

NATIONAL TRANSPORTATION SAFETY BOARD

Office of Research and Engineering
Washington, D.C. 20594

May 1, 2015

CXO Runway 1 Examination Test Plan

by John O'Callaghan

A. ACCIDENT

Location: Conroe, TX (Lone Star Executive Airport (CXO))
Date: September 19, 2014
Time: 08:47 Central Daylight Time (CDT)
(13:47 Universal Coordinated Time (UTC))¹
Aircraft: Embraer EMB-505, N322QS
NTSB#: CEN14FA505

B. PARTICIPANTS

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Craig Hatch
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4760 Oakland Street, Suite 500
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CXO Airport: Scott Smith
Airport Manager
Lone Star Executive Airport
10260 Carl Pickering Memorial Dr., Conroe, TX 77303

¹ Local time at Conroe on the day of the accident was Central Daylight Time (CDT). CDT = UTC - 5 hours. Times in this *Test Plan* are in CDT unless otherwise noted.

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C. HISTORY OF FLIGHT

On September 19, 2014, about 08:47 central daylight time, an Embraer EMB-505 airplane, N322QS, encountered soft terrain and mud after over running the runway while landing at the Lone Star Executive Airport (CXO), Conroe, Texas. Neither of the airline transport rated pilots on board were injured. The airplane was substantially damaged. The airplane was operated by Net Jets as a 14 Code of Federal Regulations Part 91 positioning flight. Instrument meteorological conditions prevailed for the flight, which was operated on an instrument flight rules flight plan. The flight originated from the Nashville International Airport (BNA), Nashville, Tennessee, at 07:10.

According to the air traffic controller who witnessed the accident, the pilots flew the area navigation (RNAV) runway 1 approach and broke out of the clouds at the minimums for the approach. The controller stated the airplane touched down just past the 1,000 foot marker on the runway and did not appear to decelerate as it continued down the runway. The airplane traveled off the departure end of the runway and continued about 400 feet through soft/muddy terrain before coming to rest half way down a ditch. The controller stated there was moderate to heavy rain at the time of the accident.

The role of the Aircraft Performance Specialist in the investigation is to determine and analyze the motion of the airplane and the physical forces that produce that motion. In particular, the Specialist attempts to define the airplane's position and orientation during the relevant portion of the flight, and determine the airplane's response to control inputs, external disturbances, ground forces, and other factors that could affect its trajectory.

The data used to determine and analyze the airplane motion includes but is not limited to the following:

- Wreckage location and condition.
- Ground scars / markings.
- Airport Surveillance Radar (ASR) data.
- Flight Data Recorder (FDR) data.
- Cockpit Voice Recorder (CVR) information.
- Runway macrotexture, cross-slope, and friction measurement information.
- Weather information.
- Airplane thrust and aerodynamic performance information.
- Output from computer programs and simulations that calculate aircraft performance.

This *Test Plan* describes the objectives of and methods for an examination of runway 1 at CXO, including the data to be gathered, the equipment required, and the test procedures.

D. DETAILS OF THE TEST

I. Test Objectives

The objectives of the test are to:

1. Measure the runway 1 macrotexture depth at 40 locations, as defined below.
2. Measure the runway 1 cross-slope at those same 40 locations.
3. Measure the runway friction along the length of runway 1 using the NAC DFT trailer provided and operated by IAH personnel, at 4 different speeds and at 4 different distances from the runway centerline, as defined below.
4. Use the measured DFT data to compute the wet runway braking coefficient as a function of ground speed for the EMB-505 airplane, using a method developed by NASA Langley (see Appendix B).
5. Use the measured macrotexture and cross-slope data to compute the expected water depth on the runway as a function of rainfall rate, per a drainage model developed by the Texas Transportation Institute (TTI).²
6. Examine the runway 1 edges for vegetation or other obstructions that would prevent proper water drainage from the runway.

II. Test Location and Date

The test is scheduled for Tuesday, May 5, 2015, on runway 1 at CXO. The street address of CXO is:

Lone Star Executive Airport
10260 Carl Pickering Memorial Dr., Conroe, TX 77303

² B. Gallaway, R. Schiller, Jr., and J. Rose, *The Effects of Rainfall Intensity, Pavement Cross Slope, Surface Texture, and Drainage Length on Pavement Water Depths*. Texas Transportation Institute (TTI) Research Report 138-5, May 1971.

The test team should meet at the CXO airport offices at 8:00 CDT to brief the test plan for the day.

If weather forecasts preclude testing on that day, the test will be postponed.

III. Test Equipment

- Geo7x survey GPS
- Measuring wheel for measuring off runway distances
- 250 ft. tape measure
- Chalk
- Level (3 ft. or 6 ft.)
- Digital inclinometer
- ELAtextur macrotexture scanner
- Newbert Aero Corporation Dynamic Friction Tester (NAC DFT) Continuous Friction Measurement Equipment (CFME) trailer and truck
- Data log – macrotexture and cross slope measurements
- Run matrix and log – NAC DFT measurements
- Video / still camera (e.g., iPhone)

IV. Safety Equipment

- VHF radio for ATC Tower communications, for each of two teams (described below), operated by CXO personnel
- Visibility vest
- Whistle for signaling personnel on the runway

V. Test Teams

The tests will be conducted by two teams, working independently:

- The “DFT team”: operates the DFT CFME truck and trailer.
- The “Macrotexture” team: conducts the macrotexture and cross-slope measurements at discrete points on the runway; examines runway edge.

For simplicity and safety reasons, only one team will be working on the runway at a time. The DFT team will do its work first, so as to release the DFT vehicle as soon as possible. The sequence of runs and test points for each team is prioritized as shown in Appendix C.

VI. Runway 1-19 closure and coordination with the ATC Tower

Runway 1-19 will be NOTAM'd "closed" prior to the test, and will remain closed during the duration of the test. The CXO person assigned to each test team will monitor the VHF radio and communicate as required with the ATC tower and the other team, and advise when the team should clear runway 1 and / or remain clear of the 250 ft. safety zone on either side of the centerline of intersecting runway 14-32.³ Any presence of the teams inside the safety zone must be coordinated with the ATC tower through the CXO team member.

While the Macrotecture team is on the runway, the CXO team member will be in possession of a whistle. If this person determines that the team must clear the runway immediately, he will blow three blasts on the whistle. Upon hearing the whistle, team members will exit the runway immediately. If he blows one long blast, the team will assemble at his location.

VII. Test Procedure: NAC DFT friction runs

1. Set up the DFT per IAH's normal operating procedures / checklists.
2. Measure and record the friction tire's inflation pressure at the start of the day, at water refills, and at the end of the day. Adjust inflation pressure as necessary to maintain a constant value throughout the tests.
3. Conduct friction test runs in one direction only: starting from the threshold of runway 1, and testing towards the threshold of runway 19. Drive back to the runway 1 threshold to start a new run.
4. Conduct runs at the matrix of speeds and runway "y" coordinates shown in the "CFME runs" sheet of the "KXCO_RWY1_measurements.xls" *Excel* spreadsheet. Number the runs consecutively, and note the run number in the appropriate cell of the matrix. Note the time of the start of the run, and any other identifying information, in the "Run Log" section of the spreadsheet, so that the data recorded by the DFT can be associated with the correct run number later.

The "PLANNED" matrix shows the suggested order of runs, sequenced so as to obtain the high-priority runs first. Note that runs 13, 14, 19, & 20 are repeat runs. Log the actual conduct of the runs in the "ACTUAL" matrix.

The runway coordinates originate at the threshold of runway 1 on the centerline. The +x coordinate runs down the runway towards the threshold of runway 19. The +y coordinate runs towards the right edge of the runway. Note that the test y coordinates are not centered about the centerline, but are biased toward the left side of the runway. This is to reflect the actual track of N322QS as evidenced by the skid marks left by the airplane.

Set up the Geo7x to record a "generic line" feature during each run, logging GPS coordinates at regular time intervals. These coordinates can then be later used to compare the actual track of the DFT to the planned track.

³ Runway 14-32 intersects runway 1-19 about 4170 ft. from the runway 1 threshold (see diagram in Appendix A).

In addition to the driver, the DFT tow vehicle can accommodate 4 observers. One of these should be the CXO team member to handle communications with the tower. A second, at least, should be present to take notes and fill out the run log.

VIII. Test Procedure: Macrotexture and cross-slope measurements

1. In advance of the test, create waypoints in the Geo7x device locating the x runway coordinate of measurement points, as shown in the “Macrotexture” sheet of the “KXCO_RWY1_measurements.xls” *Excel* spreadsheet.
2. Navigate to the measurement x coordinate using the Geo7x, and double-check with measuring wheel. Then, use the tape measure to find the correct y coordinates (see Appendix D). Note that the test y coordinates are not centered about the centerline, but are biased toward the left side of the runway. This is to reflect the actual track of N322QS as evidenced by the skid marks left by the airplane.
3. Mark and label the measurement point with chalk. See the spreadsheet for the point names (the names are constructed from the x and y coordinates of the point).
4. Using the ELAtextur scanner, measure the macrotexture three times, on and around the marked point. Record all three measurements in the appropriate cells in the spreadsheet. (Note the gray cells in the spreadsheets are for calculations that will be performed after the data is collected).
5. Using the level and digital inclinometer, measure and record the runway cross slope in the spreadsheet. Positive slope is for the centerline higher than the runway edge. Negative slope is for the centerline lower than the runway edge.
6. Photograph both the left and right runway edges to document vegetation or other obstructions that might cause runway drainage problems.
7. Repeat until all 40 points have been measured and recorded. See Appendix D for the suggested order of x-runway coordinate stations to test, so as to maximize coverage of the runway in the minimum amount of time (in the case that testing gets interrupted).
8. If the CXO team member determines that the team should clear the runway, he will blow 3 short blasts on the whistle. Upon hearing the whistle, the team will immediately clear the runway. If he blows one long blast, the team will assemble at his location.

IX. Other information

Appendix A contains an airport diagram and other useful information for CXO.

Appendix B contains the NASA Langley method for relating CFME measurements to airplane braking coefficients on a wet runway.

Appendix C contains printouts of the “Macrotexture” and “CFME runs” sheets in the “KXCO_RWY1_measurements.xls” *Excel* spreadsheet.

Appendix D contains details of proposed procedures for locating the measurement points on the runway.

Appendix A: KCXO Airport Diagram and Other Information

AIRPORT DIAGRAM

HOUSTON/LONE STAR EXECUTIVE (CXX)

AL-5573 (FAA)

HOUSTON, TEXAS

ATIS
118.325
LONE STAR TOWER ★
124.125
GND CON
120.45
CLNC DEL
120.45
119.55 (When Tower Closed)

D

COMPASS
ROSE

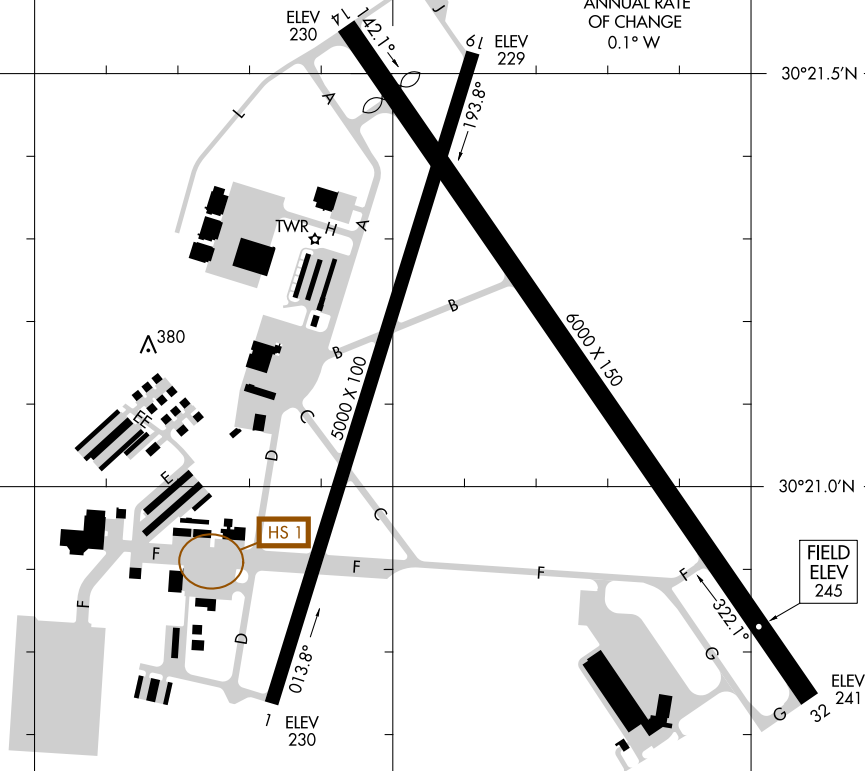
JANUARY 2010
ANNUAL RATE
OF CHANGE
0.1° W

30°21.5'N

30°21.0'N

30°20.5'N

SC-5, 13 NOV 2014 to 11 DEC 2014



CAUTION: BE ALERT TO RUNWAY CROSSING CLEARANCES.
READBACK OF ALL RUNWAY HOLDING INSTRUCTIONS IS REQUIRED.

AIRPORT DIAGRAM

Airport Details for KCXO - ACTIVE
Chart Date: 09/23/2010
LONE STAR EXECUTIVE
HOUSTON
AL #: 5573

State:	TEXAS	Magnetic Variation/Year:	E05/2000	Weather Station:	YES
Country:	United States	Site Nbr:	24072.1	Control Tower:	NO
Category:	AERODROME ONLY	Data Source:	405 NGS		
FAR Part 139:	NO	Owner:	NTL	Use:	CIVIL
				Military Type:	
Coordinates		Office		Local Auto Weather	
Latitude:	N 30° 21' 08.5000"	Flight Inspection:	OKC	Weather Source:	ASOS
Longitude:	W 095° 24' 52.3000"	Procedure Development:	120	Type:	3
Field Elevation:	244.9	Region Code:	SW	Frequency:	
Ellipsoid Elevation:	154.5 E	Service Area:	CNTL	Service A:	N
Horizontal Datum:	NAD83	OCC Code:	MID		
Vertical Datum:	NAVD88	International:	NO		

CONTACTS

ALTIMETERS

Type	Primary	Airport ID	Field Alt Source	Latitude	Longitude	Operational Timing
L	YES	KCXO	ASOS	N 30° 21' 08.5000"	W 095° 24' 52.3000"	FULL-TIME
R	NO	KDWH	ASOS	N 30° 03' 42.6000"	W 095° 33' 10.0000"	FULL-TIME

ALTIMETER COMMENTS

RUNWAYS

01 (A) 19 (A) 01 (P) 19 (P) 14 (A) 32 (A) 14 (P) 32 (P)

RUNWAY DETAIL

Landing Strip					
Chart Date: 02/06/2014			Publication Status: A		Pseudo Rwy:
Surface: ASPH GOOD			Width: 99		Physical Length: 5000
Rwy Number: 01		Rwy Number: 19		Rwy Number: 01	
Use Category: RUNWAY ONLY		Use Category: RUNWAY ONLY		Use Category: RUNWAY ONLY	
Chart Date: 09/20/2012		Chart Date: 09/20/2012		Chart Date: 09/20/2012	
Data Source: 405 03/03/2009 NGS		Data Source: 405 03/03/2009 NGS		Data Source: 405 03/03/2009 NGS	
Markings: NPI-G		Markings: NPI-G		Markings: NPI-G	
Threshold		Threshold		Threshold	
Latitude: N 30° 20' 44.2700"		Latitude: N 30° 21' 31.5500"		Latitude: N 30° 21' 24.2900"	
Longitude: W 095° 25' 10.1600"		Longitude: W 095° 24' 53.3100"		Longitude: W 095° 24' 55.8500"	
Elevation: 229.6		Elevation: 228.8		Elevation: 237.4	
Ellipsoid Elev: 139.3 S		Ellipsoid Elev: 138.5 E		Ref Pt Elev: 763	
Ellipsoid Elev Model: WGS84		Ellipsoid Elev Model: WGS84		Height Group:	
Horz. Datum: NAD83		Horz. Datum: NAD83		Lights	
Vert. Datum: NAVD88		Vert. Datum: NAVD88		Config Len Owner Mil Type Com Dt Pilot Cntrl	
Displaced Threshold		Displaced Threshold		MIRL STATE	
Latitude:		Latitude:			
Longitude:		Longitude:			
Elevation:		Elevation:			
Ellipsoid Elev:		Ellipsoid Elev:			
Ellipsoid Elev Model:		Ellipsoid Elev Model:			
Horz. Datum:		Horz. Datum:			
Vert. Datum:		Vert. Datum:			
Landing Length: 5000		Landing Length: 5000			
FI RWY Length: 5000		FI RWY Length: 5000			
FI RWY Height: 228.8		FI RWY Height: 229.6			
Tdz Elevation: 236.6		Tdz Elevation: 236.6			
True Bearing: 17.17		True Bearing: 197.18			
Ft Disp Th:		Ft Disp Th:			
Gradient: 0.0%		Gradient: 0.0%			
RVRTouchdown:		RVRTouchdown:			
MidPoint:		MidPoint:			
Rollout:		Rollout:			
Rail: NO		Rail: NO			
OIS Data Source: ANALPV 03/03/2009 NGS_SURVEY		OIS Data Source: ANALPV 03/03/2009 NGS_SURVEY			
Assoc. Fac.:		Assoc. Fac.:			

RUNWAY LANDING STRIP COMMENTS

VGSI Lights					
VGSI Lights Type:	PAPI-2L				
Owner:	STATE				
Pilot Cntl Freq:					
Th Cross Ht:	31.0				
High Angle:					
Com. Date:					
Com. Angle:	3.00				
DWB Elev:					
DWB Thres:					
Ref Pt Lat:					
Ref Pt Long:					
Ref Pt Elev:					
Ref Pt Thres:					
Height Group:					
Lights					
Config	Len	Owner	Mil Type	Com Dt	Pilot Cntrl
MALSR		STATE			122.950
MIRL		STATE			122.950

Lights						
Config	Len	Owner	Mil	Type	Com Dt	Pilot Cntrl
MIRL		STATE				122.950
REIL		STATE				122.950

Displaced Threshold	
Latitude:	N 30° 21' 28.6715"
Longitude:	W 095° 25' 00.0957"
Elevation:	230.6
Ellipsoid Elev:	140.4 S
Ellipsoid Elev Model:	WGS84
Horz. Datum:	NAD83
Vert. Datum:	NAVD88

Landing Length: 5411
FI RWY Length: 5411
FI RWY Height: 241.3
Tdz Elevation: 242.8
True Bearing: 145.48
Ft Disp Th: 589
Gradient: 0.2%
RVRTouchdown:
MidPoint:
Rollout:
Rail: YES
OIS Data Source: PIR 03/01/1991 NGS_SURVEY
Assoc. Fac.: CXO ILS (A)

Displaced Threshold	
Latitude:	
Longitude:	
Elevation:	
Ellipsoid Elev:	
Ellipsoid Elev Model:	
Horz. Datum:	
Vert. Datum:	

Landing Length: 6000
FI RWY Length: 5411
FI RWY Height: 230.6
Tdz Elevation: 244.9
True Bearing: 325.49
Ft Disp Th:
Gradient: -0.2%
RVRTouchdown:
MidPoint:
Rollout:
Rail: NO
OIS Data Source: ANALPV 03/03/2009 NGS_SURVEY
Assoc. Fac.:

RUNWAY LANDING STRIP COMMENTS

RUNWAY 14 COMMENTS

RUNWAY 32 COMMENTS

RUNWAY DETAIL

Landing Strip		
Chart Date: 03/05/2015	Publication Status: P	Pseudo Rwy:
Surface: CONC GOOD	Width: 150	Physical Length: 7501

Rwy Number: 14

Use Category: RUNWAY ONLY
Chart Date: 03/05/2015 Pub. Status: P
Data Source: THIRD_PARTY 06/26/2011
Markings: PIR-G

Threshold	
Latitude:	N 30° 21' 45.7165"
Longitude:	W 095° 25' 13.6157"
Elevation:	234.1
Ellipsoid Elev:	143.8 S
Ellipsoid Elev Model:	NAVD88
Horz. Datum:	NAD83
Vert. Datum:	NAVD88

Displaced Threshold	
Latitude:	
Longitude:	
Elevation:	
Ellipsoid Elev:	
Ellipsoid Elev Model:	NAVD88
Horz. Datum:	NAD83
Vert. Datum:	NAVD88

Landing Length: 7501
FI RWY Length: 7501
FI RWY Height: 241.3
Tdz Elevation: 242.9
True Bearing: 145.48
Ft Disp Th:
Gradient: 0.1%
RVRTouchdown:

Rwy Number: 32

Use Category: RUNWAY ONLY
Chart Date: 03/05/2015 Pub. Status: P
Data Source: THIRD_PARTY 06/26/2011
Markings: NPI-G

Threshold	
Latitude:	N 30° 20' 44.5408"
Longitude:	W 095° 24' 25.1015"
Elevation:	241.3
Ellipsoid Elev:	151.0 S
Ellipsoid Elev Model:	NAVD88
Horz. Datum:	NAD83
Vert. Datum:	NAVD88

Displaced Threshold	
Latitude:	
Longitude:	
Elevation:	
Ellipsoid Elev:	
Ellipsoid Elev Model:	
Horz. Datum:	UNKNOWN
Vert. Datum:	UNKNOWN

Landing Length: 7501
FI RWY Length: 7501
FI RWY Height: 234.1
Tdz Elevation: 245.0
True Bearing: 325.48
Ft Disp Th:
Gradient: -0.1%
RVRTouchdown:

Rpt Date:	20:00:36 08/15/2014		
Rpt User:	dso		
MidPoint:		MidPoint:	
Rollout:		Rollout:	
Rail:	YES	Rail:	NO
OIS Data Source:	VG 06/26/2011 THIRD_PARTY	OIS Data Source:	VG 06/26/2011 THIRD_PARTY
Assoc. Fac.:	CXO ILS (P)	Assoc. Fac.:	

RUNWAY LANDING STRIP COMMENTS

RUNWAY 14 COMMENTS

RUNWAY 32 COMMENTS

COMMENTS

Topic	Priority	Date	Remark
SURVEY	1	11/05/1999	NGS 405 SURVEY DATED 04/18/98
ADDITIONAL_FLIGHT_DATA	1	06/26/2000	ASOS. 936-760-4237
NFDD	3	02/25/2004	PER NFDD #049 DATED 03/12/04, ARPT NAME CHANGED FROM LONE STAR RGNL TO LONE STAR EXECUTIVE, CITY FROM CONROE TO HOUSTON
LIGHTS	5	06/05/2006	RWY 14/32 TO CHANGE RWY 14 VASI TO PAPI PER NFDD #080 DATED 04/26/06
SURVEY	5	06/27/2007	ALTERNATE ALTIMETER SOURCE, KDWH, ADDED PER AVN-120
OWNER	2	10/15/2007	LIGHTS OWNED BY MONTGOMERY COUNTY
GENERAL	7	10/16/2007	RWY 01/19 BEING EXTENDED ON NORTH END. DATA PROVIDED BY LOCAL SURVEY. NFDD #217 DATED 11/08/07
			RWY 19 PAPI DATA PROVIDED BY PROJECT MGR, 11/05/07
			RWY 01 PAPI DATA TO CHANGE ANGLE & MODIFY DATA FORWARDED BY TX ADO FROM PROJECT MGR, 10/15/07
			TDZE USED IN LIEU OF UNKNOWN RRP ELEVATION
NFDD	9	12/09/2008	TCH IS A CALCULATED VALUE PER NFDD # 238 DATED 12/10/08 RWY 32 4 BOX VASI DELETED.

SIAPS

Nav Ident	Nav Type	Description	FAS	Amendment	Type
		RNAV (GPS) RWY 32	329 / TREE / N30°20'43.08" / W095°24'14.66" 409 / TOWER / N30°17'30.60" / W095°21'41.30"	1	CIVIL
CXO	ILS	ILS OR LOC RWY 14	379 / TREE / N30°22'36.00" / W095°26'19.00"	2B	CIVIL
		RNAV (GPS) RWY 14	325 / TREE / N30°21'38.48" / W095°25'20.28" 553 / TOWER / N30°25'50.00" / W095°26'20.00"	ORG	CIVIL
		RNAV (GPS) RWY 19	374 / TREE / N30°22'12.18" / W095°24'17.43" 409 / TREE / N30°23'24.40" / W095°24'42.08"	ORG	CIVIL
		RNAV (GPS) RWY 1	A5 395 / TOWER / N30°20'19.00" / W095°25'43.00"	ORG	CIVIL
CXO	ILS	NDB RWY 14	480 / TANK / N30°23'34.00" / W095°28'30.00"	2B	CIVIL

Rpt Date: 20:00:36 08/15/2014

Rpt User: dso

ASSOCIATED MONITORS

ASSOCIATED DGPS


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KCXO Lone Star Executive Airport

Houston, Texas, USA



GOING TO HOUSTON?



FAA INFORMATION EFFECTIVE 18 SEPTEMBER 2014

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[Com](#) | [Nav](#) | [Svcs](#) | [Stats](#) | [Notes](#)

Location

FAA Identifier: CXO

Lat/Long: 30-21-08.5000N / 095-24-52.3000W

30-21.141667N / 095-24.871667W

30.3523611 / -95.4145278

(estimated)

Elevation: 245 ft. / 74.7 m (surveyed)

Variation: 05E (2000)

From city: 37 miles N of HOUSTON, TX

Time zone: UTC -5 (UTC -6 during Standard Time)

Zip code: 77303

Airport Operations

Airport use: Open to the public

Activation date: 05/1944

Sectional chart: [HOUSTON](#)

Control tower: yes

ARTCC: HOUSTON CENTER

FSS: MONTGOMERY COUNTY FLIGHT SERVICE STATION

NOTAMs facility: CXO (NOTAM-D service available)

Attendance: 0700-2100

Wind indicator: lighted

Segmented circle: yes

Lights: DUSK-DAWN. MIRL RY 14/32 PRESET LOW INTST; TO INCR INTST & ACTVT MALSR RY 14 AND REIL RY 32 - CTAF.

Beacon: white-green (lighted land airport)

Operates sunset to sunrise.

Airport Communications

CTAF: 124.125

ATIS: 118.325

WX ASOS: 118.325 (936-760-4237)

LONE STAR GROUND: 120.45 [0700-2200]

LONE STAR TOWER: 124.125 [0700-2200]

HOUSTON APPROACH: 119.7

HOUSTON DEPARTURE: 119.7

CLEARANCE DELIVERY: 119.55 WHEN ATCT CLSD 120.45

BORRN DP: 119.7

DREMR DP: 119.7

INDIE DP: 119.7

KARRR DP: 119.7

LURIC DP: 119.7

MMALT DP: 119.7

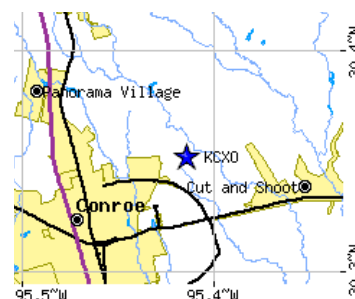
STRYA DP: 119.7

STYCK DP: 119.7

WATFO DP: 119.7

WYLSN DP: 119.7

WX ASOS at DWH (19 nm S): PHONE 281-251-7853

Road maps at: [MapQuest](#) [Bing](#) [Google](#) [Yahoo!](#)

Aerial photo

WARNING: Photo may not be current or correct



Nearby radio navigation aids

VOR radial/distance	VOR name	Freq	Var
IAH r346/24.0	HUMBLE VORTAC	116.60	05E
TNV r075/33.6	NAVASOTA VORTAC	115.90	08E

NDB name	Hdg/Dist	Freq	Var	ID
DAVID HOOKS	025/15.7	521	05E	DWH -
NIXIN	329/23.9	326	05E	BVP -
HUNTSVILLE	153/25.0	308	06E	UTS
WEISER	019/27.7	286	06E	EYQ

Airport Services

Fuel available: 100LL JET-A
 Parking: hangars and tie-downs
 Airframe service: MAJOR
 Powerplant service: MAJOR
 Bottled oxygen: HIGH/LOW
 Bulk oxygen: NONE

Runway Information

Runway 14/32

Dimensions: 6000 x 150 ft. / 1829 x 46 m
 Surface: concrete, in good condition
 Weight bearing capacity: Single wheel: 60.0
 Double wheel: 100.0
 Runway edge lights: medium intensity
RUNWAY 14
 Latitude: 30-21.557890N
 Longitude: 095-25.065068W
 Elevation: 230.1 ft.
 Gradient: 0.3%
 Traffic pattern: left
 Runway heading: 140 magnetic, 145 true
 Displaced threshold: 589 ft.
 Markings: precision, in good condition
 Visual slope indicator: 2-light PAPI on left (3.00 degrees glide path)
 Approach lights: MALSR: 1,400 foot medium intensity approach lighting system with runway alignment indicator lights

Runway end identifier lights: yes
 Touchdown point: yes, no lights
 Instrument approach: ILS/DME
 Obstructions: 10 ft. road, 200 ft. from runway, 40 ft. left of centerline
 10 FT ROAD FM THLD TO 200 FT.

RUNWAY 32
 30-20.742347N
 095-24.418363W
 241.3 ft.
 0.3%
 left
 320 magnetic, 325 true
 no
 nonprecision, in good condition

Runway 1/19

Dimensions: 5000 x 100 ft. / 1524 x 30 m
 Surface: concrete, in good condition
 Weight bearing capacity: Single wheel: 30.0
 Double wheel: 75.0
 Runway edge lights: medium intensity
RUNWAY 1
 Latitude: 30-20.737833N
 Longitude: 095-25.169333W
 Elevation: 229.6 ft.
 Gradient: 0.2%
 Traffic pattern: left
 Runway heading: 012 magnetic, 017 true
 Declared distances: TORA:5000 TODA:5000
 ASDA:5000 LDA:5000
 Markings: nonprecision, in good condition
 Visual slope indicator:

RUNWAY 19
 30-21.525833N
 095-24.888500W
 228.8 ft.
 0.2%
 left
 192 magnetic, 197 true
 TORA:5000 TODA:5000 ASDA:5000
 LDA:5000
 nonprecision, in good condition

Photo by Nigel Milligan / Kevin Williams
 Photo taken 25-Sep-2014
 looking west.

Do you have a better or more recent aerial photo of Lone Star Executive Airport that you would like to share? If so, please [send us your photo](#).

Sectional chart



Airport diagram

CAUTION: Diagram may not be current



Airport distance calculator

Flying to Lone Star Executive Airport? Find the distance to fly.

From to KCXO
[CALCULATE DISTANCE](#)

Sunrise and sunset

	Times for 06-Oct-2014	
	Local (UTC-5)	Zulu (UTC)
Morning civil twilight	06:55	11:55
Sunrise	07:19	12:19
Sunset	19:00	00:00
Evening civil twilight	19:24	00:24

Current date and time

Zulu (UTC)	06-Oct-2014 11:58:15
Local (UTC-5)	06-Oct-2014 06:58:15

METAR

KCXO 061153Z 00000KT 10SM CLR 18/18
 A2988 RMK AO2 SLP113 T01830178
 10189 20167 58001
KDWH 061053Z 00000KT 10SM CLR 20/18
 19nm S A2987 RMK AO2 SLP114 T02000183

TAF

KCXO 060520Z 0606/0706 00000KT P6SM
 FEW025 FM061000 15005KT P6SM
 BKN020 FM061600 17009KT P6SM
 VCSH SCT030 BKN120 FM061900
 17009KT P6SM VCSH SCT040 PROB30
 0619/0623 TSRA BKN040CB BKN250

NOTAMs

[Click for the latest NOTAMs](#)

NOTAMs are issued by the DoD/FAA and will open in a separate window not controlled by AirNav.

2-light PAPI on left (3.15 degrees glide path)	2-light PAPI on left (3.00 degrees glide path)
Touchdown point: yes, no lights	yes, no lights
Obstructions: none	4 ft. tree, 350 ft. from runway, 70 ft. right of centerline, 37:1 slope to clear

Airport Ownership and Management from official FAA records

Ownership: Publicly-owned

Owner: MONTGOMERY COUNTY

501 N. THOMPSON ST.

CONROE, TX 77301

Phone 936-539-7811

Manager: SCOTT SMITH

10260 CARL PICKERING MEMORIAL

CONROE, TX 77303

Phone 936-788-8311

Airport Operational Statistics

Aircraft based on the field: 329 Aircraft operations: avg 219/day *

Single engine airplanes: 234 58% local general aviation

Multi engine airplanes: 36 39% transient general aviation

Jet airplanes: 32 2% military

Helicopters: 3 <1% air taxi

Military aircraft: 24 * for 12-month period ending 30 July 2011

Additional Remarks

A23 HELICOPTERS USE RIGHT-HAND TRAFFIC.

- EXTENSIVE MILITARY HELICOPTER ACTIVITY ON ARPT.

- AVOID NOISE SENSITIVE AREA 10 MI SW QUADRANT OF ARPT.

- UNMANNED ACFT MAY BE OPERATING IN THE IMMEDIATE AREA DURING DALGT HRS.

Instrument Procedures

NOTE: All procedures below are presented as PDF files. If you need a reader for these files, you should [download](#) the free Adobe Reader.

NOT FOR NAVIGATION. Please procure official charts for flight.

FAA instrument procedures published for use between 18 September 2014 at 0901Z and 16 October 2014 at 0900Z.

STARs - Standard Terminal Arrivals

HUDZY TWO

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OHIO TWO

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RIICE SEVEN

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WHAEL ONE

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IAPs - Instrument Approach Procedures

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RNAV (GPS) RWY 14

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RNAV (GPS) RWY 19

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RNAV (GPS) RWY 32

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NDB RWY 14

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NOTE: Special Alternate Minimums apply

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Departure Procedures

ALEXANDRIA SIX

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LUFKIN SEVEN

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LURIC ONE (RNAV) **CHANGED**	2 pages: [1] [2]
MMALT ONE (RNAV) **CHANGED**	2 pages: [1] [2]
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STRYA ONE (RNAV) **CHANGED**	2 pages: [1] [2]
STYCK ONE (RNAV) **CHANGED**	download
WATFO ONE (RNAV) **CHANGED**	download
WYLSN ONE (RNAV) **CHANGED**	2 pages: [1] [2]
NOTE: Special Take-Off Minimums/Departure Procedures apply download (70KB)	

Other nearby airports with instrument procedures:

[KDWH](#) - David Wayne Hooks Memorial Airport (19 nm S)
[6R3](#) - Cleveland Municipal Airport (21 nm E)
[KIAH](#) - George Bush Intercontinental/Houston Airport (22 nm S)
[KUTS](#) - Huntsville Municipal Airport (25 nm N)
[KEYQ](#) - Weiser Air Park (28 nm SW)

FBO, Fuel Providers, and Aircraft Ground Support

Business Name	Contact	Services / Description	Fuel Prices	Comments
 General Aviation Services	123.30 936-760-1717 [web site] [email]	In business since 1982, General Aviation Services will provide you with the best FBO services in the area. We are located center field between taxi ways Bravo and Charlie, the best location on the field for a quick turn around and convenient to all runways, which allows for a smooth and hassle free arrival and departure. We have the best prices in the area. Our experienced, professional, and courteous staff will see to your every request. Make your next stop with us and see why our customers keep coming back for more!" More info and photos of General Aviation Services 	 100LL Jet A FS \$5.65 \$5.10 SS \$5.25 --- GUARANTEED MEMBERS ONLY Discounts Login Join	★★★★★ 14 read write
 Galaxy FBO	ASRI 130.525 936-494-4252 [web site] [email]	Come see what has made Galaxy the best reviewed FBO at the LoneStar Executive Airport! Our friendly and attentive staff is always ready to assist you during your stay at KCXO. Free courtesy cars, volume fuel discounts, maintenance, rental car reservations, oxygen/nitrogen services, hotel reservations, catering, aircraft detailing. More info and photos of Galaxy FBO 	 100LL Jet A FS \$5.49 \$5.19 GUARANTEED MEMBERS ONLY Discounts Login Join	★★★★★ 12 read write
 Wing Jet Center, LLC	936-441-9555 toll-free 1-866-449-9555 [web site] [email]	Aviation fuel, Oxygen service, Aircraft parking (ramp or tiedown), Hangars, Hangar leasing / sales, GPU / Power cart, Passenger terminal and lounge, ...  More info about Wing Jet Center, LLC	 EPIC 100LL Jet A not yet rated FS \$6.69 \$5.25 GUARANTEED FS=Full service SS=Self service UPDATE PRICES	2 read write

Where to Eat: Catering, Restaurants, Food shops

Business Name	Contact	Services / Description	Distance	Comments
Black Walnut Cafe	936-202-2824 [web site]	Restaurant More info about Black Walnut Cafe	on airport	not yet rated 1 read write

Where to Stay: Hotels, Motels, Resorts, B&Bs, Campgrounds

In this space we feature lodging establishments that are convenient to the Lone Star Executive Airport. If your hotel/inn/B&B/resort is near the Lone Star Executive Airport, provides convenient transportation, or is otherwise attractive to pilots, flight crews, and airport users, consider listing it here.

FEATURE A LODGING ESTABLISHMENT

AirNav users who flew into KCXO have stayed at...

[COURTYARD BY MARRIOTT HOUSTON THE WOODLANDS](#)
[SUPER 8 CONROE](#)
[BAYMONT INN AND SUITES](#)
[DAYS INN CONROE](#)

Miles	Price (\$)
12.8	110-111
4.1	48-64
5.4	68-93
4.9	47-60

Hotels in other cities near Lone Star Executive Airport

9 in Conroe	3 in Magnolia
2 in Willis	3 in Cleveland
13 in The Woodlands	2 in New Caney
4 in Montgomery	

Other hotels near Lone Star Executive Airport

[HOLIDAY INN EXPRESS HOTEL & SUITES CONROE INTERSTATE45 NORTH](#)
[HAMPTON INN & SUITES CONROE INTERSTATE 45 NORTH](#)
[COMFORT INN CONROE](#)
[FAIRFIELD INN & SUITES BY MARRIOTT HOUSTON CONROE/WOODLANDS](#)
[LA QUINTA INN & SUITES CONROE](#)
[DAYS INN CONROE](#)
[RAMADA INN- CONROE/THE WOODLANDS](#)

Miles	Price (\$)
3.9	116-117
3.9	125-135
4.0	89-90
4.1	109-119
4.2	95-96
4.2	
5.5	66-70

Distances are approximate, and may vary depending on the actual route traveled and the location of the travel start on the airport.

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APPENDIX B: Data Reduction Procedures for Using Ground Vehicle Friction Measurements to Calculate Aircraft Tire Friction Performance

Tom Yager

Distinguished Research Associate
NASA Langley Research Center

Data Reduction Procedures
For
Using Ground Vehicle Friction Measurements
To
Calculate Aircraft Tire Friction Performance
Tom Yager, NASA Langley Research Center

Basic Data Requirements –

1. Accurate and suitable ground vehicle friction measurements must be collected through a speed range (e.g. 10-60 mph) for each wet surface condition evaluated.
2. The test tire(s) operating mode and inflation pressure must be properly maintained and documented
3. The test tire(s) operating mode should be selected to provide one of three friction boundary conditions: locked-wheel skidding, peak braked rolling, or peak yawed (cornering) rolling
4. A characteristic dry friction coefficient, μ_{cd} must be determined experimentally for each ground vehicle test tire operating mode by conducting test runs at very low speed (<3 mph)
5. The aircraft main landing gear tire inflation pressure value must be known

Overall Tire Friction Methodology – See figure 1

Data Reduction Procedures –

STEP 1 - Determine best fit curve for aircraft and ground vehicle friction- speed gradient data. Figure 2 provides an example of the friction data range obtained on a wet slurry seal asphalt surface with the NASA instrumental B-737 aircraft and four different ground test vehicles: a diagonal-braked vehicle, a mu-meter, a Saab friction tester, and a BV-11 skiddometer.

STEP 2 – For each test vehicle, calculate the minimum tire dynamic hydroplaning spin down speed using the following equation (see table I)

$$V_p, \text{Knots} = 9\sqrt{p} \quad (1a)$$

$$V_p, \text{mph} = 10.35\sqrt{p} \quad (1b)$$

where V_p , tire dynamic hydroplaning spindown speed

p , tire inflation pressure, psi

NOTE: Experimental data obtained with the mu-meter trailer indicates a V_p value of 45 mph rather than the 33 mph derived from eq. 1b. Use $V_p = 45 \text{mph}$ for mu-meter calculations.

STEP 3 – Tabulate characteristic dry friction coefficient values obtained experimentally for each ground vehicle test tire (see table I).

STEP 4 – Calculate characteristic dry friction coefficient value for air craft main gear tire using the following equation:

$$\mu_{cd} = 0.93 - 0.0011 p \quad (2)$$

where, μ_{cd} characteristic dry friction coefficient

p , tire inflation pressure, psi

NOTE: Table I gives these values for both the B-737 and B-727 aircraft together with the pertinent ground vehicle tire friction parameters.

STEP 5 – Select and tabulate an appropriate number (minimum 5) of the friction coefficient and ground speed values to properly define the friction-speed gradient data measured by each ground test vehicle. Determine the ground speed/hydroplaning speed ratio associated with each of the selected friction coefficient values (see table II).

STEP 6 – Determine ground vehicle tire hydroplaning parameter values using the following general relationship:

$$\bar{y} = \frac{\mu_{wet}}{\mu_{cd}} \quad (3)$$

where $\bar{y}$, tire hydroplaning parameter

μ_{wet} , Experimental or predicted wet pavement friction coefficient value

μ_{cd} , characteristic dry friction coefficient value

In determining the tire hydroplaning parameter, distinction is made between two types of tire operating modes-non rotating and rotating. For locked-wheel, sliding (non rotating) tire friction data (e.g. DBV), the tire hydroplaning parameter is labeled $\bar{y}_L$. For braked or yawed rolling (rotating) tire friction data (e.g. BV-11, SFT and Mu-meter), the tire hydroplaning parameter is labeled $\bar{y}_R$. The relationship between $\bar{y}_L$ and $\bar{y}_R$, which was empirically derived from NASA track aircraft tire test data, is given in table III. Hence, knowing one tire hydroplaning parameter allows determination of the other (see table III).

STEP 7 – Calculate aircraft tire maximum braking friction coefficient, μ_{max} , values by simply multiplying the $\bar{y}_R$ values determined in STEP 6 by the aircraft tire characteristic dry friction coefficient value determined for eq. 2 in STEP 4 (see table II).

STEP 8 – Determine estimated aircraft tire effective braking coefficient, μ_{eff} , values by use of the following equations:

$$\text{For } \mu_{max} < 0.7; \mu_{eff} = 0.2 \mu_{max} + 0.7143 \mu_{max}^2 \quad (4a)$$

$$\text{For } \mu_{max} \geq 0.7; \mu_{eff} = 0.7 \mu_{max} \quad (4b)$$

These relationships between aircraft tire maximum braking and effective braking friction coefficient are based on the assumption that the total aircraft braking system (tires, brakes, hydraulics, gear, and antiskid) efficiency can be generalized by a single curve defined by equations 4 a and b. Values derived for B-737 aircraft are listed in table II.

STEP 9 – Calculate an equivalent aircraft ground speed associated with each μ_{eff} value by multiplying the appropriate ground vehicle speed ratio obtained in STEP 5 by the aircraft tire hydroplaning speed determined in STEP 2 (see table II).

STEP 10 – Compare estimated aircraft tire friction performance to actual measured performance (see figure 3).

Supplemental Data Analysis –

1. Statistical methods should be used to identify data set tolerances and degree of confidence in data correlation.
2. Parameter sensitivity studies should be performed to define effects on data correlation agreement.

Table I.- Compilation of test aircraft and ground vehicle tire friction parameters

TEST PARAMETER	TEST AIRCRAFT		GROUND TEST VEHICLES			
	B-737	B-727	DIAGONAL BRAKED	MU- METER	FRICTION TESTER	BV-11 SKIDDOMETER
Tire: Size Infl. Press. kPa (psi) Tread design	Main gear 40 x 14 1069 (155) 4-Groove	Main gear 49 x 17 931 (135) 6-Groove	ASTM E524 G78 x 15 165 (24) Smooth	RL-2 4.00 - 8 69 (10) Smooth	RL-2 4.00 - 8 207 (30) Smooth	RL-2 4.00 - 8 207 (30) Smooth
Braking method	Maximum Antiskid	Maximum Antiskid	Locked Wheel	None (7.5° yaw)	Constant 10% Slip	Constant 17% Slip
Friction reading	μ_{EFF}	μ_{EFF}	μ_{SKID}	μ_{SIDE}	μ_{DRAG}	μ_{DRAG}
Spin-down hydroplaning Speed, V_p , knots (mph)	112* (129)	105* (121)	44.1* (50.8)	39.1 (45)	49.3* (56.7)	49.3* (56.7)
Low speed characteristic dry friction, μ_{cd}	0.76*	0.78*	1.20	0.90	1.10	1.10

* Calculated values using:

$$(V_p) \text{ spin-down} = 3.43 \sqrt{p}$$

for SI Units

$$\mu_{cd} = 0.93 - 1.6 \times 10^{-4} p$$

$$(V_p) \text{ spin-down} = 9 \sqrt{p}$$

for U.S. Customary Units

$$\mu_{cd} = 0.93 - 1.1 \times 10^{-3} p$$

where p, tire inflation pressure, kPa (psi)

Table II - Compilation of parameter values used to estimate aircraft braking performance from ground vehicle data
(a) Slurry seal asphalt surface; Truck wetted; Water depth 0.5mm (0.02 in.)

GROUND TEST VEHICLE	FAIRED μ	SPEED, V_G		V_G/V_P	TIRE HYDROPLANING PARAMETERS		ESTIMATED B-737 AIRCRAFT BRAKING			ACTUAL B-737 A/C μ_{EFF}
		KNOTS	MPH		$\bar{Y}_L$	$\bar{Y}_R$	μ_{MAX}	μ_{EFF}	V_G , KNOTS	
Diagonal	0.77	10	12	0.227	0.642	0.895	0.680	0.466	25.4	—
Braked	.59	20	23	.454	.492	.742	.564	.340	50.8	0.365
Vehicle	.47	30	34	.680	.392	.642	.488	.268	76.2	.290
(DBV)	.38	40	46	.907	.317	.564	.429	.217	101.6	—
	.31	50	58	1.134	.258	.495	.376	.176	126.6	—
↓	.24	60	69	1.361	.200	.412	.313	.133	152.4	—
Saab	—	10	12	.203	—	—	—	—	22.7	—
Friction	.93	20	23	.406	.581	.845	.642	.423	45.5	.380
Tester	.78	30	34	.609	.460	.709	.539	.315	68.2	.315
(SFT)	.66	40	46	.811	.350	.600	.456	.240	90.8	.250
	.54	50	58	1.014	.255	.491	.373	.174	113.6	—
↓	.43	60	69	1.217	.188	.391	.297	.122	136.3	—
BV-11	—	10	12	.203	—	—	—	—	22.7	—
SKiddometer	.93	20	23	.406	.581	.845	.642	.423	45.5	.380
	.80	30	34	.609	.478	.727	.553	.329	68.2	.315
	.67	40	46	.811	.359	.609	.463	.246	90.8	.250
	.55	50	58	1.014	.262	.500	.380	.179	113.6	—
↓	.44	60	69	1.217	.193	.400	.304	.127	136.3	—
Mu-meter	.88	10	12	.256	.873	.978	.743	.520	28.7	.430
	.83	20	23	.512	.689	.922	.701	.491	57.3	.345
	.78	30	34	.767	.604	.867	.659	.442	85.9	.260
	.72	40	46	1.023	.544	.800	.608	.386	114.6	—
	.67	50	58	1.279	.494	.744	.565	.341	143.2	—
↓	.62	60	69	1.535	.441	.689	.524	.301	171.9	—

Table III. - Relationship between rotating ($\bar{Y}_R$) and nonrotating ($\bar{Y}_L$) tire hydroplaning parameters.

$\bar{Y}_R$	$\bar{Y}_L$	$\bar{Y}_R$	$\bar{Y}_L$	$\bar{Y}_R$	$\bar{Y}_L$	$\bar{Y}_R$	$\bar{Y}_L$	$\bar{Y}_R$	$\bar{Y}_L$
0.000	0.000	.200	.095	.400	.193	.600	.350	.800	.544
.005	.002	.205	.097	.405	.196	.605	.355	.805	.548
.010	.005	.210	.099	.410	.199	.610	.360	.810	.551
.015	.007	.215	.101	.415	.202	.615	.365	.815	.555
.020	.010	.220	.104	.420	.205	.620	.370	.820	.560
.025	.012	.225	.106	.425	.208	.625	.375	.825	.564
.030	.015	.230	.108	.430	.211	.630	.380	.830	.568
.035	.017	.235	.111	.435	.215	.635	.385	.835	.572
.040	.019	.240	.113	.440	.218	.640	.390	.840	.576
.045	.021	.245	.116	.445	.221	.645	.395	.845	.581
.050	.024	.250	.118	.450	.225	.650	.400	.850	.586
.055	.026	.255	.120	.455	.228	.655	.405	.855	.591
.060	.028	.260	.122	.460	.232	.660	.410	.860	.597
.065	.030	.265	.125	.465	.235	.665	.415	.865	.602
.070	.033	.270	.127	.470	.239	.670	.421	.870	.608
.075	.035	.275	.130	.475	.243	.675	.426	.875	.614
.080	.038	.280	.132	.480	.247	.680	.431	.880	.620
.085	.040	.285	.134	.485	.250	.685	.437	.885	.626
.090	.043	.290	.137	.490	.254	.690	.442	.890	.634
.095	.045	.295	.139	.495	.258	.695	.447	.895	.642
.100	.047	.300	.141	.500	.262	.700	.451	.900	.650
.105	.050	.305	.144	.505	.266	.705	.456	.905	.659
.110	.052	.310	.146	.510	.270	.710	.461	.910	.667
.115	.054	.315	.148	.515	.274	.715	.466	.915	.677
.120	.057	.320	.151	.520	.279	.720	.471	.920	.687
.125	.059	.325	.154	.525	.283	.725	.476	.925	.698
.130	.062	.330	.156	.530	.287	.730	.481	.930	.709
.135	.064	.335	.158	.535	.292	.735	.485	.935	.720
.140	.066	.340	.161	.540	.296	.740	.490	.940	.734
.145	.068	.345	.163	.545	.300	.745	.495	.945	.748
.150	.071	.350	.166	.550	.305	.750	.500	.950	.762
.155	.073	.355	.168	.555	.309	.755	.504	.955	.779
.160	.075	.360	.170	.560	.314	.760	.509	.960	.795
.165	.078	.365	.173	.565	.318	.765	.514	.965	.815
.170	.080	.370	.175	.570	.322	.770	.518	.970	.835
.175	.083	.375	.178	.575	.327	.775	.523	.975	.859
.180	.085	.380	.181	.580	.332	.780	.527	.980	.882
.185	.087	.385	.184	.585	.336	.785	.531	.985	.910
.190	.090	.390	.187	.590	.340	.790	.535	.990	.940
.195	.092	.395	.190	.595	.345	.795	.540	.995	.975
								1.000	1.000

Figure 1.- Methodology used to estimate aircraft tire friction performance.

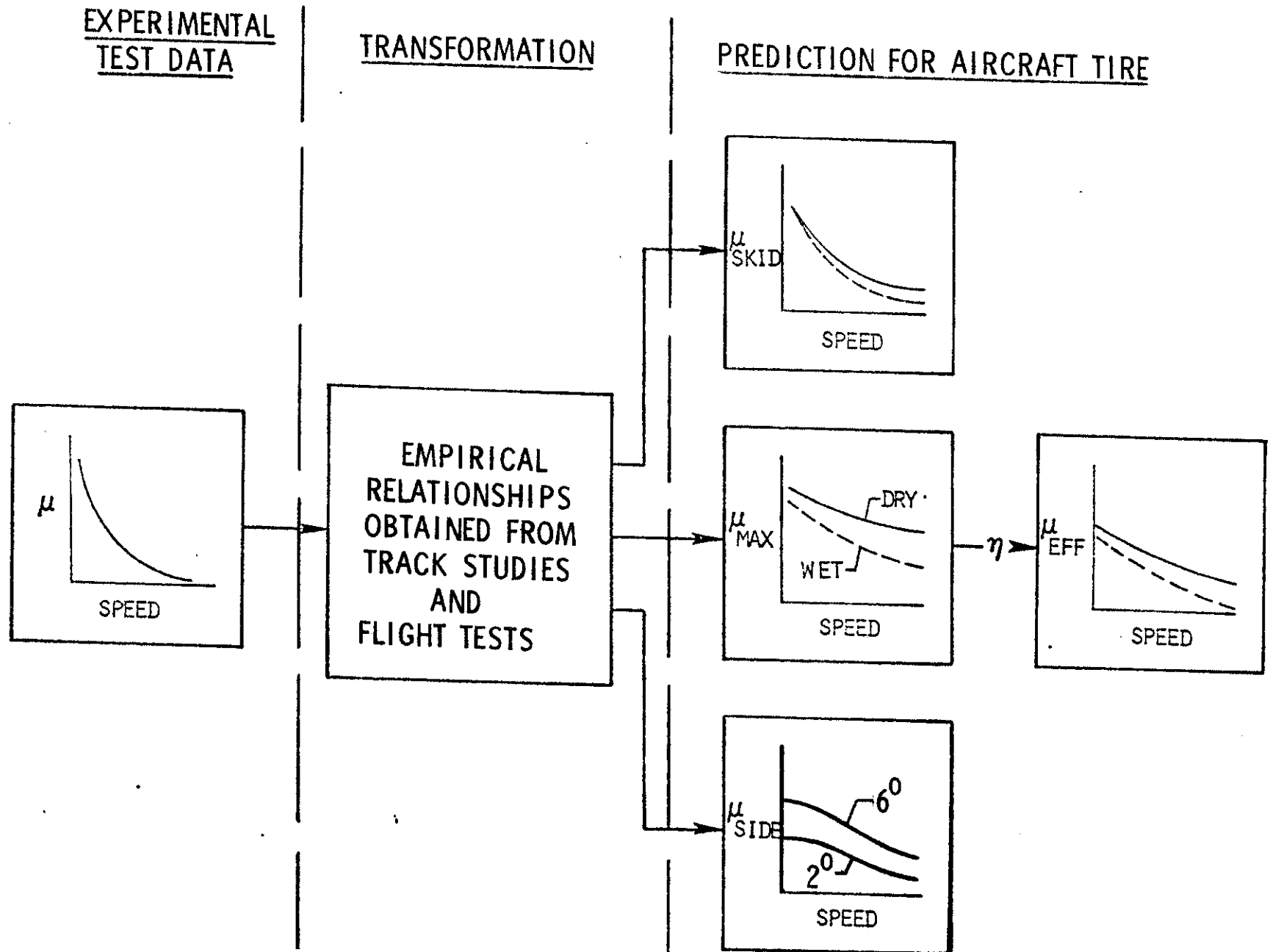


Figure 2 - RANGE OF AIRCRAFT AND GROUND VEHICLE PRACTICAL MEASUREMENTS

SLURRY SEAL ASPHALT SURFACE
THICK WETTED WATER DEPTH 0.5 INCH (0.02 IN.)

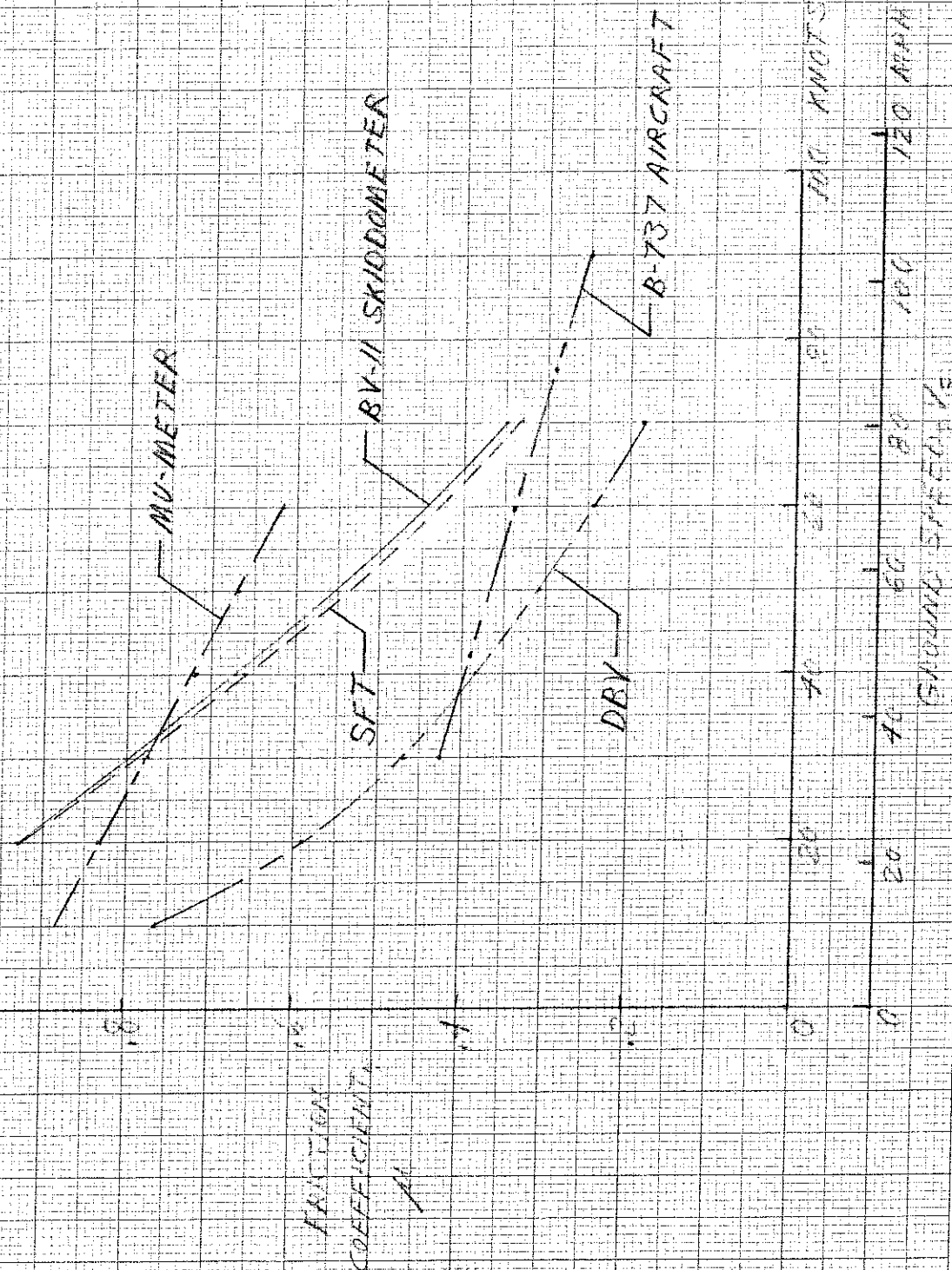
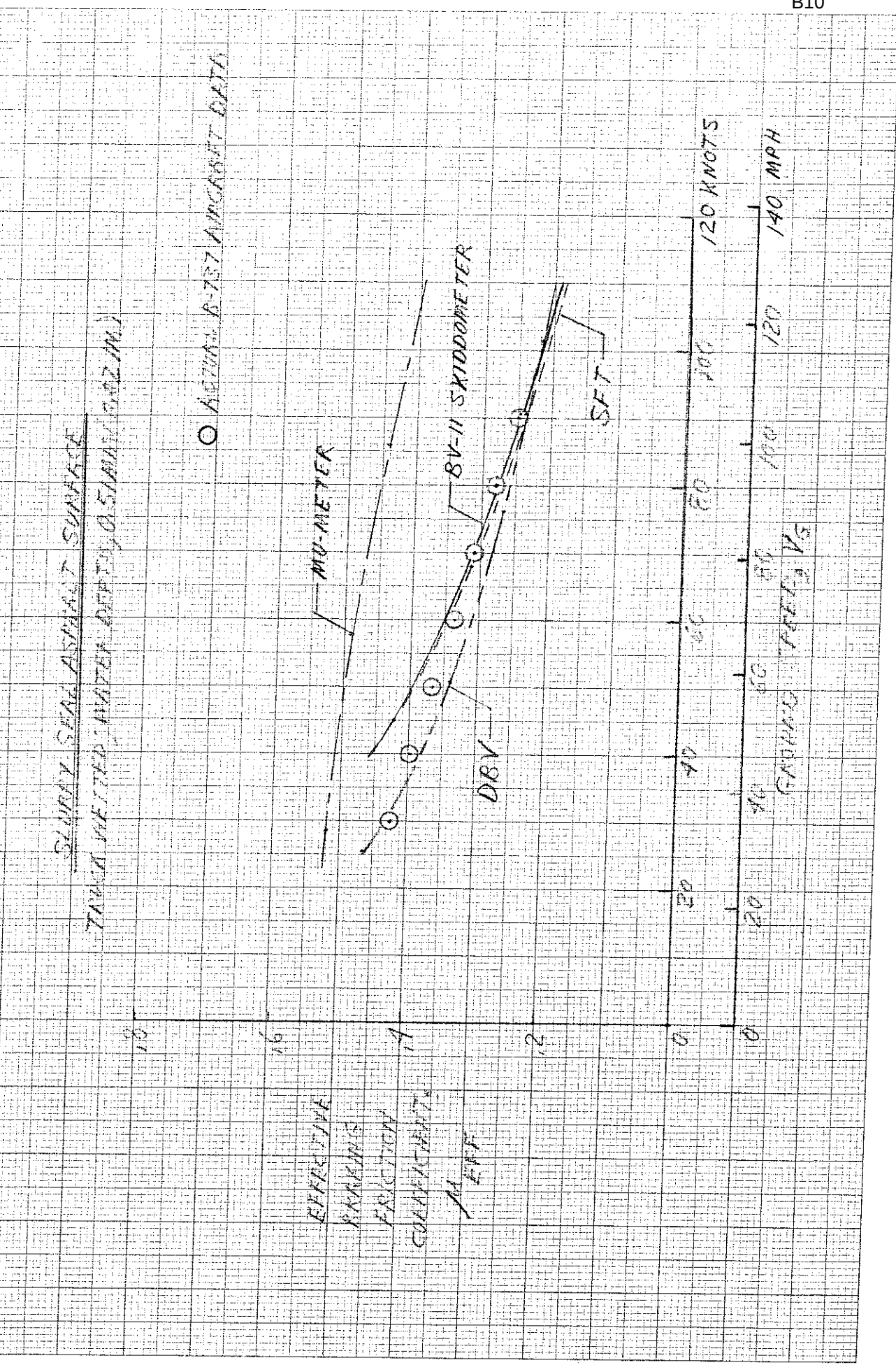


Figure 3. - ESTIMATED AIRCRAFT BRAKING PERFORMANCE FROM SPEED WHEEL FRICTION DATA

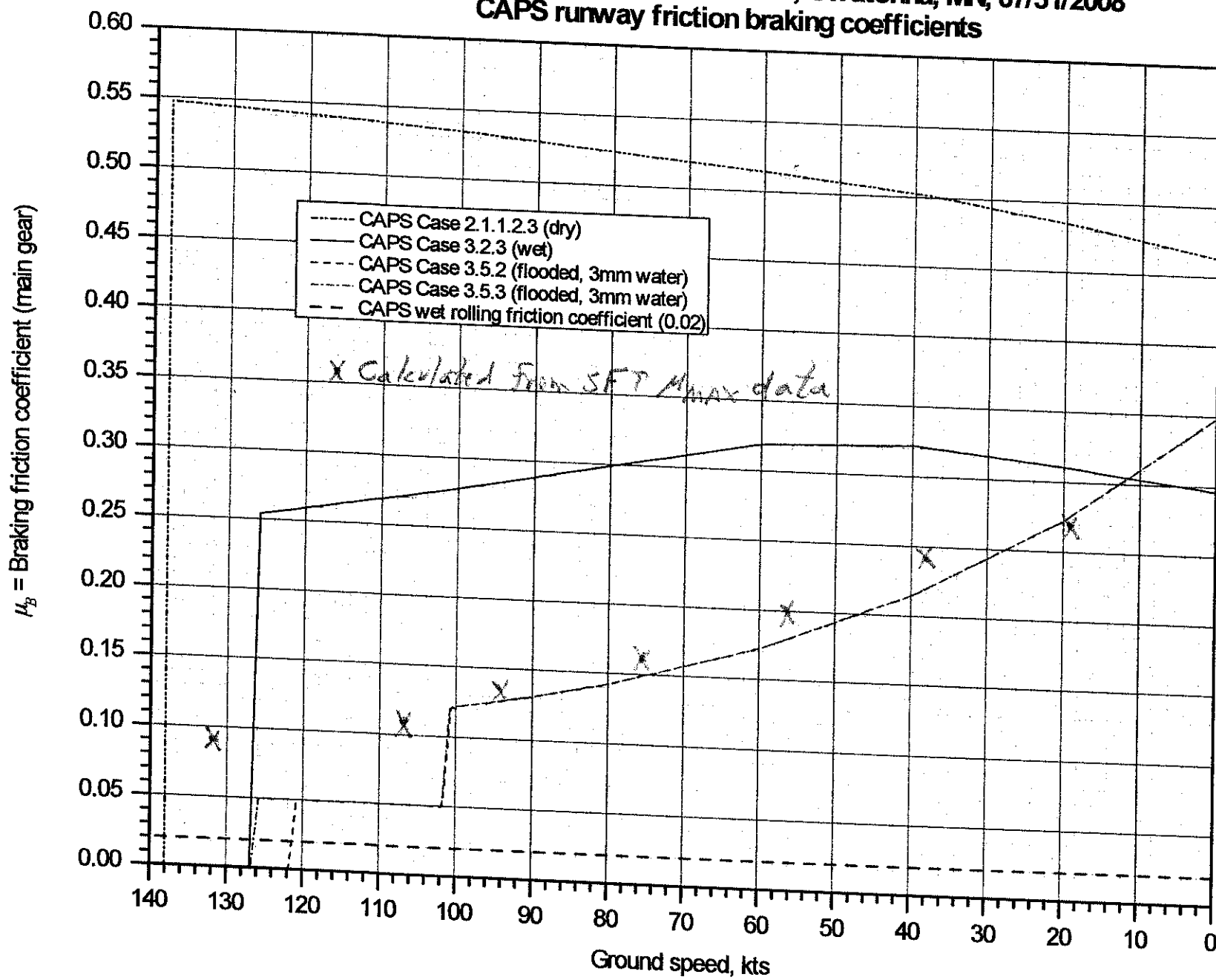


SET $M_{GRY} = 1.10$; $V_p = 50.9$ mph

SECRET

[illegible]

DCA08MA085: BAe125-800A, N818MV, Owatonna, MN, 07/31/2008
CAPS runway friction braking coefficients



Appendix C: “KXCO_RWY1_measurements.xls”

Excel spreadsheet forms

NOTE: Darker-shaded points are lower priority			Runway y (ft.)			
Station #	Runway x (ft.)		-35	-20	-5	+5
1	300	Name	300-35	300-20	300-5	300+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
2	800	Name	800-35	800-20	800-5	800+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
3	1300	Name	1300-35	1300-20	1300-5	1300+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
4	1800	Name	1800-35	1800-20	1800-5	1800+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
5	2300	Name	2300-35	2300-20	2300-5	2300+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
6	2800	Name	2800-35	2800-20	2800-5	2800+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				

7	3300	Name	3300-35	3300-20	3300-5	3300+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
8	3800	Name	3800-35	3800-20	3800-5	3800+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
9	4300	Name	4300-35	4300-20	4300-5	4300+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				
10	4800	Name	4800-35	4800-20	4800-5	4800+5
		Macro 1 (mm)				
		Macro 2 (mm)				
		Macro 3 (mm)				
		Macro avg. (mm)				
		Slope (deg.)				
		Slope (%)				

Note: + slope is centerline higher than runway edge

Equipment: Neubert Aero Corp. (NAC) Dynamic Friction Tester (DFT)

Slip ratio: 12%

Tire inflation pressures:

Time	Pressure (psi)

*** Run numbers ***

PLANNED	Runway y coordinate (ft.)			
Speed (mph)	-35	-20	-5	+5
60	15	5	9	1 & 13
50	16	6	10 & 19	2
40	17 & 20	7	11	3
30	18	8 & 14	12	4

ACTUAL	Runway y coordinate (ft.)			
Speed (mph)	-35	-20	-5	+5
60				
50				
40				
30				

Run Log

Run #	Time	Other identifying information
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		
15		
16		
17		
18		
19		
20		

Appendix D:

Proposed Measurement Point Location Procedures

This Appendix contains proposed methods for efficiently locating the runway measurement points. These are only *proposed* procedures, and are the result of imagining how things might work out on the runway. In reality, the procedures will likely have to be adjusted by trial-and-error based on actual experience, in real-time, so as to achieve the most productive workflow.

Locating the runway measurement points

1. At the start of the test, navigate to the runway 35 threshold using the Timble Geo7x device, and verify that the device locates the threshold properly. This provides a “sanity check” on the combination of the coordinates programmed into the device, and the device’s actual accuracy.
2. Proceed to the first runway x station ($x=300$ ft.), using *both* the Geo7x and the measuring wheel to locate the x coordinate. Verify agreement.
3. Stretch the measuring tape across the runway, with the 40 ft. mark located on the runway centerline, and the 0 mark (start of the tape) on the left side of the runway.
4. Using the chalk, mark and label the measurement points as shown in the Table D-1 and in Figure D-1:

Point label $x = \text{runway } x \text{ coordinate}$	Point y-coordinate	Tape measure mark
$x-35$	-35 ft.	5 ft.
$x-20$	-20 ft.	20 ft.
$x-5$	-5 ft.	35 ft.
$x+5$	+5 ft.	45 ft.

Table D-1. Tape marks corresponding to measurement y-coordinates.

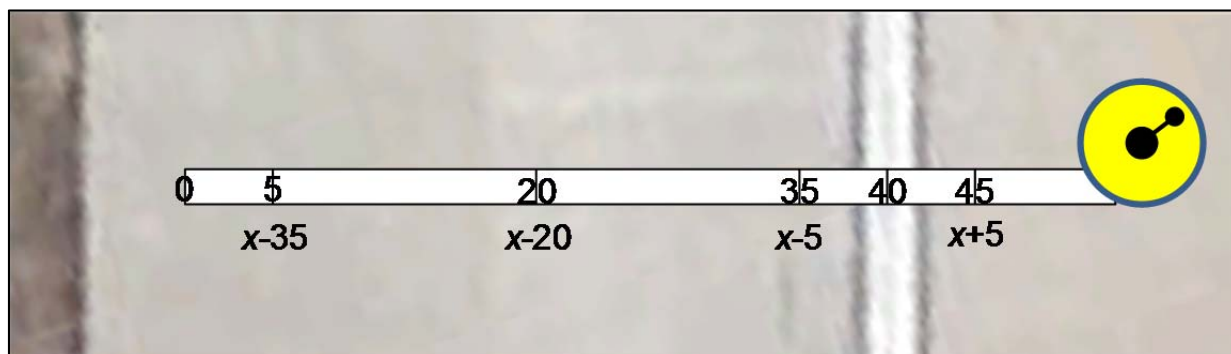


Figure D-1. Illustration of correspondence between tape marks and measurement y-coordinates.

5. After the measurement points are labeled, proceed to the next x-coordinate and locate / label the measurement points there. However, the Macrotexture team members locating the points should always remain within 1000 ft. of the CXO team member who is maintaining contact with the DFT team and airport tower. Further, no team members will venture north of the x=3800 ft. point by themselves, so as to avoid encroaching on the runway 14-32 intersection safety zone. Movement north of x=3800 ft. will be coordinated with the control tower by the CXO team members.

The Macrotexture team will be attentive to whistle blows from their CXO team member. If this individual blows three short blasts on the whistle, the team will immediately clear the runway. If he blows one long blast on the whistle, the team will assemble at his location.

6. In order to obtain maximum coverage of the runway in the minimum amount of time (in case testing gets interrupted for whatever reason), the Macrotexture team should take macrotexture and cross-slope measurements at x-coordinate stations in the following order: Stations 1, 3, 5, 7, 9, 10, 8, 6, 4, 2. Note that Station 9 is within the runway 14-32 intersection safety zone, and may be tested “out of order” if a lull in airport traffic makes testing that point opportune. However, locating and labeling the measurement points can proceed in the numeric order of stations, since this activity should take less time than the macrotexture and cross-slope measurements.

Testing within the runway 14-32 intersection safety zone

Procedures for testing within the 14-32 intersection safety zone will be briefed by CXO personnel on the morning of the test. Note that the DFT team will likely need clearance from the tower before each of their test runs.