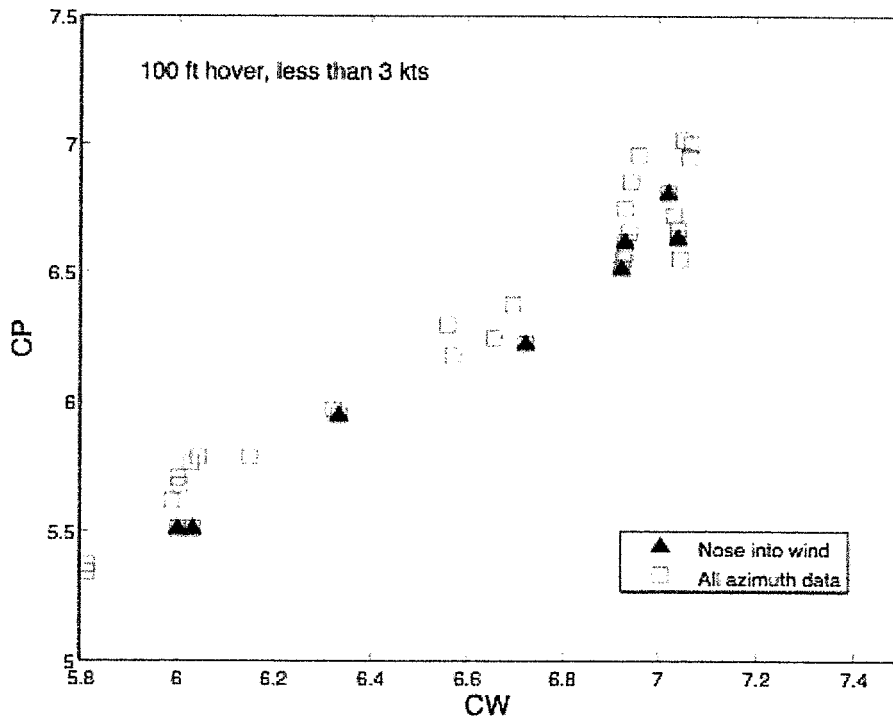


Figure 7: Effect of Wind Azimuth on Hover Performance. Wind Less Than 3 kts

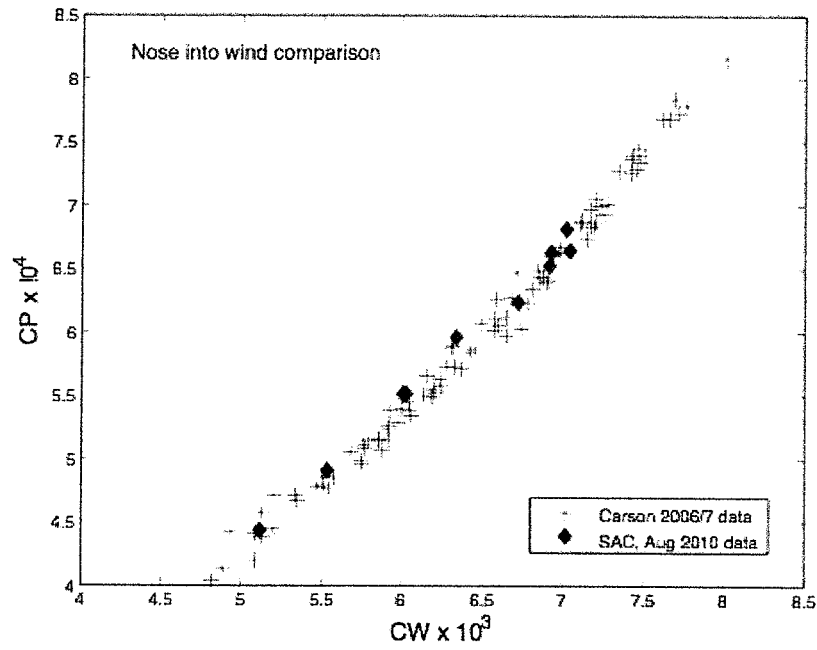


Figure 8: Comparison of Nose into Wind Data, Carson 2006/7 and SAC 2010 Flight Test

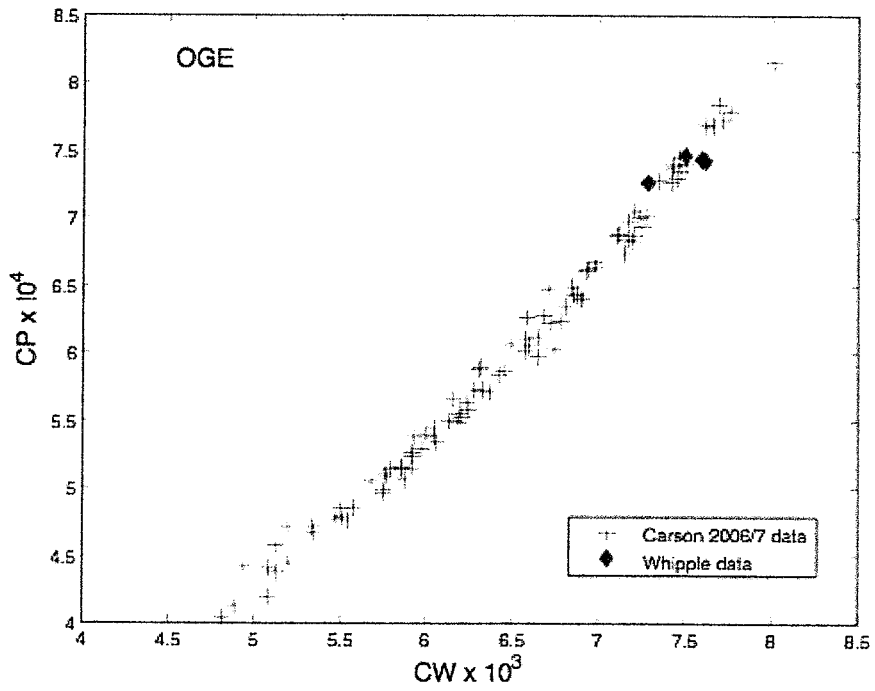


Figure 9: Comparison of Carson Flight Test 2006/7 with Whipple Test 2010

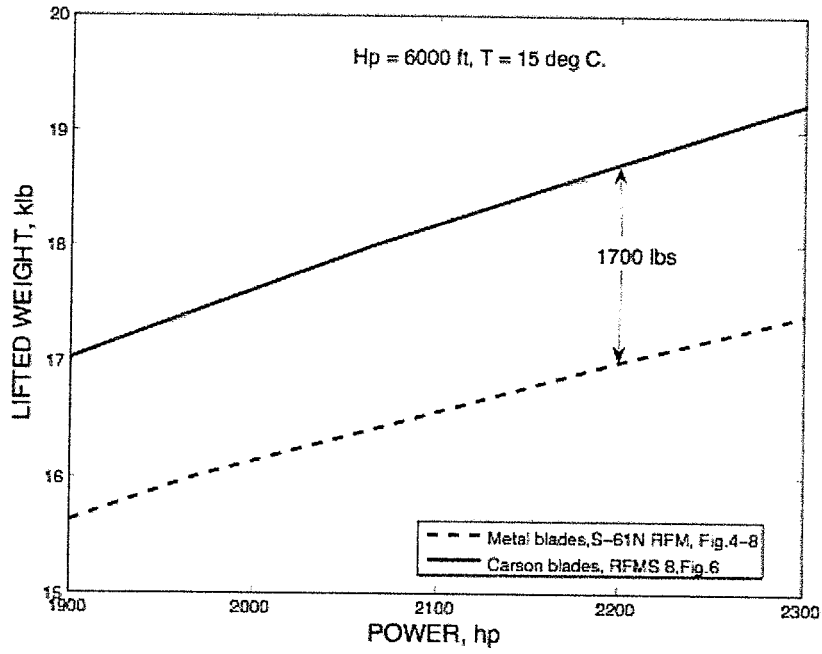


Figure 10: Comparison of S-61N Performance with Carson Blades and Metal Blades Derived from Performance Charts

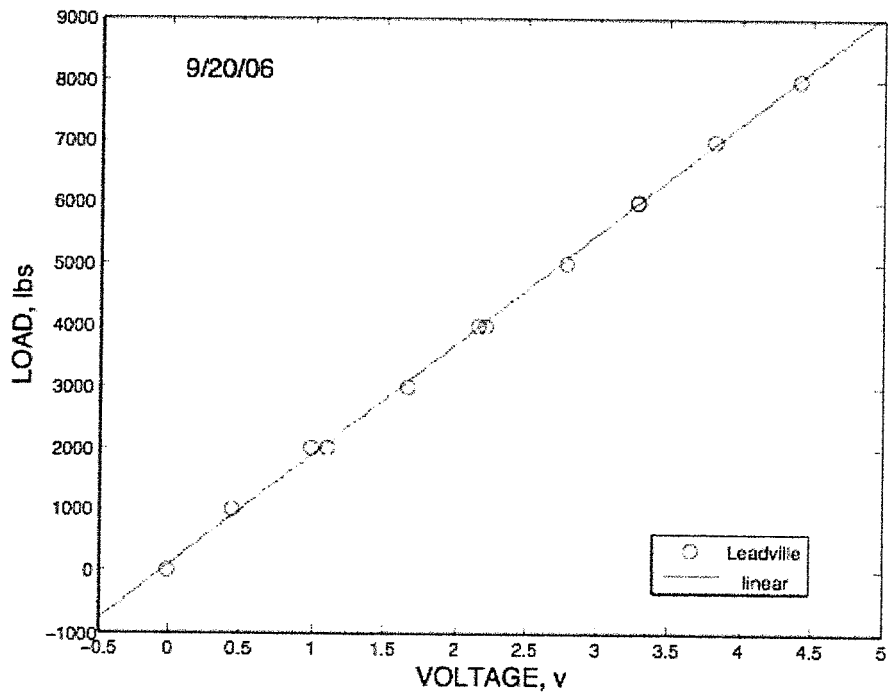


Figure 11: First Load Cell Calibration, Leadville, CO

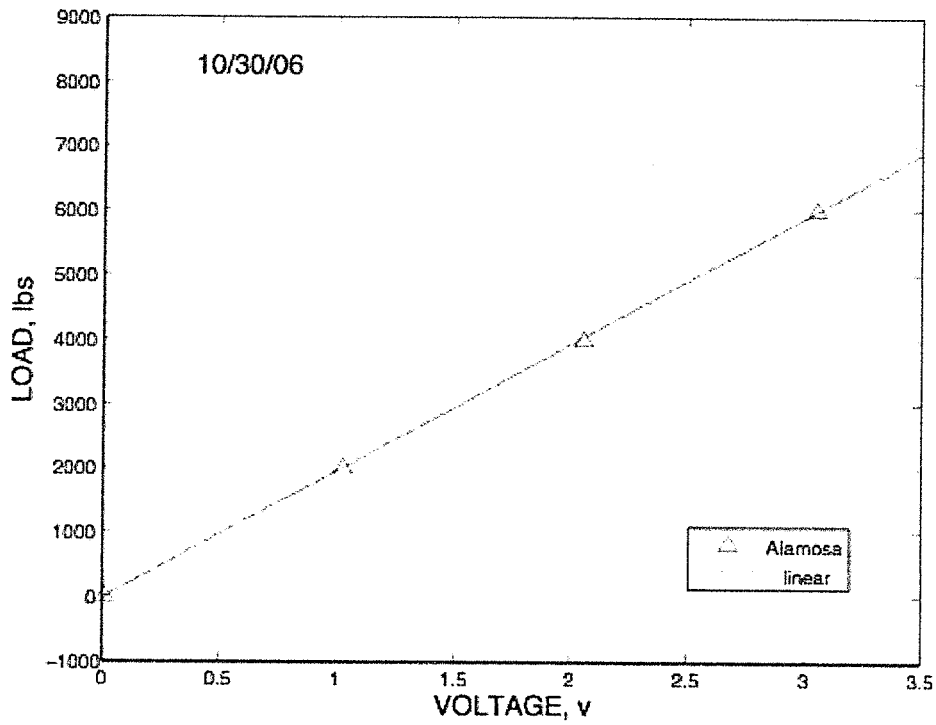


Figure 12: Second Load Cell Calibration, Alamosa, CO

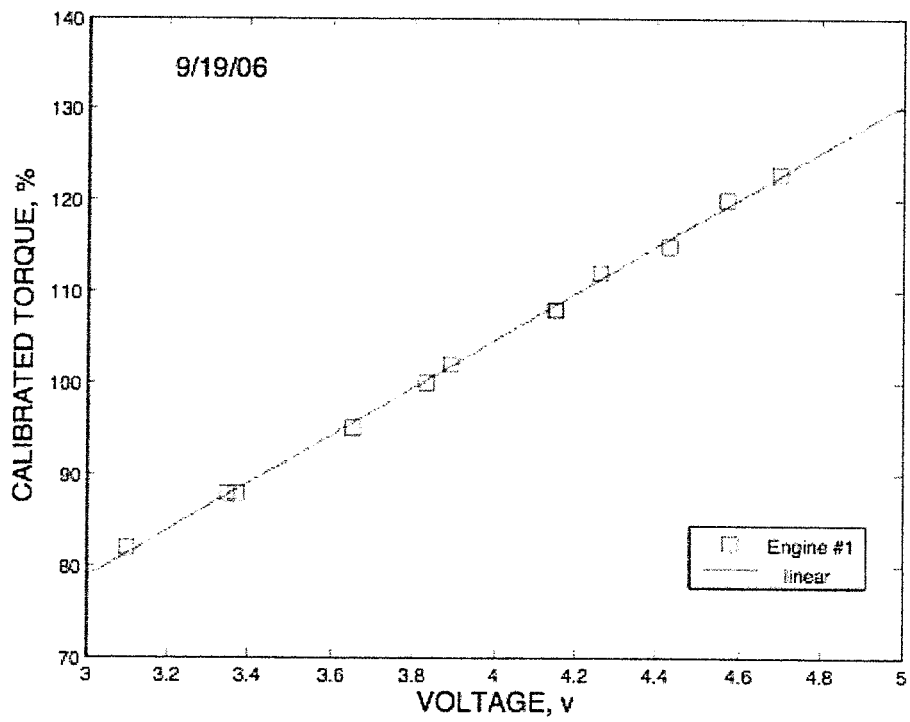


Figure 13: Engine #1 Torque Calibration

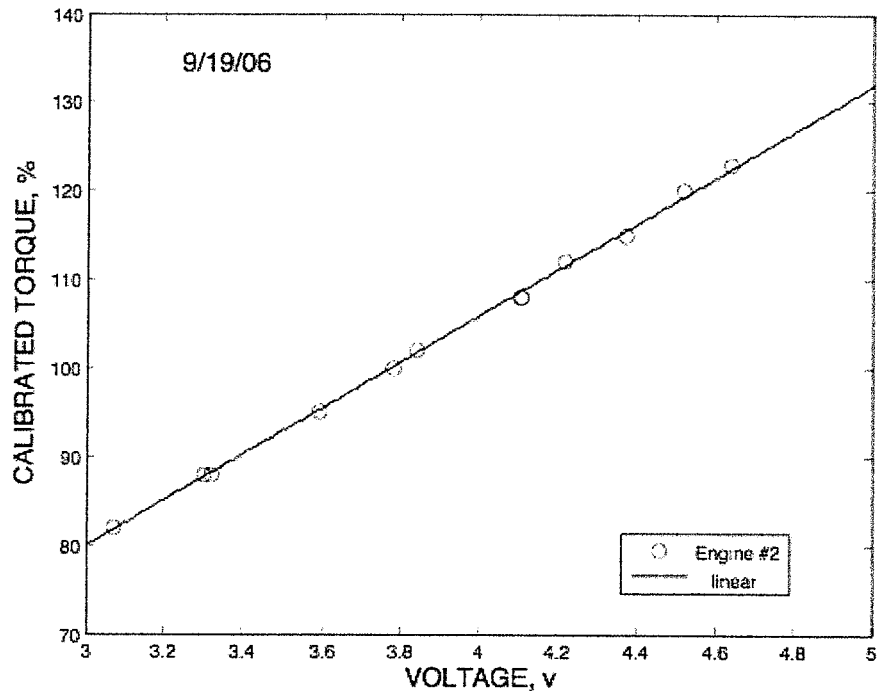


Figure 14: Engine #2 Torque Calibration.

Appendix A

Aircraft Components

This appendix identifies certain components installed in the two aircraft employed in flight tests described above.

N15456(C/N 61826)

Engines: CT58-140-1, no modifications

Engine accessories:

Anti Ice Valve: 4025T87P03

Accessory Gearbox: 5001T90G06

Start Bleed Valve: 4003T62P04

Exciter: 370400347P101, Flow Divider: 4003T68G04

Fuel Control: 725725-5

Fuel Pump: 5003T42P02

Centrifugal Filter: 4005T01P03

Oil Pump: 4000T98P02

Pilot Valve: 4920T00G05
Tachometer Generator Nf: 32005-007
Tachometer Generator Ng: TG255-002
Main Transmission: S6135-20600-039

Main Transmission accessories:
AC generator (2ea.): 28B135-145AM
DC Generator: 30E20-97A
Tachometer Generator: GEU7A
Primary Hydraulic Pump: 66WAP200-1
Auxiliary Hydraulic Pump: 66WAP200-2

Drive Line components:
Intermediate Gear Box: S6135-66300-002
Tail Gear Box: S6135-66600-043

No Major alterations on this aircraft

External configuration:
Engine Air Inlet Screens were installed (Bird Screens) S61N optional
S6130-80179-002 Engine air Inlet duct installed
Flown with both fixed landing gear and Sponsons
Long Fuselage Aircraft

Tail Rotor Blades: S6117-30101-045
Bifilar: S6112-23039-017
Pitch Beam: S6135-66705-1
Pylon Assembly: S6120-76265-1
Stabilizer Assembly: S6120-76150-71

N3173U (C/N 61186)

All components of this aircraft are the same as N15456 as listed above except as follows:

Intermediate Gear Box: S6135-66100-041
Pitch Beam: S6135-66705-041
Pylon Assembly: 61200-66001-42
Stabilizer Assembly: S6120-76150-76

Engine Air Inlet Screens were installed (Bird Screens)
Flown with fixed landing gear
Short Fuselage Aircraft

Appendix B

Pilot Cards, Weight and Balance Statements

The pilot cards and weight and balance statements are contained in this Appendix. Note that the listed values in the cards of average engine torque and load cell tether tension should serve only as guidelines. The true values of these quantities as determined by the calibrations in Appendix A and calculated as averages over the recording time by a computer were used to develop the CP-CW relationship for the aircraft charts.

FLT #1

ATTN: JERRY WASHCALUS.

ALL FILES ARE 8 SECONDS

Flight No 1891
 A/C N15455 CG _____ GW 13706 DATE 9.26.06
 Fwd Fuel 675 700 ACC Aft Fuel 650 700 ACC
 Location LEADVILLE OAT -2 PA 9480 9500 FlightTime 48 mins
 Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rory/Rud
 Aircraft Configuration SS1N Composite Blades Long Body Fixed Gear

Test Description 100 Foot Tethered Hover

Fuel

	Torque	Load Cell	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
wt	80	0	106	650	500	✓	4		1
	85	1250	106	625	575	✓	4	T P 90 60	2
	70	2000	106	600	560	✓	3	T P 100 60	3
	75	3250	106	600	550	✓	3	T P 100 60	4
	80	4000	106	575	550	✓	3	T P 100 60	5
b	85	4400	105.5	550	500	✓	3	T P 100 60	6
r	90	5600	105	550	500	✓	3	T P 100 60	7
v	75	6100	105	550	500	✓	3	T P 100 60	8
wt	60	0	106	550	500	✓	3	T P 100 60	9
wt	60	0	103	550	500	✓	3	T P 100 60	10
	65	1000	103	505	475	✓	3	T P 100 60	11
	70	1700	103	500	475	✓	+4	T P 105 60	12
	75	2750	103	500	475	✓	+4	T P 105 60	13
	80	3700	103	500	475	✓	4	T P 105 60	14
	85	4750	103	475	450	✓	4	105 60	15
	90	5800 5500	103	475	450	✓	4	105 60	16
	95	6500	103	475	450	✓	4	105 60	17
wt	60	0	103	450	400	✓	4	105 60	18
wt	60	0	100	450	400	✓	4	105 60	19
	65	1200	100	425	400	✓	4	105 60	20
	70	2000	100	425	375	✓	4	105 60	21

100ft tethered hover

Flight No 1 Pg 2

AC N15498 CG _____ GW 13706 DATE 9/25/06

Fwd Fuel 360 Aft Fuel 200

Location Lewisville OAT +4 PA 9500 FlightTime 48 mins

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rory / Rod

Aircraft Configuration S61N Composite Blades Long Body Fixed Gear

Test Description 100 Foot Tethered Hover

Fuel

Torque	Load Cell	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS TOP	EVENT
75	3000	100	425	350	✓	+3 9600	105 60	22
80	3900	100	415	350	✓	+3 9600		23
85	4700	100	415	350	✓	+3 9600		24
90	5200	100	400	350	✓	+3 9600	105 60	25
95	6400	100	400	350	✓	+3 9600		26
60	0	100	375	325	✓	+3 9600	105 60	27
50	0	100	375	300	✓	+3 9600	105 60	28
65	2800	105	350	300	✓	+3 9600	105 60	29
70	3100	105	350	300	✓	+3 9600	105 60	30
75	3700	105	325	300	✓	+3 9600	110 60	31
80	4900	105	325	300	✓	+3 9600	110 60	32
85	5600	105	325	275	✓	+3 9600	112 60	33
90	6500	105	300	275	✓	+3 9600	112 60	34
95	7000	105	300	250	✓	+3 9600	112 60	35
55	4100	105	300	250	✓	+3 9600	112 60	26
			200	200				

FLT #2

ATTN: Jerry

Flight No 2 p.1 17535
 A/C N16468 CG _____ GW 18515 DATE 9/28/06
 Fwd Fuel 675 1015 *Hee* Aft Fuel 675 1250 *Hee* start 726
end 918
 Location Leadville, Co OAT -3 PA 9450 FlightTime 1.8
 Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rory/Red
 Aircraft Configuration S51N Composite Blades Long Body Fixed Gear

Test Description 10 Foot Free Flight Hover

Fuel

Torque	WT Reduction	NR	FWD	AFT	W/O <3KTS	OAT/PA	TRNS TOP	EVENT
82		182	990	1250	2.2	-3	95/60	1
80		106	990	1250	2.2	-3	98/60	2
82		100	950	1225	2.2	-3 9450	100/60	3
79		106	950	1200	✓	-3 9450	102/60	4
83		103	925	1175	✓	-3 9450	100/60	5
84		100	900	1175	✓	-2 9450	110/60	6
77	400 #	106	900	1150	✓	-2 9450	100/60	7
80		103	900	1150	✓	-2 9440	100/60	8
80		100	875	1125	✓	-2 9440	101/60	9
77		106	875	1125	✓	-2 9440	110/60	10
77		103	850	1100	✓	-2 9440	112/60	11
80		100	825	1100	✓	+2 9440	112/60	12
74	400 #	106	800	1075	✓	+3 9440	112/60	13
75		103	800	1050	✓	+3 9440	115/60	14
77		100	800	1050	✓	+3 9440	115/60	15
73		106	775	1050	✓	+3 9440	115/58	16
75		103	775	1025	✓	+3 9440	115/58	17
76		100	750	1025	✓	+3 9440	115/58	18
70	400 #	106	750	1000	✓	+3 9440	105/60	19
71		103	725	975	✓	+3 9440	115/60	20
73		100	700	950	✓	+3 9440	105/60	21

18515

ATTN: Jerry

Flight No 2 pg 2

AC N18458

CG _____

GW 18515

DATE 9/28/06

Fwd Fuel _____

Aft Fuel _____

Location Leadville, Co

OAT _____

PA _____

FlightTime 1.8

Crew: Pilot Bob Boyd

Test pilot Charlie Evans

Computer Operator Eric/Ed

Aircraft Configuration _____

S91N

Composite Blades Long Body Fixed Gear

Test Description 10 Foot Free Flight Hover

Fuel

Torque	WT Reduction	NR	FWD	AFT	W@ <KTS	OAT/PA	TRNS TOP	EVENT
72		105%	700	950	✓	+3 9440	105/60	22
70		103	700	950	✓	+3 9440	105/60	23
72		100	575	950	✓	+3 9440	110/60	24
68	400 #	106	575	950	✓	+3 9440	105/60	25
67		103	550	925	✓	+3 9440	110/60	26
70		100%	550	925	✓	+3 9440	112/60	27
66		105	550	900	✓	+3 9440	110/60	28
68		103	550	900	✓ 1.0-1.5	+3 9440	110/60	29
69		100	550	900	✓	+3 9440	105/60	30
65	400 #	106	600	875	✓	+5 9440	105/60	31
65		103	600	875	✓	+5 9440	105/60	32
65		100	600	875	✓	+5 9440	105/60	33
64		106	575	875	✓ 1.0-1.5	+5 9440	105/60	34
66		103	575	850	✓	+5 9440	105/60	35
67		100	575	850	✓	+5 9440	105/60	36
62	400 #	106	550	850	✓	+5.5 9440	105/60	37
63		103	550	825	✓	+5.5 9440	105/60	38
63		100	550	825	✓ 1.5-2.0	+5.5 9440	105/60	39
61		106	525	800	✓	+5.5 9440	105/60	40
62		103	525	800	✓	+5.5 9440	105/60	41
64		100	525	800	✓	+5.5 9440	105/60	42

Flight No 2 Pg. 3

A/C N18498

CG _____

GW 18515

DATE 9/28/06

Fwd Fuel _____

Aft Fuel _____

Location Lendoille, Ca

OAT _____

PA _____

FlightTime 1.8

Crew: Pilot Bob Boyd

Test pilot Charlie Evans

Computer Operator Rory/RJ

Aircraft Configuration

S81H

Composites Blades Long Body Fixed Gear

Test Description 10 Foot Free Flight Hover

Fuel

Torque	WT Reduction	NR	FWD	AFT	W/O <KTS	OAT/PA	TRNS TOP	EVENT
59	400#	108%	500	750	✓	5.5 9440	110/60	43
60		103	500	750	✓	5.5 9440	111/60	44
62		100	500	750	✓	5.5 9440	111/60	45
58		106	500	725	1.5	5.5 9440	110/60	46
59		103	475	725	✓	5.5 9440	111/60	47
60		100%	475	725	✓	5.5 9440	110/60	48
50	400#	106	450	700	2.5-3.0	6 9440	110/60	49
57		103	450	675	CALM	6 9440	110/60	50
58		100	425	675	✓	6 9440	110/60	51
57		106	425	675	✓	6 9440	110/60	52
57		103	425	675	✓ 5?	6 9440	110/60	53
57		100	400	650	✓	6 9440	110/60	54
53	550#	106%	400	650	✓	6 9440	110/60	55
53		103	375	650	3.5	6 9440	110/60	56
54		100	375	650	✓	6.5 9440	110/60	57
53		106	350	625	2.5-3.0	6.5 9440	112/60	58
54		103	350	625	✓	6.5 9440	112/60	59
55		100%	350	600	20-4.0	6.5 9440	112/60	60

End Fuel ^{Fwd} 350 ^{Aft} 600 924 AM

Flight No 2 Page 1 of 2

AC N16458 CG _____ GW 20507 DATE 10-25-06

Gross Weight includes this fuel Fwd Fuel 640 Aft Fuel 1260

Location Alamosa, CO. OAT 2° PA 7480 FlightTime _____

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Red/Bred

Aircraft Configuration SR1N Composite Blades Long Body Fixed Gear

Test Description 10 Foot Free Flight Hover

Fuel Remaining

Torque	WT Reduction	NR	FWD	AFT	WG <3KTS	OAT/PA	TRNS TOP	EVENT
90		106	620	1240			90°/60	1
91		103	600	1200				2
93		100	590	1190				3
87	400	106	580	1170	<1	2/7480	92°/60	4
88		103	560	1160				5
90		100	550	1150				6
82	400	106	530	1120	<3		94°/60	7
85		103	520	1120				8
87		100	510	1110				9
80	400	106	500	1100	<2		96°/65	10
81		103	480	1090				11
84		100	460	1070				12
77	400	106	460	1060	3	2/7480		13
80		103	450	1050				14
82		100	450	1040				15
75	400	106	430	1030	4	3/7480		16
76		103	420	1020	<3			17
77		100	420	1020				18
72	400	106	400	1000				19
74		103	380	980	2			20
76		100	370	970				21

FLT 2 10 FT hover

N15458	WEIGHT	ARM	MOMENT
N15458 ALS CO	11420	264.29	3018191.8
PILOT	230	88.8	20378
TEST PILOT	204	88.8	18074.4
FLIGHT LOG PERSON	175	128.5	22487.5
COMPUTER OPERATOR	285	201	57285
FWD FUEL	640	203.9	130496
AFT FUEL	1260	305.9	385434
STA 128.5		128.5	0
Net-Tie down straps floor mat	131	203.9	26710.9
BALLAST (30in) 2.5ft x 6ft f3000	700	203.9	142730
Net-Tie down straps floor mat	131	266	34846
BALLAST (42in) 3.5ft x 6ft f4200	4150	266	1103900
Net-Tie down straps floor mat	131	305.9	40072.9
BALLAST (30in) 2.5ft x 6ft f3000	1050	305.9	321195
Net-Tie down straps floor mat		440	0
BALLAST C18 aft cg		440	0
A/C TOTAL WEIGHT	20507	259.5114585	5321801.5
		700/25=28	
CG=258		1050/25=42	
		4150/25=166	

ATTN GERRY 1047

Flight No 6

A/C N15456 CG _____ GW 13714 DATE 11/1/06

Gross Weight Includes this fuel Fwd Fuel 700 Aft Fuel 700 Start - 7:35

Location Alamosa, CO OAT -3 PA 7300 End - 8:00
Total Flight Time 1.1

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rod / Brad

Aircraft Configuration S81N Composite Blades Long Body Fixed Gear

Test Description 100 Foot Tethered Hover

Fuel

	Torque	Load Cell	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS TOP	EVENT
SLP	60	150	106	650	650	0	-2/7400	85/65	1
	65	1030	106	640	640	0	-2/7400		2
	70	1720	106	630	630	0	-2/7400		3
	75	2630	106	630	620	0	-2/7400		4
	80	3530	106	620	610	0	-2/7400		5
	85	4100	106	620	610	0	-2/7400	90/60	6
	90	5250	106	610	600	0	-2/7400		7
	95	5650	106	600	590	0	-2/7400		8
	100	---	106	No	Good	0	-2/7400	95/55	9
	100	6620	106	580	560	0	-2/7400		10
SLP	57	150	103	570	550	0	-2/7400		11
	65	1220	103	560	540	2-3	-2/7400		12
	70	2450	103	560	530	2-3	-1/7400	95/55	12
	75	3050	103	550	530	0	-1/7400		14
	80	3970	103	540	520	0	-1/7400		15
	85	4800	103	540	510	0	-1/7400		16
	90	5240	103	530	510	0	-1/7400		17
	95	5900	103	520	500	0	-1/7400	98/50	18
	100	6740	103	510	490	0	-1/7400		19
SLP	60	150	100	500	480	0	-1/7400		20

Flight No 6

A/C N15456 CG _____ GW 14314 DATE 11/11/06

Gross Weight includes this fuel Fwd Fuel 1000 Aft Fuel 1000

9:56
10:50

Location Casa Grande, AZ OAT 18 PA 1400 FlightTime .9

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rad/Brad

Aircraft Configuration S61N Composite Blades Long Body Fixed Gear

Test Description 100 Foot Tethered Hover

Fuel

	Torque	Load Cell	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
0									
SLP	60	12	106	980	950	1-2	19/1500	98/50	1
	65	142	106	930	900	1-2	19/1500	100/50	2
	70	222	106	920	900		19/1500	100/50	3
	75	330	106	920	890		19/1500	100/50	4
GP	80	407	106	910	880		19/1500	100/50	5
GP	85	525	106	900	870		19/1500	100/50	6
GP	90	570	106	890	860		19/1500	100/48	7
GP	95	670	106	880	860		19/1500	100/48	8
GP	100	730	106	870	850		19/1500	100/48	9
GP	103	798	106	860	840		19/1500	102/45	10
SLP	61	15	103	860	840		19/1500	102/45	11
	65	60	103	850	830		19/1500	102/45	12
	70	184	103	845	825		19/1500	102/45	13
	75	284	103	840	820		19/1500	102/44	14
	80	360	103	835	815		19/1500	102/44	15
GP	85	446	103	830	810		19/1500	102/43	16
GP	90	538	103	825	805		19/1500	102/42	17
	95	620	103	820	800	↓	19/1500	102/42	18
GP	100	662	103	815	795	1-2	19/1500	102/42	19
GP	103	740	103	810	790	1-2	19/1500	102/42	20

Flight No 6

AC N15456 CG _____ GW 14314 DATE 11/11/06

Gross Weight includes this fuel Fwd Fuel 1000 Aft Fuel 1000

Location Casa Grande, AZ OAT 18 PA 1400 FlightTime _____

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rod/Brad

Aircraft Configuration S61N Composite Blades Long Body Fixed Gear

Test Description 100 Foot Tethered Hover

Fuel

	Torque	Load Cell	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
SLP	60	14	106	720	690	2	20/1540	108/42	31
GP	65	134	106	715	685		20/1540	108/42	32
	70	310	106	710	680		20/1540	108/42	33
	75	395	106	710	670		20/1540	108/42	34
	80	450	106	705	660		20/1540	108/42	35
GP	85	565	106	700	650		20/1540	108/42	36
	90	584	106	695	645		20/1540	108/42	37
	95	680	106	690	640		20/1540	108/42	38
	100	808	106	685	635	↓	20/1540	108/42	39
	103	800	106	680	630	1-2	20/1540	108/42	40
LP	58	14	103	670	620	1-2	20/1540	108/42	41
	65	154	103	660	610		20/1540	108/42	42
	70	248	103	650	600		20/1540	108/42	43
	75	360	103	645	595		20/1540	109/40	44
GP	80	438	103	640	590		20/1540	109/40	45
	85	520	103	635	580		20/1540	109/40	46
	90	628	103	630	570		20/1540	109/40	47
IP	95	748	103	620	560		20/1540	109/40	48
	100	770	103	610	550		21/1550	109/40	49
	103	751	103	600	540	↓	21/1550	109/40	50
							21/1550	109/40	

Flight No 07 ~~07~~ Page 1 of 2A/C N12456 CG _____ GW 20407 DATE 18 JAN 07Gross Weight includes this fuel Fwd Fuel 900 Aft Fuel 900 8:02
8:44Location Casa Grande OAT 1 PA 1500 FlightTime .7Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rad/BradAircraft Configuration S61N Composite Blades Long Body Fixed GearTest Description 10 Foot Free Flight Hover

Fuel Remaining

Torque	WT Reduction	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
82		106	850	840	calm	1	90/55	1
84		103	840	830		1	90/55	2
85		100	830	820		1	90/55	3
80	400	106	810	800		1	90/50	4
82		103	800	790		1	95/50	5
83		100	790	780	calm	1	95/50	6
84		100	780	770		1	95/50	7
78	400	106	770	760		1	95/50	8
78		103	760	750		1	95/50	9
80		100	750	740		1	95/50	10
77		106	740	730		1	95/50	11
73	400	106	720	710	calm	2	95/50	12
75		103	715	705		2	95/50	13
77		100	710	700		2	95/50	14
71	400	106	700	690		2	95/50	15
73		103	695	685		2	95/50	16
74		100	690	680		2	95/55	17
71	400	106	680	660		2	95/55	18
72		103	670	655		2	95/55	19
73		100	660	650	calm	2	95/55	20
							/	BE

2045

Flight No 07 Page 2 of 2

A/C N18458 CG _____ GW 20407 DATE 18 JAN 07

Gross Weight includes this fuel Fwd Fuel 900 Aft Fuel 900

Location Casa Grande OAT 1 PA 1500 FlightTime .7

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Rod/Brad

Aircraft Configuration 861N Composite Blades Long Body Fixed Gear

Test Description 10 Foot Free Flight Hover

Fuel Remaining

Torque	WT Reduction	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
66	400	106	650	640	calm	2	95/55	21
67		103	645	630		2	95/55	22
68		100	640	620		2	95/55	23
66	400	106	630	610		2	95/50	24
66		103	620	600		2	95/50	25
68		100	610	590		2	95/50	26
64	400	106	600	580		2	95/50	27
65		103	595	575	calm	2	95/50	28
65		100	590	570		2	95/50	29
61	400	106	580	550		2	95/50	30
63		103	575	545		2	96/50	31
65		100	570	540		2	96/50	32
59	400	106	560	530		2	96/50	33
60		103	550	520		2	97/50	34
61		100	545	510	calm	2	97/50	35

30/5

Flight No 08 PAGE 1 OF 2

A/C N15456 CG _____ GW 22321 DATE 18 JAN 07

Gross Weight includes this fuel Fwd Fuel 1200 Aft Fuel 1200

Location Casa Grande OAT 7 PA 1500 FlightTime 1.0

10:22
11:20

Crew: Pilot Bob Boyd Test pilot Charlie Evans Computer Operator Red/Brad

Aircraft Configuration S61N Composite Blades Long Body Fixed Gear

Test Description 10 Foot Hover - External Load Combination

Fuel Remaining

Torque	WT Reduction	NR	FWD	AFT	W@ <3KTS	OAT/PA	TRNS T@P	EVENT
101	LEFT 10 KTS	106	1150	1150	1-2	7	100/50	1
99	RIGHT 10 KTS	106	1140	1140	1-2	7	100/50	2
101	REAR 5 KTS	106	1130	1130		7	100/45	3
93		106	1120	1110		8	100/45	4
93		103	1115	1105		8	100/45	5
96		100	1110	1100		8	100/45	6
89	400	106	1060	1050		8	100/45	7
91		103	1050	1040		8	110/45	8
91		100	1040	1030		8	110/45	9
87	400	106	1000	980		9	110/45	10
89		103	990	970		9	110/45	11
90		100	980	960		9	110/45	12
83	400	106	950	930	↓	10	110/45	13
85		103	940	920	2-3	10	110/45	14
87		100	930	910		10	110/45	15
82	400	106	910	890		10	110/45	16
84		103	900	880		10	110/45	17
85		100	890	870		10	110/45	18
81	400	106	870	850		11	110/45	19
82		103	860	840		11	110/45	20
83		100	850	830	↓	11	110/45	21

* Events 1, 2, 3 are controllability.

30/5

FL 08 Casa Grande 18 JAN 07

N15456 MID CG	WEIGHT	ARM	MOMENT
N15456	11420	264.29	3018191.8
PILOT	230	88.6	20378
TEST PILOT	204	88.6	18074.4
FLIGHT LOG PERSON	175	128.5	22487.5
COMPUTER OPERATOR	285	201	57285
FWD FUEL	1200	203.9	244680
AFT FUEL	1200	305.9	367080
EXTERNAL LOAD	2020	267	539340
Net-Tie down straps floor mat		203.9	0
BALLAST (30in) 2.5ft x 6ft		203.9	0
Net-Tie down straps floor mat	131	266	34846
BALLAST (42in) 3.5ft x 6ft	3300	266	877800
Net-Tie down straps floor mat	131	305.9	40072.9
BALLAST (30in) 2.5ft x 6ft	2025	305.9	619447.5
A/C TOTAL WEIGHT	22321	262.5188432	5859683.1
		3300/25=132	
		2025/25=81	

FL 08 CASA Grande, AZ 18 JAN 07

Controllability + IGE ~~22321~~ 22321

50/5